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NAVAL POSTGRADUATE SCHOOL  
Monterey, California



THESIS

PERFORMANCE OF MULTIPLE, ANGLED NOZZLES  
WITH SHORT MIXING STACK EDUCTOR SYSTEMS

by

Charles Carver Davis

September 1981

Thesis Advisor:

P.F. Pucci

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REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER	2. GOVT ACCESSION NO. <b>AD-A220</b>	3. REGISTRY'S CATALOG NUMBER <b>817</b>
4. TITLE (and Subtitle) Performance of Multiple, Angled Nozzles with Short Mixing Stack Eductor Systems		5. TYPE OF REPORT & PERIOD COVERED Master's Thesis September 1981
7. AUTHOR(s) Charles Carver Davis		6. PERFORMING ORG. REPORT NUMBER
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Postgraduate School Monterey, California 93940		8. CONTRACT OR GRANT NUMBER(s)
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Postgraduate School Monterey, California 93940		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		12. REPORT DATE September 1981
		13. NUMBER OF PAGES 434
		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Angled, multiple nozzle, gas eductor system, cold flow tests on short mixing stacks		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Cold flow tests were conducted on a four-nozzle gas eductor system to evaluate the feasibility of reducing mixing stack lengths by the application of angled primary flow nozzles. Three short mixing stacks with length to diameter ratios of 1.75, 1.5, and 1.25 were tested using a set of straight nozzles and a series of angled nozzles having tilt angles of 10, 15, 20 and 22.5 degrees. The nozzles were constructed with an area of primary flow to area of mixing stack ratio of 2.5. Pumping coefficients, mixing stack pressure		

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Performance of Multiple, Angled Nozzles  
with Short Mixing Stack Eductor Systems

by

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Submitted in partial fulfillment of the  
requirements for the degree of

MASTER OF SCIENCE IN MECHANICAL ENGINEERING

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### ABSTRACT

Cold flow tests were conducted on a four-nozzle gas eductor system to evaluate the feasibility of reducing mixing stack lengths by the application of angled primary flow nozzles. Three short mixing stacks with length to diameter ratios of 1.75, 1.5, and 1.25 were tested using a set of straight nozzles and a series of angled nozzles having tilt angles of 10, 15, 20, and 22.5 degrees. The nozzles were constructed with an area of primary flow to area of mixing stack ratio of 2.5. Pumping coefficients, mixing stack pressure distributions, flow changes, exit velocity profiles, and back pressures were used to evaluate the various mixing stack length and angled nozzle combinations. A preferred combination was obtained, which, when compared with a longer mixing stack with a length to diameter ratio of 2.5 using straight nozzles, showed equal pumping coefficients and comparable mixing stack pressure distributions while actually improving the mixing. Back pressure increases for the preferred combination of short mixing stack and angled nozzles were slightly greater than for the longer mixing stack with straight nozzles.

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## NOMENCLATURE

### English Letter Symbols

A	Area (in. <sup>2</sup> )
c	Sonic velocity (ft/sec)
C	Coefficient of discharge
D	Diameter (in.)
F <sub>a</sub>	Thermal expansion factor
F <sub>fr</sub>	Wall skin-friction force (lbf)
g <sub>c</sub>	Proportionality factor in Newton's Second Law ( $g_c = 32.174 \text{ lbf-ft/lbf-sec}^2$ )
h	Enthalpy (Btu/lbm)
k	Ratio of specific heats
L	Length (in.)
P	Pressure (in. H <sub>2</sub> O)
P <sub>a</sub>	Atmospheric pressure (in. Hg)
P <sub>v</sub>	Velocity head (in. H <sub>2</sub> O)
PMS	Static pressure along the length of the mixing stack (in. H <sub>2</sub> O)
R	Gas constant for air ( $R = 53.34 \text{ ft-lbf/lbm-R}$ )
s	Entropy (Btu/lbm-R)
S	Distance from primary nozzle exit plane to mixing stack entrance plane (in.)
T	Absolute temperature (R)

u	Internal energy (Btu/lbm)
U	Velocity (ft/sec)
v	Specific volume (ft <sup>3</sup> /lbm)
W	Mass flow rate (lbm/sec)
Y	Expansion factor

#### Dimensionless Groupings

A*	Ratio of secondary flow area to primary flow area
AR	Area ratio
f	Friction factor
K	Flow coefficient
K <sub>e</sub>	Kinetic energy correction factor
K <sub>m</sub>	Momentum correction factor at the mixing stack exit
K <sub>p</sub>	Momentum correction factor at the primary nozzle exit
L/D	Ratio of mixing stack length to mixing stack diameter
M	Mach number
p*	Pressure coefficient
PMS*	Mixing stack pressure coefficient
Re	Reynolds number
S/D	Standoff; ratio of distance from primary nozzle exit plane to entrance plane of the mixing stack (S) to the diameter of the mixing stack (D)

$T^*$	Absolute temperature ratio of the secondary flow to primary flow
$T_t^*$ , $TT^*$	Absolute temperature ratio of the tertiary flow to primary flow
$W_s^*$ , $W^*$	Secondary mass flow rate to primary mass flow rate ratio
$W_t^*$ , $WT^*$	Tertiary mass flow to primary mass flow rate ratio
$e^*$	Induced flow density to primary flow density ratio

#### Greek Letter Symbols

$\mu$	Absolute viscosity (lbf-sec/ft <sup>2</sup> )
$e$	Density (lbm/ft <sup>3</sup> )
$\theta$	Primary nozzle tilt angle
$\phi$	Primary nozzle rotation angle
$\psi$	Nozzle base plate rotation angle
$\beta$	Ratio of ASME long radius metering nozzle throat diameter to inlet diameter

#### Subscripts

0	Section within secondary air plenum
1	Section at primary nozzle exit
2	Section at mixing stack exit
f	Film or wall cooling
m	Mixed flow or mixing stack
or	Orifice

p	Primary
s	Secondary
t	Tertiary (Cooling)
u	Uptake
w	Mixing stack inside wall

#### Computer Tabulated Data

DPOR	Pressure differential across the orifice (in. H <sub>2</sub> O)
POR	Static pressure at the orifice (in. H <sub>2</sub> O)
PSEC	Static pressure at the mixing stack entrance (in. H <sub>2</sub> O)
PTER	Static pressure in the tertiary air plenum (in. H <sub>2</sub> O)
PUPT	Static pressure in the uptake (in. H <sub>2</sub> O)
TAMB	Ambient air temperature (°F)
TOR	Air temperature at the orifice (°F)
TUPT	Temperature of air in the uptake (°F)
UM	Average velocity in the mixing stack (ft/sec)
UP	Primary flow velocity at primary nozzle
UUPT	Primary flow velocity in uptake (ft/sec)
UPT MACH	Uptake Mach number
UE	Average velocity at the mixing stack exit (ft/sec)
WM	Mass flow rate from mixing stack (lbm/sec)
WP	Mass flow from primary nozzles (lbm/sec)
WS	SEcondary mass flow rate (lbm/sec)
WT	Tertiary mass flow rate (lbm/sec)

### ACKNOWLEDGEMENT

The author wishes to express his sincere appreciation to those individuals who conducted past research on the multiple nozzle gas eductor systems at the Naval Postgraduate School. Your efforts and professionalism were of great benefit while conducting the present research. I hope I have maintained the exacting standards you instituted and that the present results prove as helpful to future research as yours did for this investigation.

I would like to further express sincere appreciation to Professor Paul Pucci, the thesis advisor, for his many hours of assistance, guidance, and moral support, as well as to the personnel in the Mechanical Engineering Machine and Electrical Shops for their timely support and suggestions.

To my family, I am grateful for your constant support and understanding.



## I. INTRODUCTION

Gas turbine applications in marine propulsion and in auxiliary systems have increased dramatically over the last decade. Their high horsepower to specific weight, increasingly competitive specific fuel consumption, and lower watchstander and maintenance requirements have made them extremely attractive for advanced marine designs such as hydrofoil, planing hulls, SWATH, and SES as well as more conventional monohull vessels. Consequently, special considerations must be given to the applications of gas turbines due to their particular air breathing and exhausting characteristics.

### A. NATURE OF THE PROBLEM

Gas turbines require large amounts of cooling air in addition to the quantity needed for combustion, therefore air-fuel ratios are generally three to five times those of conventional steam and diesel power plants of comparable size. The exhaust gases are also roughly twice as hot as for these conventional power plants. In general, gas turbine power plants produce considerably larger volumes of higher temperature exhaust or stack gases. These exhaust gases contribute to greater thermal and corrosive damage in the electrical equipment located on masts near the exhaust stream, hot gas corrosion of masts and superstructures in the hot gas wake, possible aircraft control problems for helicopter

operation in or near the exhaust stream, and a significantly greater infrared radiation signature due to both the high volumetric and temperature exhaust plumes as well as the hotter external surfaces on the exhaust stacks.

#### B. POSSIBLE SOLUTIONS

The volume and temperatures of exhaust gases are fairly well fixed by gas turbine size, power loading, and current gas turbine technology; consequently, other means must be employed to counter the problems associated with gas turbine systems.

Waste heat boilers or heat exchangers do reduce the exhaust gas temperatures and offer increased economy by recovering thermal energy which would otherwise be lost to the atmosphere. Unfortunately, such systems require considerable space and tend to generate back pressures which lower gas turbine performance. Fouling is also an ever present problem. Waste heat boilers have been tried on auxiliary power systems with limited success and research is still underway in this area.

Water injection systems are another possible solution. They are active systems which require moving parts, injection metering and control equipment, and large amounts of water. Costs and maintenance thus become problems.

One of the most promising systems for combatting the overall problem is the gas eductor. By using properly dimensioned primary flow nozzles for the exhaust gases and mixing stacks, secondary or ambient air is induced. The turbulent mixing

reduces the overall exhaust temperatures, back pressures are minimized when compared with other systems, and resultant negative pressures along the mixing stack walls can be utilized to further induce a tertiary ambient cooling flow through ports in the mixing stack. If the mixing stack is then shrouded, this tertiary flow creates a film cooled outer stack while adding additional thermal mixing of the exhaust gases. The straight, unshrouded mixing stack system is presently in operation on several naval vessels. An additional positive feature of gas eductor systems is that they can be used in conjunction with either of the other two possible solutions with minor modifications.

#### C. GAS EDUCTOR RESEARCH AT THE NAVAL POSTGRADUATE SCHOOL

This thesis is a further extension of research conducted by Ellin [Ref. 1], Moss [Ref. 2], Lemke and Staehli [Ref. 3], Shaw [Ref. 4], and Ryan [Ref. 5] on the cold flow eductor model testing facility. Hill's research [Ref. 6] on the hot flow eductor model testing facility should also be mentioned as it verified that cold flow modeling procedures correlated extremely well with actual hot flow data on geometrically similar eductor configurations. This correlation allows utilization of the more time and cost effective cold flow facility to develop optimum designs and configurations which can then be verified with actual hot flow testing.

Ellin initiated the early work by constructing an eductor model testing facility consisting of an uptake, centrifugal

compressor, primary flow nozzle section, mixing stack, and a means to control and measure the primary and secondary air flows. See Figures 1 and 2 for the general test model layout. The primary air flow in the test facility represents the gas turbine's hot exhaust gases. The secondary air flow is ambient air induced into the mixing stack by the primary air flow and gas eductor concept. From Ellin's study of multiple vice single nozzle flow systems, it was determined that four primary flow nozzles were preferable to either three or five nozzle systems. Ellin also determined that the nozzle length had little if any effect on the overall performance of the gas eductor system. He then verified the independence of the one-dimensional gas eductor modelling correlation parameters used on the flow rate or Mach number. His research showed that one-dimensional analysis provided good correlation of data for Mach numbers from 50 to 145 percent of the design Mach number of 0.064.

Moss's research initially consisted of reverification of the one-dimensional analysis. Moss then explored the effects of the stand-off distance, which is the distance from the primary nozzle exit plane to the entrance plane on the mixing stack. For non-dimensional analysis, the stand-off distance is divided by the mixing stack diameter to give the S/D ratio. Moss determined that eductor pumping was maximized when the stand-off distance was one-half the mixing stack diameter ( $S/D = 0.5$ ). An independent investigation conducted by

Harrell [Ref. 7] confirmed Moss's results. Moss then explored the effects of adding a conical transition piece to the entrance of the mixing stack to enhance eductor pumping. Experiments showed that the entrance transition piece actually slightly degraded overall performance.

Lemke and Staehli investigated overall eductor system's performance for different geometric configurations of the mixing stack and for different area ratios of the primary nozzles. The area ratio for nozzles is defined as the cross sectional area of the mixing stack divided by the total cross sectional area of the primary nozzles. Their work showed that decreasing the nozzle area ratio from 3.0 to 2.5 decreased the back pressures but also decreased the eductor's pumping coefficient. Lemke and Staehli then investigated the effects of adding a solid diffuser, a two ring diffuser, and a three-ring diffuser to the exit region of the mixing stack. These tests showed a decrease in uptake back pressure and an improvement in the eductor's pumping capacity. They then added slotted ports to the mixing stack to induce tertiary air. Their results showed significant air flow occurred through the ports. A shroud was then added, and tests showed that the shroud did not degrade either the pumping or mixing characteristics of the eductor but that it did provide an effective thermal shield around the mixing stack. Their final configuration was a ported mixing stack with a shroud and ring diffusers at the exit. The 3.0 area ratio nozzles and a standoff ratio of 0.5

were used in several of their investigations with mixing stack length to diameter ratios of 2.5 and 3.0.

The object of this thesis is directed toward reducing the length of the mixing stack by investigating the effects of angled primary flow nozzles on a four-nozzle gas eductor system. The results of investigations by Moss and Lemke and Staehli on the longer L/D ratios of 3.0 and 2.5 thus serve as a data base for comparing the effects of both straight and angled primary flow nozzles on the shorter mixing stack L/D ratios of 1.75, 1.5, and 1.25 used in this investigation.

#### D. EVALUATION OF GAS EDUCTOR SYSTEM PERFORMANCE

Evaluation of the gas eductor system performance is measured in the following areas: the amount of secondary air flow induced by the primary air flow; the amount of tertiary air flow induced; the degree of mixing of the primary and induced flows within the mixing stack; the amount of uptake back pressure impressed upon the gas turbine exhaust by the eductor system; and the amount of wall cooling air available to reduce the exterior stack temperatures. Because of the angled primary flow nozzles, several new parameters were defined to assist in evaluating the gas eductor system's performance. The new parameters include the primary nozzle tilt angle, primary nozzle rotation angle, and the nozzle base plate rotation angle. These parameters will be discussed in further sections of this report.

## II. MAJOR DIMENSIONLESS PARAMETERS

This investigation is an extension of earlier work conducted by Ellin, Moss, and Lemke and Staehli [Ref. 1,2,3] and utilizes the same one-dimensional analysis technique to model the gas eductor system. The more detailed analysis is given in Appendix A. In conducting this analysis, four major dimensionless parameters are used. The first three are used to evaluate the eductor's pumping performance, and the last is used to evaluate the static pressure distribution along the length of the mixing stack. The four major dimensionless parameters are:

$$P^* = \frac{\frac{P_a - P_{os}}{\rho_s}}{\frac{U_p^2}{2g_c}}$$

a pressure coefficient which compares the pumped head,  $(P_a - P_{os})/\rho_s$ , to the driving head,  $U_p^2/2g_c$ , of the primary flow

$$W^* = \frac{W_s}{W_p}$$

a flow rate ratio of secondary to primary mass flow rates

$$T^* = \frac{T_s}{T_p}$$

an absolute temperature ratio of secondary to primary air temperatures

$$PMS^* = \frac{\frac{PMS}{\rho_s}}{\frac{U_p^2}{2g_c}}$$

a pressure coefficient which compares the pumped head,  $PMS/\rho_s$ , to the driving head,  $U_p^2/2g_c$ , where PMS is the static pressure along the mixing stack.

### III. EXPERIMENTAL CORRELATION

For the geometries and flow rates investigated, it was confirmed by Ellin and Moss [Ref. 1 and 2] that a satisfactory correlation of the variables  $P^*$ ,  $T^*$ , and  $W^*$  takes the form

$$\frac{P^*}{T^*} = f(W^*T^{*n}) \quad (1)$$

where the exponent 'n' was determined to be equal to 0.44. The details of the determination of  $n \approx 0.44$  as the correlating exponent for the geometric parameters of the gas eductor model being tested is given in Reference [1]. To obtain a gas eductor model's pumping characteristic curve, the experimental data is correlated and analyzed by using equation (1), that is,  $P^*/T^*$  is plotted as a function of  $W^*T^{*0.44}$ . This correlation is used to predict the open-to-the-environment operating point for the gas eductor model. Variations in the model's geometry will change the pumping ability, which can be evaluated by the plot of equation (1). For ease of discussion,  $W^*T^{*0.44}$  will be referred to as the pumping coefficient in this report. Similarly,  $WT^{*TT^{*0.44}}$  will be referred to as the film cooling or tertiary pumping coefficient.



#### IV. MODEL GEOMETRIES

The four-nozzle gas eductor system investigated in this report made use of a single primary flow uptake, a single cluster of four primary flow angled nozzles held in a rotatable base plate, and a straight, unshrouded, unported mixing stack without diffuser rings at the mixing stack exit.

##### A. MIXING STACK CONFIGURATION AND GEOMETRIES

The primary thrust of this research was to study the effects of angled nozzles on the performance of shorter mixing stacks. Three short mixing stacks were manufactured from nominally 12 inch OD and 11.7 inch ID PVC agriculture water irrigation pipe. The mixing stacks were constructed with L/D ratios of 1.75, 1.5, and 1.25. The L/D ratio of 1.75 was chosen as a starting point since baseline data was available for the primary nozzle area ratio of 2.5 from Lemke and Staehlis research [Ref. 3]. Their major research was concerned with longer mixing stacks with L/D ratios of 2.5 and 3.0, which could also be used to compare with the shorter mixing stacks. Pressure taps were installed in the shorter mixing stacks at 0.25 X/D increments (2.93 inch spacing) to provide more data points for evaluating the mixing stack pressure distribution. 0.5 X/D spacing had been used on the longer mixing stacks. The dimensions for the three mixing stacks are provided in

Figure 6, and pictures of the mixing stack can be found in Figures 8 and 9.

#### B. ANGLED PRIMARY FLOW NOZZLE CONFIGURATION AND GEOMETRIES

The angled nozzle concept was chosen as the starting point for reducing the overall length of the mixing stacks by enhancing the mixing process. The nozzles were to have a constant cross section while having the ability to be inclined and rotated about a centerline axis. Several new parameters were defined for designing, manufacturing, and measuring the angled nozzles. The first parameter is the nozzle tilt angle,  $\theta$ , which is the cant angle measured from the centerline of a straight nozzle to the centerline of an angled nozzle. The nozzle rotation angle,  $\phi$ , is the angle that the nozzle is rotated inward toward the mixing stack centerline from a perpendicular to a radial line from the base plate center to the center of the nozzle. It is difficult to picture these definitions, and Figures 10 and 13 provide a clearer visualization for the nozzle configurations.

Several concepts were explored while attempting to design an easily manufactured and measurable angled nozzle. The most practical solution was to take a section of straight piping, cut it in two sections on a line mitered one half of the overall tilt angle desired, rotating the two sections 180 degrees, and then joining them together for the final tilt angle. The nozzles used in actual testing were manufactured from clear, cast acrylic pipe with a nominal 4.0 inch OD and

3.625 inch ID which had to be machined to 3.7 inches ID to give a nozzle area ratio of 2.5 for the four nozzles in each group. The nozzles were also machined 0.5 inches up from the base to properly mate with the recesses in the nozzle base plate. The edges where the two nozzle sections were joined were faired in to reduce abrupt flow direction changes both inside and outside the individual nozzles. Four nozzles for each configuration were constructed for nozzle tilt angles of 10 degrees, 15 degrees, 20 degrees, and 22.5 degrees as well as a set of straight nozzles for baseline data and mixing stack alignment purposes. The angled nozzles were dimensioned so that the intersection of their centerline and exit plane corresponded with the length of the straight nozzles used by Ellin, Moss, and Lemke and Staehli, thus establishing a common measurement for the standoff distance. This allowed alignment of the nozzles and mixing stack and setting the S/D ratio with the straight nozzles and not having to completely realign the system everytime the angled nozzles were changed. The nozzles and base plate were constructed of similar material with tight tolerances where they mated together. Thermal expansion was essentially equal for both components, and the friction provided was sufficient for holding the nozzles in place while allowing rotation angle changes. This feature allowed deletion of O-rings for seals and some form of mechanical locking device. The angled nozzle geometries are given in Figure 10, and photographs of the nozzles are found in Figures 11, 12, and 16.

### C. NOZZLE BASE PLATE CONFIGURATION AND GEOMETRIES

The nozzle base plate was constructed from acrylic plexiglass flat stock. Four recess holes were machined to accept the nozzles, and they were in turn machined to a 0.5 inch radius on the underside to present a smooth flow entrance region for the nozzles. The outer edge of the base plate was machined so that the whole base plate fit inside a matching aluminum base ring. The construction was such that the base plate could be rotated within the ring, primary flow pressure kept the two concentric surfaces mated which eliminated seals, and the base plate could not be ejected from the uptake by the considerable dynamic pressures associated with the high velocity primary air flow. Four symmetrically located locking cams allowed the base plate and installed nozzles to be locked in place. This was required for alignment procedures and prevent rotation during initial start-up. Once the system was warmed up to operating conditions, the difference between thermal expansion factors for the ring and base plate allowed sufficient expansion to make the use of the locking cams unnecessary. In fact, rotation of the base plate could be difficult when the system was fully warmed up, and a dry teflon lubricant was used to help overcome this problem.

A third new parameter was need for the base plate's ability to be rotated. The base plate rotation angle,  $\psi$ , is hereby defined as the angle of base plate rotation measured from the 90 degree point on the uptake transition piece as

depicted in Figure 13. This parameter serves to give a general indication of the flow directions within the mixing stack due to the angled nozzles. The base plate's geometry and dimensions are given in Figure 14, and photographs can be seen in Figures 15 and 16.

## V. EXPERIMENTAL FACILITY

Air is supplied to the primary nozzles by means of a centrifugal compressor and associated ducting schematically illustrated in Figure 1. The mixing stack configuration being tested is placed inside an air plenum containing an airtight partition so that two separate air flows, secondary and tertiary, may be measured. The air plenum facilitates the accurate measurement of secondary and tertiary air flows by using ASME long radius flow nozzles.

### A. PRIMARY AIR SYSTEM

The circled numbers found in this section refer to locations on Figure 1. The primary air ducting is constructed of 16-gage steel with 0.635 cm (0.25 in) thick steel flanges. The ducting sections were assembled using 0.635 cm (0.25 in) bolts with air drying silicone rubber seals between the flanges of adjacent sections. Entrance to the inlet ducting (1) is from the exterior of the building through a 91.44 cm (3.0 ft) square to a 30.48 cm (1.0 ft) square reducer, each side of which has the curvature of a quarter ellipse. A transition section (2) then changes the 30.48 cm (1.0 ft) square section to a 35.31 cm (13.90 in) diameter circular section (3). This circular section runs approximately 9.14 m (30 ft) to the centrifugal compressor inlet.

A standard ASME square edged orifice (4) is located 15 diameters downstream of the entrance reducer and 11 diameters upstream of the centrifugal compressor inlet, thus insuring stability of flow at both the orifice and compressor inlet. Piezometer rings (5) are located one diameter upstream and one-half diameter downstream of the orifice. The duct section also contains a thermocouple just downstream of the orifice. Primary flow is measured by means of the standard ASME square edged orifice designed to the specifications given in the ASME power test code [Ref. 8]. The 17.55 cm (6.902 in) diameter orifice used was constructed out of 304 stainless steel 0.635 cm (0.25 in) thick. The inside diameter of the duct at the orifice is 35.31 cm (13.90 in) which yields a beta ( $\beta = d/D$ ) of 0.497. The orifice diameter was chosen to give the best performance in regard to pressure drop and pressure loss across the orifice for the primary air flow rate used (1.71 Kg/sec (3.77 lbm/sec)).

The centrifugal compressor (7) used to provide primary air to the system is a Spencer Turbo Compressor, catalogue number 25100-H, rated at 6000 cfm at 2.5 psi back pressure. The compressor is driven by a three phase, 440 volt, 100 horsepower motor.

A manually operated sliding plate variable orifice (6) was designed to constrict the flow symmetrically and facilitate fine control of the primary air flow. During operation, the butterfly valve (8), located at the compressor's

discharge, provided adequate regulation of primary air flow, eliminating the necessity of using the sliding plate valve. The sliding plate valve was positioned in the wide-open position for all data runs.

On the compressor discharge side, immediately downstream of the butterfly valve, is a round to square transition (9) followed by a 90 degree elbow (10) and a straight section duct (11). All ducting to this point is considered part of the fixed primary air supply system. A transition section (12) is fitted to this last square section which reduces the duct cross section to a circular section 29.72 cm (11.17 in) in diameter. This circular ducting tapers down to a diameter of 26.30 cm (11.5 in) to provide the primary air inlet to the eductor system being tested. The transition is located far enough upstream of the model to insure that the flow reaching the model is fully developed.

#### B. SECONDARY AIR PLENUM

The secondary air plenum, shown in Figures 1, 2, and 3, is constructed of 1.905 cm (0.75 in) plywood and measures 1.22 m by 1.22 m by 1.88 m (4. ft by 4 ft by 6.17 ft). It serves as an enclosure that can contain all or only part of the eductor model and still allow the exit plane of the mixing stack to protrude. The purpose of the secondary air plenum is to serve as a boundary through which secondary air for the eductor system must flow. Long radius ASME flow nozzles,



designed in accordance with ASME power test codes [Ref. 8] and constructed of fiberglass, penetrate the secondary air plenum, thereby providing the sole means for metering the secondary air reaching the eductor as shown in Figures 1 through 4. Appendix D of reference [1] outlines the design and construction of the secondary air flow nozzles. By measuring the temperature of the air entering and the pressure differential across the ASME flow nozzles, the mass flow rate of secondary air can be determined. Flexibility is provided in measurement of the mass flow rate of secondary air by employing flow nozzles with three different throat diameters: 20.32 cm (8 in), 10.16 cm (4 in), and 5.08 cm (2 in). By using a combination of flow nozzles, a wide variety of secondary cross sectional areas can be obtained.

A secondary air flow straightener, shown in Figures 1, 2, and 4, consisting of a double screen is installed 1.22 m (4 ft) from the open end of the secondary air plenum, between the ASME long radius nozzles and the primary air flow nozzles. The purpose of the straightener is to reduce any swirl effect that could result when only a small secondary air flow area exists.

#### C. TERTIARY AIR PLENUM

The tertiary air plenum, shown in Figures 1, 2, 8 and 9, is constructed of 1.90 cm (0.75 in) plywood and measure 1.22 m by 1.22 m by 1.22 m (4 ft by 4 ft by 4 ft). It serves as an enclosure that completely surrounds the mixing stack and allows

the exit and entrance regions to protrude. An airtight rubber diaphragm type seal, schematically illustrated in Figure 2, is located at each end of the enclosure. This allows measurement of a tertiary air flow independent of the secondary air flow. Tertiary air flow is measured with the use of long radius ASME flow nozzles designed in accordance with ASME test codes [ Ref. 8 ] and constructed of fiberglass. These nozzles are located so that they penetrate the airtight tertiary air plenum, thereby providing the sole means for metering the tertiary air reaching the eductor. By measuring the temperature of the air entering and the pressure differential across the ASME flow nozzles, the mass flow rate of tertiary air can easily be obtained. Flexibility in measuring the tertiary flow is provided by employing different size flow nozzles: two of 20.32 cm (8 in) throat diameter, three of 10.16 cm (4 in) throat diameter, and two of 5.08 cm (2 in) throat diameter. By using various combinations of these flow nozzles, a wide variety of tertiary cross section flow areas can be obtained.

The interior of the tertiary air plenum is pictured in Figures 8 and 9. The stand which holds the mixing stack can be seen mounted inside the plenum.

#### D. ALIGNMENT

The alignment of the mixing stack with the primary air flow nozzles is accomplished by using two round alignment plugs, a nozzle alignment plate, and a 0.75 inch OD steel

alignment bar. The two circular alignment plugs are inserted into opposite ends of the mixing stack, and the nozzle alignment plate is then carefully inserted over the straight nozzles. The steel alignment bar is then inserted through the centerline holes in the alignment plugs and brought up to the centerline hole in the nozzle alignment plate. The three axis mounting stand, pictured in Figure 8, is adjusted until the alignment bar can be fully inserted into the nozzle alignment plate and recess in the nozzle base plate without difficulty.

#### E. INSTRUMENTATION

Pressure taps for measuring gage pressures are located inside the primary air uptakes just prior to the primary nozzles, inside the secondary air plenum, inside the tertiary air plenum, and at various points on the model. A variety of manometers, pictured in Figure 18, were used to indicate the pressure differentials. A schematic representation of the pressure measuring instrumentation is illustrated in Figures 17 and 19. Monitoring of each of the various pressures was facilitated by the use of a scanivalve and a multiple valve manifold. The scanivalve was used to select the pressure tap to be read, while the multiple valve manifold allowed selection of the optimum manometer for the pressure being recorded. A vent was included in the multiple valve manifold which provided a means of venting the manometers between pressure readings. When taking readings of the pressure distribution in the mixing stack, it was necessary to manually change the

tubing from one end of the manometer to the other in order to get the positive pressure readings. The valve manifold provided a selection of a 15.24 cm (6.0 in) inclined water manometer, a 5.08 cm (2.0 in) inclined water manometer, and a 1.27 cm (0.5 in) inclined oil manometer (specific gravity 0.827). In addition, the following dedicated manometers were used in the system: a 50.80 cm (20 in) single column water manometer connected to the primary air flow just prior to the primary nozzles, a 1.27 cm (50 in) U-tube water manometer with each leg connected to a piezometric ring on either side of the orifice plate in the air inlet duct, and a 2.55 cm (1.0 in) inclined water manometer connected to the upstream piezometric ring.

Primary air temperatures, measured at the orifice outlet and just prior to the primary nozzles, are measured with copper-constantan thermocouples. The thermocouples are in assemblies manufactured by Honeywell under the trade name Megapak. Polyvinyl covered 20 gage copper-constantan extension wire is used to connect the thermocouples to an Omega Digital Thermometer, Model Number 2176A, which provided a digital display of the measured temperatures in degrees Fahrenheit or Centigrade. Due to the longer data runs involved with this thesis, another thermocouple was added to measure the secondary/tertiary ambient air temperature to provide more timely data. The mercury-glass thermometer was retained for comparison purposes.

Velocity traverse profiles at the mixing stack exit plane are obtained by using a pitot tube mounted in a revised velocity traverse bar. The entire assembly was rebuilt to provide increased stability and support for the pitot tube which had to reach up to 30 inches into the tertiary plenum to record velocity profiles on the short,  $L/D = 1.25$  mixing stack. The tram bar was also equipped with a new distance measuring system to increase accuracy and lower data acquisition time. The pitot tube is used in conjunction with the 50.80 cm (20 in) single column water manometer vice the 6.0 inch inclined water manometer, mainly due to the higher pressures involved with the shorter mixing stacks and the greater pressure fluctuations. Threaded studs were used to locate the velocity traverse bar and pitot tube assembly for both the horizontal and diagonal velocity profiles. Four nuts kept the system in place and provided rapid changeover from one profile to the other. The assembly can be seen in Figure 8.

## VI. EXPERIMENTAL METHOD

Evaluation of the eductor model requires the experimental determination of pressure differentials across the ASME long radius flow nozzles, temperatures of primary and induced air flows, internal mixing stack pressure distributions, and mixing stack exit velocity profiles from pitot tube pressure readings. In addition, base plate rotation angles are used to get a general understanding of the flow patterns within the mixing stack. These experimentally determined quantities are then reduced with the aid of a computer to obtain pumping coefficients, induced air flow rates, pressure distributions and flow distributions in the mixing stack, and mixing stack velocity profiles at the exit plane of the mixing stack. The performance characteristics of the eductor due to the different nozzle geometric configurations are then evaluated graphically by use of computer generated plots. The plots also help to determine the model's relative effectiveness and problem areas which may not be apparent when reviewing raw and processed data.

The following sections address the individual performance criteria used to evaluate the eductor and nozzle combinations. Circled numbers refer to regions located on the representative plots used in the evaluation process.

#### A. PUMPING COEFFICIENT

The secondary pumping coefficient and the tertiary pumping coefficients provided a basis for analyzing the eductor's pumping capability. Nozzle combination changes alter the eductor's pumping performance, and the pumping coefficient is one of the major criteria for comparing various nozzles as well as any changes to the mixing stack such as shrouding, porting, diffuser rings, L/D ratios, and S/D ratios. The pumping coefficient(s) for the model should correspond to the coefficients for the shipboard gas eductor system. At the operating point, the eductor is exposed to no restrictions in the secondary or tertiary air flows. In the model, this is simulated by completely opening the air plenums to the environment. Unfortunately, at this condition, the secondary and/or tertiary air flow rates can not be measured. The eductor model's characteristics must then be established by extrapolating the measured pumping coefficients to the desired operating point.

The data for this extrapolation is established by varying the associated induced air flow rate, either secondary or tertiary, from zero to its maximum measurable rate. These rates are determined by sequentially opening the ASME flow nozzles mounted in the appropriate plenum and recording the pressure drop across the nozzles. Values for nozzle cross-section areas, pressure drops, induced flow air temperatures, and barometric pressures are then used to calculate the

dimensionless parameters  $P^*/T^*$  and  $W^*T^{0.44}$  as described in Appendix A. The dimensionless parameters are then plotted as illustrated in Figure 20. The data point (1) corresponds to closing all ASME flow nozzles. Data points in region (2) corresponds to opening most of the ASME flow nozzles and the final data point corresponds to opening all flow nozzles, plenum doors, or other plenum penetrations available. Early data runs attempted to gain more accuracy in this region by taking more data. Unfortunately, the pressure drop across the nozzles is so critical in this region that any error or fluctuations causes considerable data scatter. Such points were deleted from the finished plots contained in this thesis. In theory, there should be no pressure inside the plenum at the operating point except for ambient pressure. In reality there is always some small negative pressure present. The data points in region (3) provide the most consistent and accurate data. Extrapolation of the pumping characteristics curve to intersect the zero  $P^*/T^*$  or  $PT^*/T^*$  abscissa locates the appropriate operating point for the eductor model configuration.

#### B. INDUCED AIR FLOWS

Secondary and tertiary air flows are induced flows. In this thesis, only the secondary air flow was of concern although both flows were written into the documentation and computer programs.



The secondary air flow is the amount of air induced by the primary nozzles which is mixed within the mixing stack with primary air to reduce the exhaust gas temperature.

#### C. PRESSURE DISTRIBUTION IN THE MIXING STACK

The axial pressure distribution in the mixing stack is obtained by taking static pressure reading from pressure taps attached to the stack in two rows. In the cold flow test facility, the mixing stack is located horizontally in the tertiary plenum. The first row is located on the top of the mixing stack, and the second row is offset 45 degrees from the first row as shown in Figures 6 and 7. The pressure taps were located 0.25 mixing stack diameters apart. Actual locations are given in Figure 6. The dimensionless mixing stack pressure term,  $PMS^*$ , as previously mentioned in Section II and as derived in Appendix A, is then calculated from the static pressure data.  $PMS^*$  is plotted versus  $X/D$  pressure tap locations to obtain the mixing stack pressure distribution. A sample distribution is shown in Figure 21. Region (1) is located at the entrance of the mixing stack, and it has the highest negative pressure readings for each stack. The early tests confirmed that there were definite limits on the amount of nozzle tilt and rotation before the primary flow started to interfere with the secondary flow in this region. Pressures near region (2), located toward the exit of the stack, tend to possess lower potential for inducing tertiary flow when compared to pressures near region (1). Pressures located

at region (3), located just prior to the exit of the mixing stack may actually be positive, or above ambient pressure. In the sample plot, the data point at region (2) has very little potential for inducing tertiary flow, and the data point at region (3) is positive which would hinder tertiary flow. It is therefore desirable to look for nozzles combinations which produce pressure distributions remaining below the zero PMS\* line on the plot and as low down on the PMS\* axis as possible.

#### D. MIXING STACK ROTATION ANGLE

The straight nozzles produce a symmetric flow consisting of four peak and four null pressure areas along the axis of the mixing stack. Pressure taps at position 'A' normally could be used to record the peaks while the position 'B' taps could be used to record the lower pressure regions or nulls. With introduction of the angled nozzles, the flow became swirled. A rotatable base plate was used to scan the entire circumference of the mixing stack at each L/D position and thereby obtain a better record of the varying axial pressure distribution. This allowed the peaks and troughs to be rotated to the stationary pressure taps for data acquisition. The base plate rotation angle,  $\psi$ , is recorded for each pressure tap position, and when plotted, provides a rough indication of the flow pattern variations. Region (1) in Figure 22 corresponds to the rotation angle needed to align the peak position 'A' reading with the pressure tap and is always the

actual angle recorded. The other data points were actually rotated 90 degrees for plotting purposes. The data in Figure 22 is fairly stable and indicates little twisting of the primary flow. Region (2) often showed a considerable change in flow direction as did region (3). Again, the plots of this data only serves as a general indication of flow directions, which were in agreement with observations of tufts of string used to follow the flow paths on each run.

Tests were conducted early in the research to determine the sensitivity of the rotation angles. Results showed that changes as small as one degree of rotation could cause large pressure changes while at other times the base plate could be rotated 30 degrees without any pressure changes.

#### E. VELOCITY TRAVERSES

The velocity traverses are generated by moving the pitot tube in measured increments across the horizontal and diagonal lines as indicated in Figure 7. Stagnation pressure readings are read from the 20 inch manometer and combined with data taken for the pumping coefficients to calculate mixing stack exit velocities in units of feet/second. Computer generated two-dimensional plots of the velocity traverses can then be used to get indications of mixing, wall effects, and primary flow core formation.

The sample horizontal velocity profile shown in Figure 23 shows two, essentially primary flow peaks at regions (2) and (4). Regions (1) and (5) are essentially secondary

induced flows and show some wall efforts. Region (3) should be symmetrically located at the center of the stack, however misalignment of the base plate may cause the center trough to appear displaced. Region (6) should have data points which overlap data points on the diagonal velocity plot.

The sample diagonal velocity profile shown in Figure 24 shows noticeable peaks and troughs. The peaks at regions (1) and (7) are the primary nozzle flows which have not been rotated inward enough to get better mixing. The peaks at (3) and (5) correspond to peaks (2) and (4) on the horizontal velocity profile. Region (4) should be at the same point as region (3) in the horizontal profile, and serves as a quick indication of rotation angle misalignment. Region (8) data points should be the same as those in the other profile. This region also is observed for coring effects when the nozzles have excessive tilt and rotation.

The dashed lines in both sample profiles are just rough indications of what a fully developed turbulent flow should look like. With the short mixing stacks, this will never be achieved, but the goal is to select nozzle combinations which can give generally flat overall profiles as an indication of enhanced mixing. Sharp peaks and troughs should therefore be avoided or minimized. The comparison plots of the two profiles serves to determine data accuracy, the interaction of the flows, and base plate misalignment which can seriously skew the profiles.

Due to the flow rotation created by the angled primary nozzles, the nozzles base plate had to be rotated on a trial-and-error basis to bring the primary flows into alignment with the pitot tube for the diagonal velocity traverse profile. This setting of the nozzle base plate was kept intact for the horizontal velocity profile. Alignment procedures called for obtaining a peak pressure reading on the diagonal traverse, adjusting the sliding scale on the velocity traverse bar and moving the bar until a symmetric profile was achieved, and then verifying the base plate rotation.

## VII. DISCUSSION OF EXPERIMENTAL RESULTS

Major components for the straight geometry mixing stacks were relocated, overhauled, and installed while the components and computer software for the angled primary flow nozzles were being developed. The data reduction process and basic cold flow test facility components were then verified by taking a series of tests with a set of straight nozzles used by Lemke and Staehli [Ref. 3]. This set of nozzles had inner diameters of 3.38 inches and an area ratio of 3.0. This early data is not presented in this report, but it correlated extremely well with Lemke and Staehli's results. These tests confirmed that higher pumping coefficients on the order of 0.75 could be obtained if you are willing to suffer the considerably higher, approximately 2.5 inches of water higher back pressure and higher nozzle exhaust velocities when compared to straight nozzles having an inner diameter of 3.70 inches and area ratio of 2.5 on the same mixing stack with an L/D ratio of 1.75. The test results for the 3.7 inch ID and AR = 2.5 straight nozzles on a mixing stack with L/D = 1.75 and S/D = 0.5 are given in Tables 2 through 2.3, and the plots are given in Figures 25 through 25.4. This data compared extremely well with Lemke and Staehli's results as listed in Table V.c of Reference [3] and is plotted in Figure 25. This data served as a baseline for evaluating the angled nozzles with the same L/D, S/D, and AR ratios for the early data runs.

The angled nozzle combinations in the remainder of this discussion will appear as 15/10 for example, where the 15 is the nozzle tilt angle,  $\theta$ , and the 10 is the nozzle rotation angle,  $\phi$ . Due to the large number of plots and tables involved, references to individual plots and tables for the various nozzle combinations will not normally be made except by references to the series of data for that particular combination. The notation FT 15/8, for example, will be used to indicate that the plots are located in the Figure 15 series and that the data is located in the Table 8 series for the nozzle combination specified. The summary tables, Tables 1.1, 1.2, and 1.3, and the summary plots given in Figures 75 through 81 may also prove to be of great value when reading this discussion. The mini-plots given with the tabulated data are also quite helpful when reviewing data. The abbreviations MSD for mixing stack pressure distribution, PCD for pumping coefficient, and VTD for velocity traverse distribution will also be used in this discussion and in the summary of tabulated data tables. Unless specifically mentioned otherwise, the S/D ratio of 0.5 was used throughout these investigations.

The first set of angled nozzles chosen for testing were the 15 degree tilt series. These nozzles were near the middle of the 10, 15, 20, and 22.5 degree tilt angle nozzles available, and it was hoped that by testing nozzles on either side of them that a trend would quickly develop which could possibly reduce the amount of testing necessary. The four sets of

angled nozzles could be rotated from zero to between 25 and 45 degrees depending on the amount of tilt angle involved. The rotation angles can be adjusted in one degree increments which made the number of nozzles combinations available for testing extremely large. This was further compounded by the requirement to test these combinations on three different L/D ratio mixing stacks. It was decided that rotation angles in 10 degree increments would be used to help alleviate the number of runs possible while still developing a thorough data base.

#### A. L/D = 1.75 (LONG STACK) RESULTS

Although the L/D = 1.75 mixing stack was the longest mixing stack tested, it is still approximately only two-thirds the L/D ratio of stacks involved in past research as well as those in actual use on several naval vessels. The 15/00 combination was tested first with results given in the FT 30/7 series. the pumping coefficient for the straight nozzles was 0.54 and the 15/00 nozzles increased this to 0.57. The MSD profile was worse and indicated a positive PMS\* pressure value near the L/D = 1.5 pressure tap. The VTD profile showed that the primary flow was predominant along the walls for the diagonal profile while the horizonatal profile was nice and flat. Unfortunately, this first angled nozzle data run pointed out that it would take about 2.5 hours to get a complete set of acceptable data.



The PCD data was fairly easy to take, however, the angled nozzles had to be rotated with the base plate to get accurate MSD data. The alignment of the velocity profile traverse system to get the profiles centered was hard enough, but the base plate had to be rotated to the optimum position to get an unskewed profile. Consequently, there was a lot of trial-and-error adjustment required while taking the MSD and VTD data.

Tests were rerun on the 15/00 nozzles to determine if the base plate could be fixed at the zero point, rotated to the peak pressure at position 'A' and left there, or had to be rotated for both maximum and minimum pressure readings along the mixing stack. The results are given in the FT 31/8, FT 32/9, and FT 33/10 series. It was determined that the rotation angles served only as a general indication of flow directions and was not as important as the pressure readings along the stack. The results also showed that rotating the peak pressure to the top pressure taps gave fairly accurate minimum readings on the diagonal pressure taps without further rotation of the base plate. The next data run for the 15/10 nozzles showed that not only may one miss the minimum reading, one might miss any positive pressures as well when using this approach. Consequently, the MSD procedure that evolved was to rotate the base plate to get a maximum negative or positive pressure reading at the top pressure taps, record the reading and the rotation angle, rotate the base plate for a minimum reading on the diagonal taps, compare the two angles,

and record the average of the two. This did help reduce the run time down to two hours, and nothing was found to reduce the time involved obtaining the velocity profiles. The semi-automated data system in its present configuration would have actually increased the run times for the particular geometries associated with this research.

The next tests were conducted on the 15/10 and 15/20 nozzle combinations, and results are given in the FT 34/11 and FT 35/12 series. The pumping coefficients were both in the 0.59 range with the 15/20 nozzles being just slightly better. Both had similar MSD profiles with one slightly positive PMS\* reading near the stack exit. The 15/20 combination had the less positive PMS\* reading of these two nozzle combinations, and its VTD profile was also slightly better than the 15/10 combinations.

The 15/30 tests given in FT 39/16 showed a pumping coefficient of 0.55 which was lower than either of the 15/10 or 15/20 combinations. The MSD profile showed some improvement, but the positive PMS\* reading still existed in the same region. The diagonal VTD profile was excellent, but the horizontal profile showed onset of primary flow coring.

The next approach was to split the difference and try a 15/25 combination to see if there was a maximum pumping coefficient in the combination region. Results are given in FT 36/13 and the pumping coefficient fell to 0.58. The positive PMS\* reading was lower than in the 15/20 data, but the

VTD profiles were slightly worse for thermal mixing. This same nozzle combination was then used for testing S/D ratios of 0.4 and 0.25 to determine the effect of reducing the stand-off distance. Moss in Reference [2] had shown that the optimum S/D ratio for the straight primary nozzles was 0.5. Results are given in the FT 37/14 and FT 38/15 series. The S/D = 0.4 run showed a slightly better pumping coefficient of 0.585 when compared with the S/D = 0.5 pumping coefficient of 0.58. The positive PMS\* reading near the mixing stack exit was intermittently negative and finally stayed negative as the data run progressed. Unfortunately, the VTD profiles were poorer for the S/D = 0.4 ratio. The S/D = 0.25 pumping coefficient fell off to 0.55, the MSD profile was better than the other two S/D ratios, and the VTD profile was much worse than either the S/D = 0.5 or S/D = 0.4 profiles. In comparing the results, it was determined that the angled nozzles generally behaved as straight nozzles as far as stand-off distance ratios were concerned and the results followed the curve generated by Moss. Each change of the S/D ratio requires realignment of the mixing stack which can take a considerably amount of time, the results correlated with Moss's findings, and further comparison of S/D ratios for the two shorter mixing stacks was ruled out.

Full data runs were then conducted on 20/10 and 20/20 nozzle combinations with the results being given in the FT 40/17 and FT 41/18 series. Although they had pumping

coefficients below the 15/20 nozzle combination, they both exhibited improved VTD profiles. The MSD profiles both had more positive PMS\* readings and were generally poorer than for the 15/20 combination. The hoped for trend was becoming clear, however the data acquisition time for a full set of data on every nozzle combination would have precluded testing on the other two mixing stacks. It was felt that the angled nozzles did make shorter mixing stacks possible, but that the MSD profiles were substandard for the stack tested. Testing was needed on the shorter stacks to determine if the MSD profiles would be improved while maintaining or improving the pumping coefficients.

A careful review of evaluation procedures disclosed that all parameters have to be analyzed, but that the pumping coefficient was slightly predominant. The tests so far had shown that any amount of nozzle tilt and rotation improved the pumping coefficient over that of the straight nozzles. To establish a broader data base while still being able to test the shorter stacks, run times had to be reduced still further. It was decided to take partial data runs for pumping coefficient data over the remainder of the nozzles followed by full data runs on nozzle combinations with the better pumping coefficients.

The PCD data only procedure was then conducted on the 20/30 and all of the 10 degree and 22.5 degree tilt angle nozzles. The plots and tabulated data for these various combinations are provided in this report; however, the summary

of tabulated data in Tables 1.1 and 1.2 along with the summary plots in Figures 75 through 81 should be referred to for a clearer picture of the results. In general, it was found that the 10 degree tilt angle nozzles started off fairly well at low rotation angles, and the pumping coefficients then fell off dramatically as the rotation angle was increased. The 15 degree tilt angle nozzles started out with good pumping coefficients at low rotation angles, reached a peak around the 15/20 combination, and then fell off for higher rotation angles. The 20 degree tilt angle nozzles started below the other two, got better, and then stayed the same as the rotation angle was increased.

The 22.5 degree tilt angle nozzles started out the lowest for this L/D ratio and got better with increasing rotation angles. Partial tests showed that primary flow coring took effect with these nozzles with poorer mixing once you passed a rotation angle of about 25 to 30 degrees depending on the tilt angle being tested.

One interesting point became clear by taking just the PCD data to establish a broader data base, the results clearly showed that not all angled nozzle combinations give better pumping performance than the straight nozzles. Several in the 10/30 and 10/40 ranges would be considerably worse in this application.

#### B. L/D = 1.5 (MEDIUM STACK) RESULTS

The L/D ratio of 1.5 mixing stack was installed, aligned,

and tested. The straight nozzles were then tested with a full data run to establish a base line for the medium stack data results. The results are given in the FT 46/23 series. The pumping coefficient fell to 0.51 while the MSD and VTD profiles were essentially the same as those for the longer stack.

Partial data runs were conducted for the remainder of the angles nozzle combinations. The results are provided in the various figures and tables, but again, the summaries in Table 1.2 and in Figures 75 through 81 present a clearer picture of the overall results. The 15/20 nozzles again provided the best pumping coefficient, and a full data run was then conducted. The results are given in the FT 53/30 series. The pumping coefficient was slightly better than 0.58, which compared favorably with the 0.59 pumping coefficient for the same nozzles on the longer  $L/D = 1.75$  mixing stack. More importantly, the MSD profile improved considerably and there were no positive PMS\* readings. The VTD profiles showed more peaks and troughs than with the longer stack, but overall, they were generally flatter, indicating better mixing. These findings were extremely important as they verified that the pumping coefficient could be kept close to those associated with straight nozzles and considerably longer mixing stacks, achieve better mixing, and the improved MSD profile clearly indicated that the ported mixing stack with shroud and diffuser end rings was also feasible. The 15/20 angled nozzle combina-

combination, based on data up to this point, clearly appeared to be the best combination irregardless of the mixing stack length and provided the best overall performance on the medium length mixing stack.

#### C. $L/D = 1.25$ (SHORT STACK) RESULTS

The  $L/D$  mixing stack was installed and aligned. The straight nozzles were again tested with a full data run to establish a baseline for the short mixing stack. The results are given in the FT 60/37 series. The pumping coefficient fell even further to 0.50 when compared to the two longer mixing stacks. The MSD profile was good, but it was poorer than those for the other two stacks. The VTD profiles had more pronounced peaks and troughs which were higher than those of any other stack and nozzle combination tested, thus indicating extremely poor mixing within the mixing stack.

Partial data runs were conducted on the remainder of the angled nozzle combinations. The results are provided in the various figures and tables, but again, the summaries in Table 1.3 and Figures 75 through 81 presents a clearer picture of the results. The 15/20 nozzles, the previously best performers on the other two stacks, fell below the pumping coefficients of the 15/10, 20/10, and 20/30 nozzles.

Full data runs were then conducted on the 15/20 and 20/20 nozzle combinations to determine the effects of increasing the  $L/D$  ratio while holding the 15/20 nozzle combination

constant and the effects of increasing the rotation angle while holding the tilt angle constant for the short stack.

The 15/20 nozzle combination on the full run dropped from 0.57 to 0.56 with better data accuracy. The results are given in the FT 67/44 series. The MSD profile, while always negative, was generally not as good as on the  $L/D = 1.5$  mixing stack but better than on the long stack. The VTD profiles were better than the straight nozzles, but not quite as good as either of the longer mixing stacks.

The 20/20 nozzle combination had a pumping coefficient of 0.58 which was better than the 15/20 nozzles. The results of this run are given in the FT 71/48 series. The biggest difference between these two combinations was in the MSD profiles. The 20/20 nozzle combination had two positive PMS\* readings near the mixing stack exit as well as a poorer overall profile. There was some misalignment on the VTD profiles but in general, the horizontal profile was better than with the 15/20 nozzles while the diagonal profile was considerably worse with indications of some wall effects. Overall, the VTD profiles were about equal for mixing properties.

The 20/30 nozzles should have been slightly poorer performers than the 20/20 nozzles, and a full data run was not conducted. The next step would have been to conduct full data runs on the 15/10 nozzle combination; however, time expired for data acquisition and was needed to analyze data and write this report. This testing of the 15/10 nozzle combination would make an excellent starting point for the next research effort.



#### D. BACK PRESSURES

A review of the back pressure data from the various data tables showed that the better performing angled primary flow nozzles increased the back pressures on the average of 0.04 inches of water when compared to the straight nozzles on the same mixing stack. For example, the 15/20 nozzles on the  $L/D = 1.5$  mixing stack increased the back pressure only 0.02 inches of water for the test uptake Mach number of 0.062. Increasing the nozzle tilt angle about 20 degrees and the nozzle rotation angle above 25 degrees tended to raise the back pressures slightly, usually on the order of several tenths of inches of water. A firm correlation between the effects of increasing just one or both of the angles could not be obtained. For example, the 22.5/20 nozzles on the  $L/D = 1.25$  mixing stack showed 0.15 inches of water less back pressure than the 22.5/10 nozzles; however, they both were at least 0.35 inches of water greater than the straight nozzles.

The 15/20 nozzles with the  $L/D = 1.5$  mixing stack showed a back pressure of 6.30 inches of water for a test Mach number of 0.064. The straight nozzles used with the longer  $L/D = 2.5$  mixing stack were shown by Lemke and Staehli to have a back pressure of 5.8 inches of water, therefore the angled nozzles when used in the shorter mixing stacks do exhibit a slight increase in back pressure on the order of one-half inch of water.

### VIII. CONCLUSIONS

This research investigated the feasibility of reducing the length of the mixing stacks in gas turbine gas eductor systems by the use of angled primary flow nozzles. The conclusions resulting from this investigation are as follows:

1. The best combination of angled primary flow nozzles and mixing stacks tested appears to be the angled nozzles with an area ratio of 2.5, a tilt angle of 15 degrees, and a rotation of 20 degrees used in a mixing stack with an L/D ratio of 1.5 and an S/D ratio of 0.5. This combination provides a pumping coefficient of 0.58, which is equal to that reported by Lemke and Staehli for straight nozzles with the same area ratio used in a mixing stack with an L/D ratio of 2.5 and S/D ratio of 0.5. The best combination of angled nozzles and mixing stack, when further compared to this longer mixing stack, showed comparable mixing stack pressure distributions, a slight increase in back pressure of 0.50 inches of water, and improved mixing.
2. The family of 15 degree tilt angled primary flow nozzles provides the best overall eductor performance when evaluated by all parameters on the mixing stacks investigated. Not all angled nozzles tested gave

improved performance over straight primary flow nozzles for the same AR, L/D, and S/D ratios. Some of the angled primary flow nozzles which do give good pumping capacity provide poor mixing and/or mixing stack pressure distributions. The best combination of angled primary flow nozzles and mixing stack previously listed shows strong potential for further application of the shrouded, ported, and diffuser ring equipped mixing stack concept.

3. The S/D ratio of 0.5 appears to be the preferred overall location of the mixing stack from the primary flow nozzles. The angled nozzles appear to behave in this respect much like straight nozzles, and follow the general behavior obtained by Moss for varying the stand-off ratios.
4. Back pressure increases associated with the angled primary flow nozzles are insignificant when compared with straight nozzles used with the same L/D ratio mixing stacks, provided that the nozzle tilt angle is kept below approximately 20 degrees and the nozzle rotation is kept below approximately 25 degrees.

## IX. RECOMMENDATIONS FOR FURTHER STUDY

Based upon a review of this investigation and its findings, it is recommended that further study be conducted in the following areas:

1. Full data runs be conducted for the 15/10 nozzle combinations on the  $L/D = 1.25$  and  $L/D = 1.5$  mixing stacks to establish a more complete data base for the 15 degree tilt angle nozzles.
2. More verification of S/D ratio effects at 10/20 and 15/20 nozzle combinations on the above  $L/D$  ratio mixing stacks.
3. Investigate the application of angled primary flow nozzles on ported, shrouded, and diffuser ring equipped short mixing stacks to further enhance short mixing stack performance.
4. Investigate alternate nozzle cross sections, such as the fluted nozzle, to further enhance the mixing process in short mixing stacks. This research could also later be applied to the ported, shrouded, and diffuser ring equipped short stacks.
5. Hot flow verification of cold flow findings should be conducted once the above recommendations have established the better performing geometries and configurations for short mixing stack and gas eductor enhancement in gas turbine applications.

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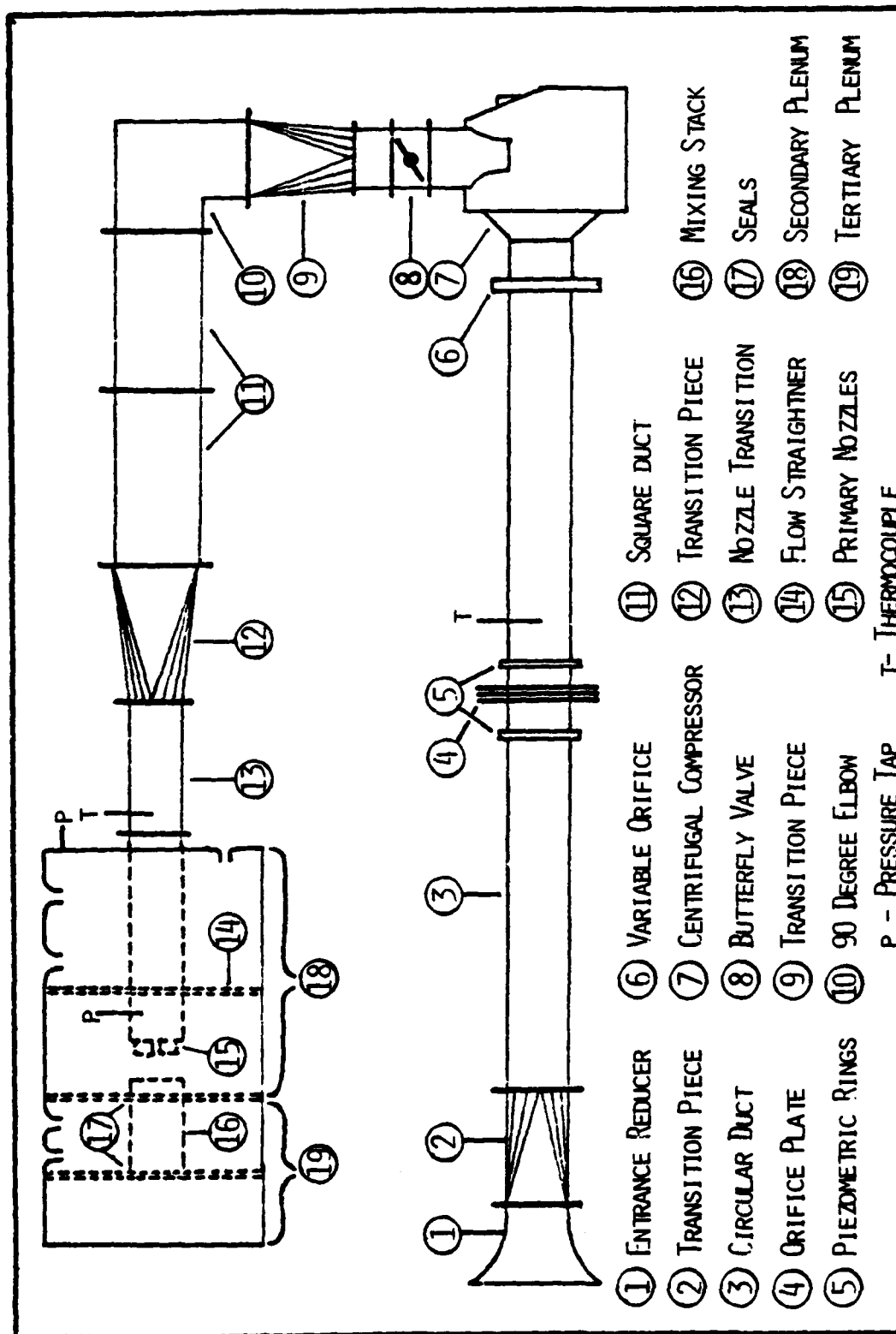


FIGURE 1 - EDUCTOR MODEL TESTING FACILITY

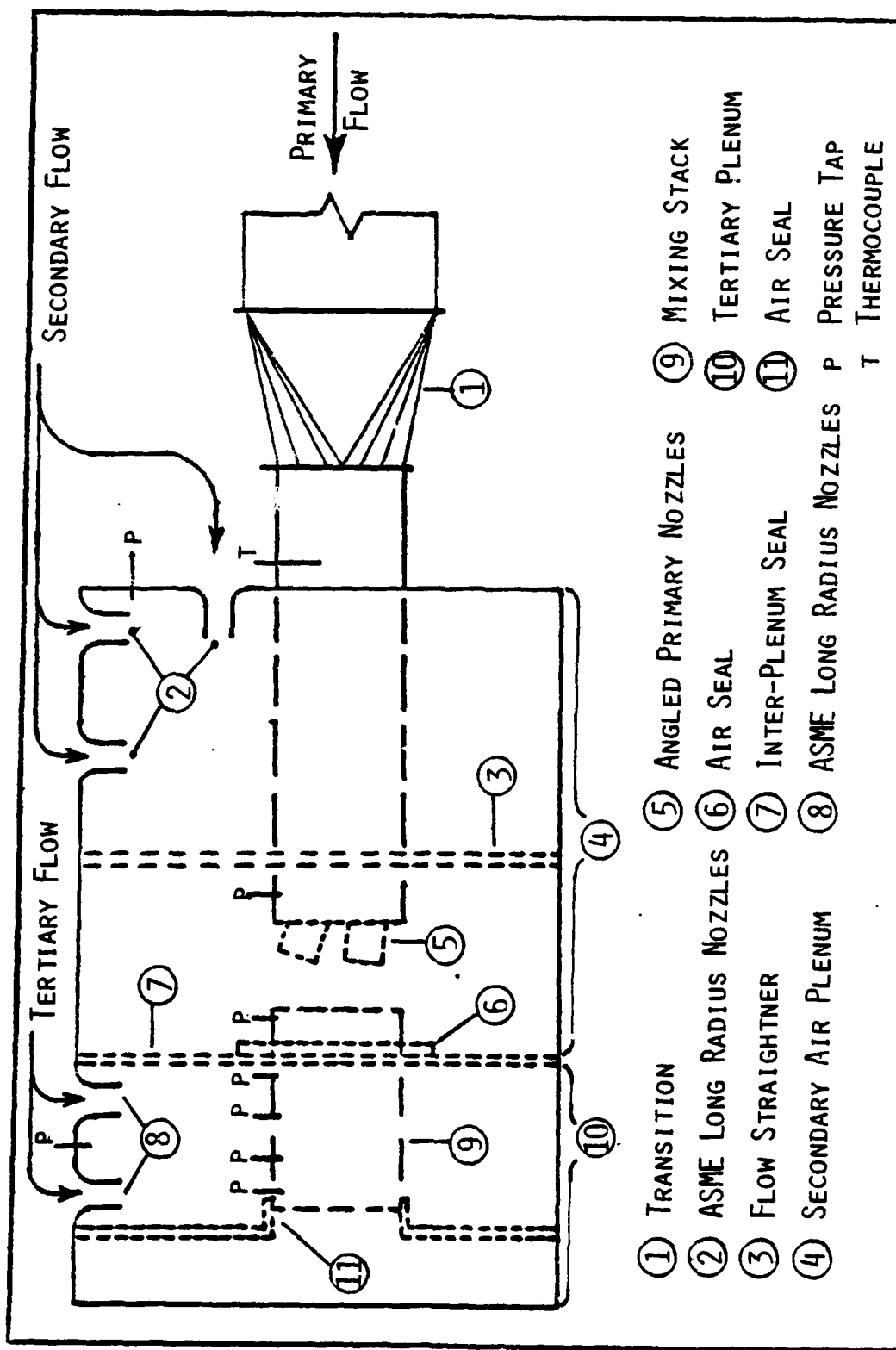


FIGURE 2 - GAS EDUCTOR MODEL TEST FACILITY WITH SECONDARY AND TERTIARY PLENUMS

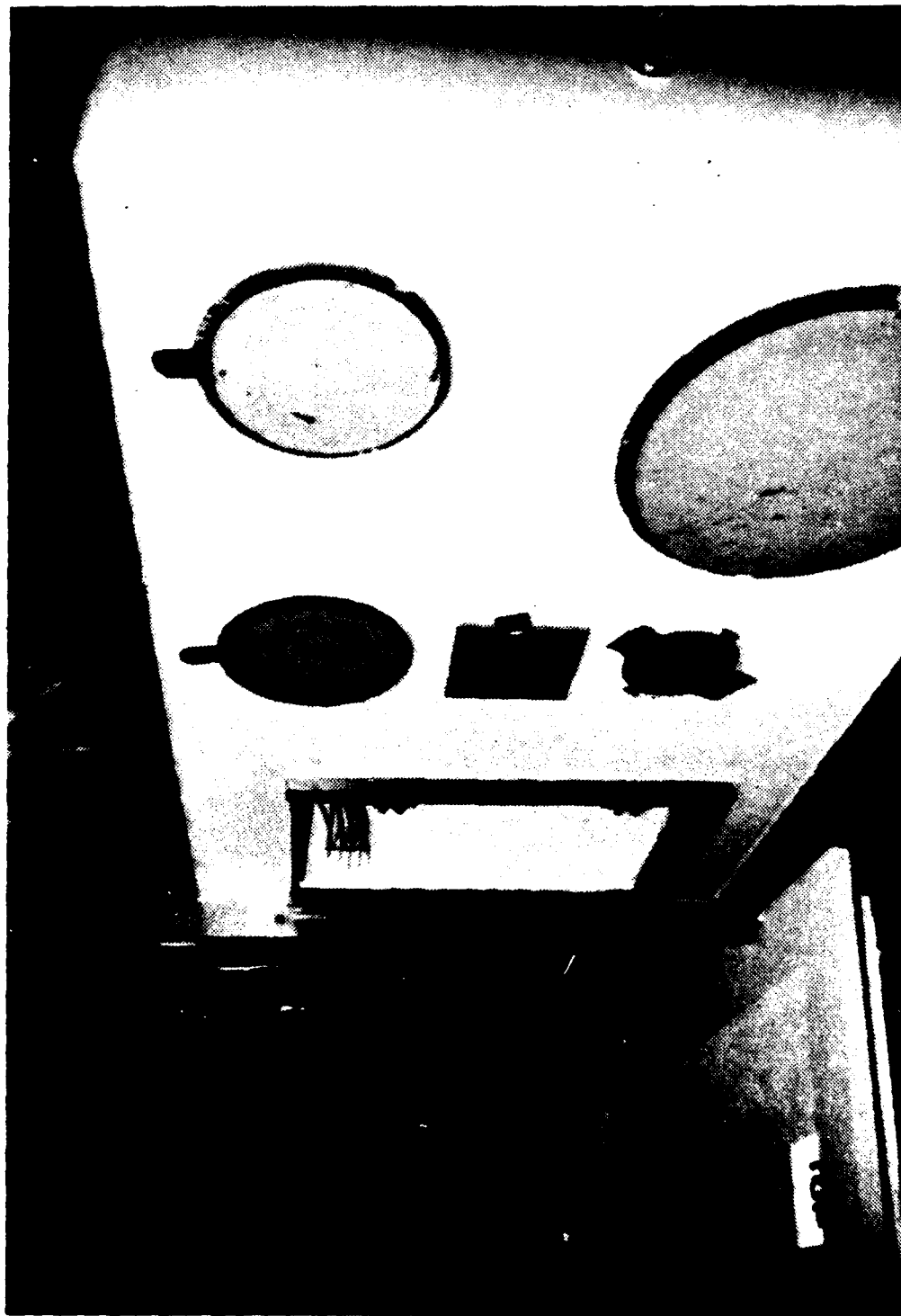


FIGURE 3 - EXTERIOR OF SECONDARY PLENUM WITH PLENUM DOOR OFF AND ASME FLOW NOZZLES CLOSED



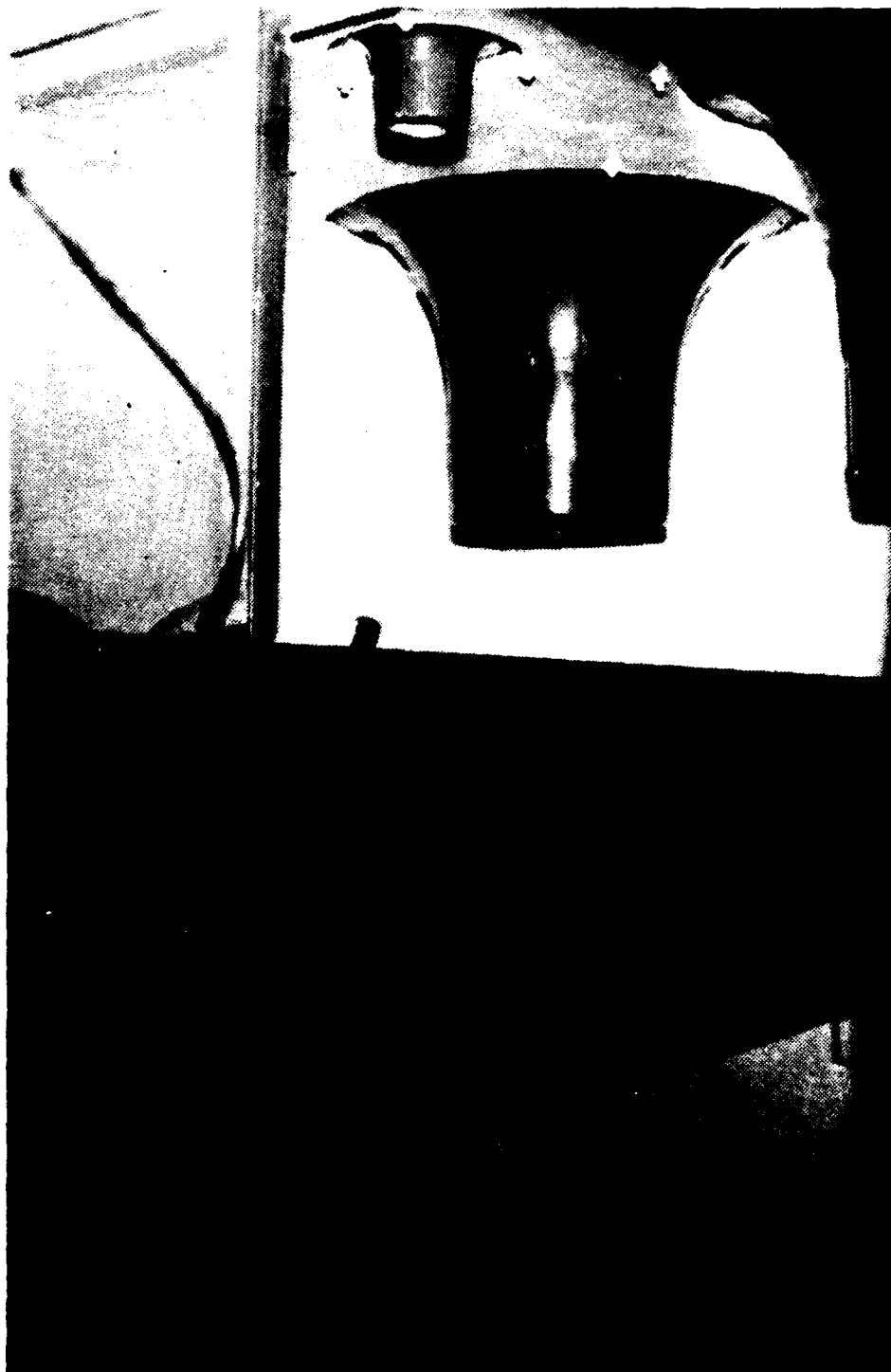


FIGURE 4 - INTERIOR OF SECONDARY PLENUM WITH ONE OF TWO FLOW STRAIGHTNERS REMOVED TO ALLOW VIEWING OF ASME FLOW NOZZLES AND NOZZLE TRANSITION DUCT

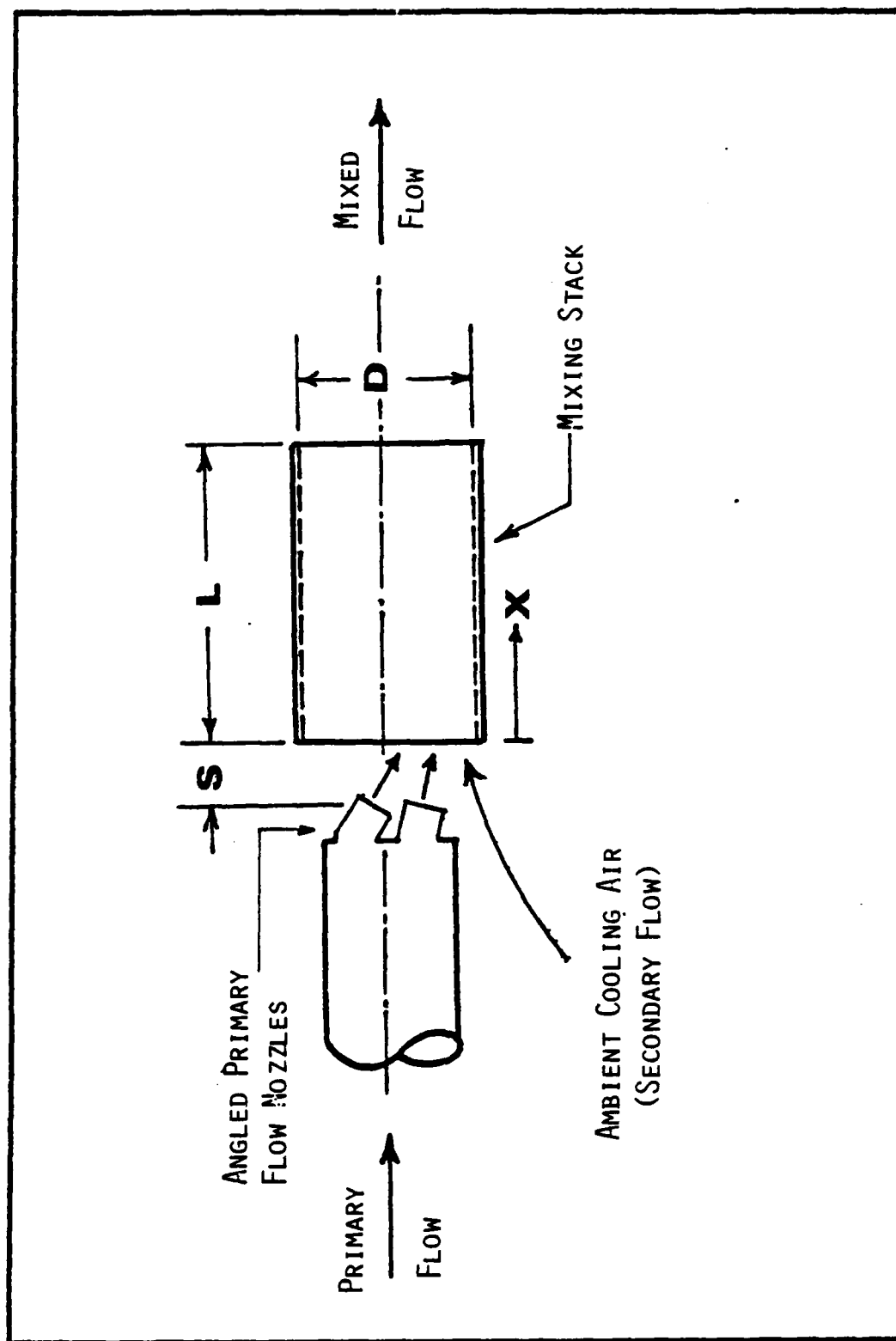


FIGURE 5 - SCHEMATIC OF STRAIGHT MIXING STACK GAS EDUCTOR WITH ANGLED NOZZLES

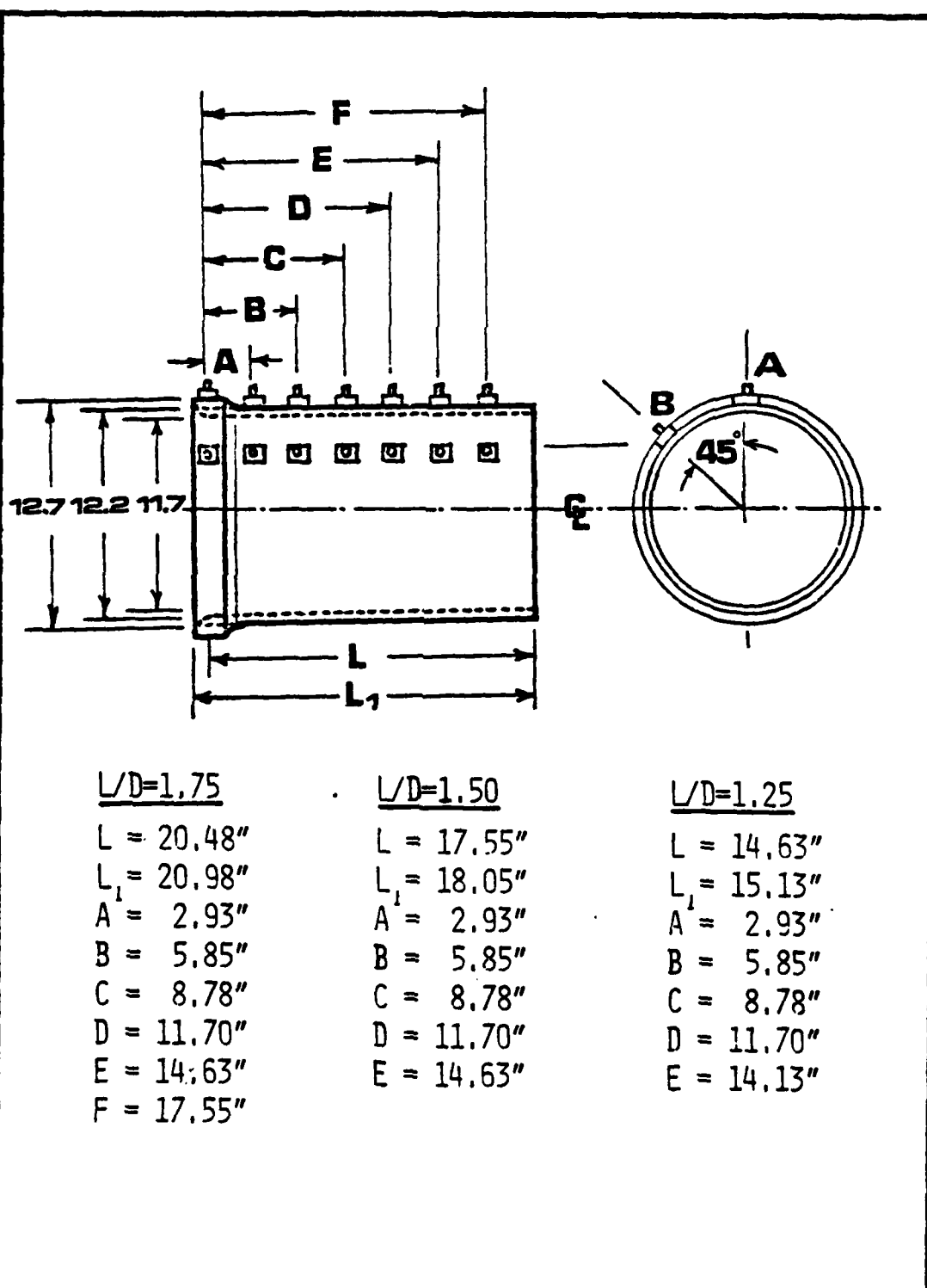


FIGURE 6 - DIMENSIONS FOR SHORT MIXING STACKS INVESTIGATED

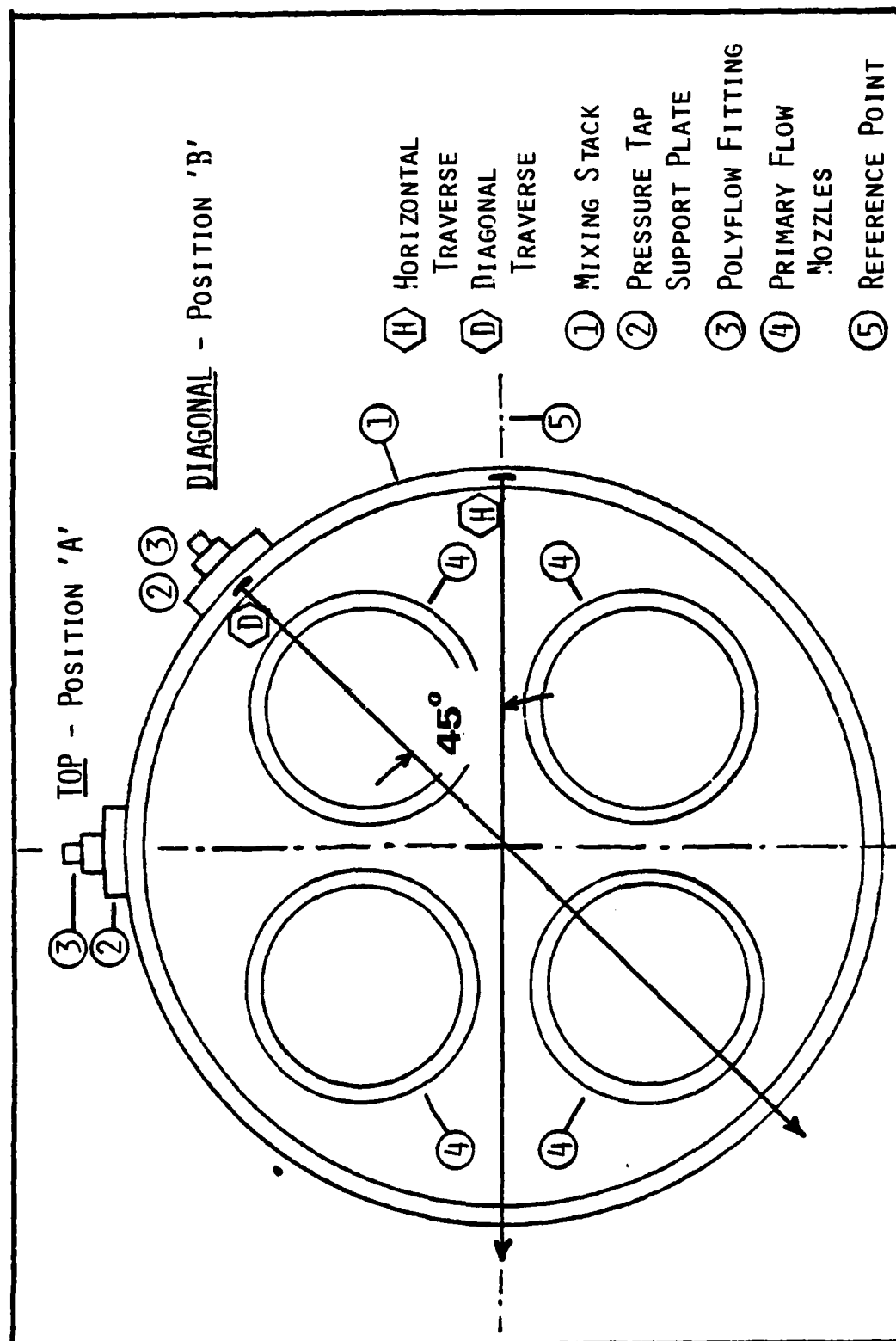


FIGURE 7 - MIXING STACK EXIT WITH VELOCITY PROFILE DIRECTIONS AND PRESSURE TAP LOCATIONS

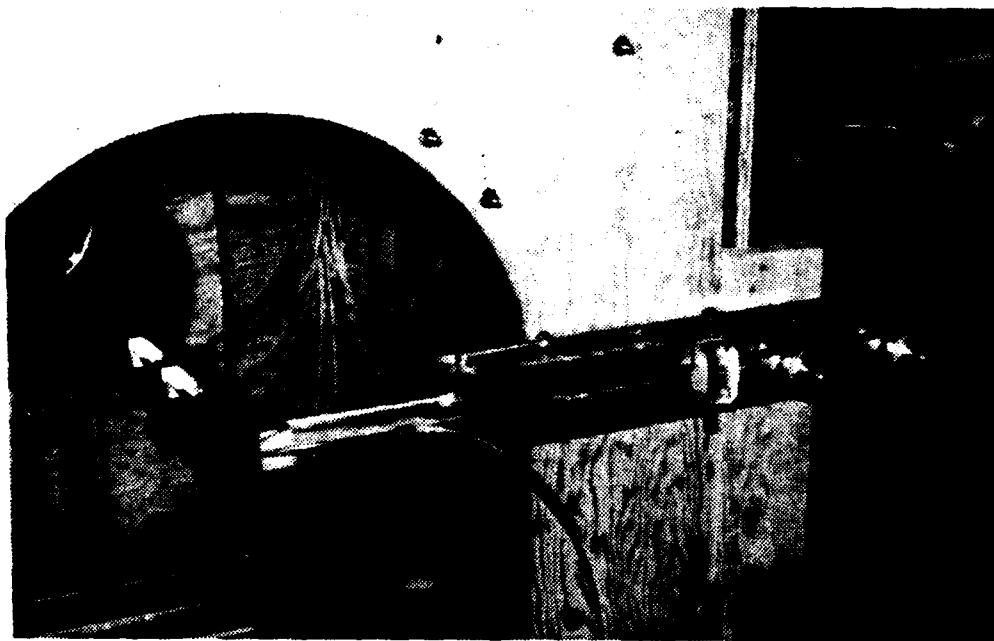


FIGURE 8 - VELOCITY TRAVERSE BAR AND MIXING STACK

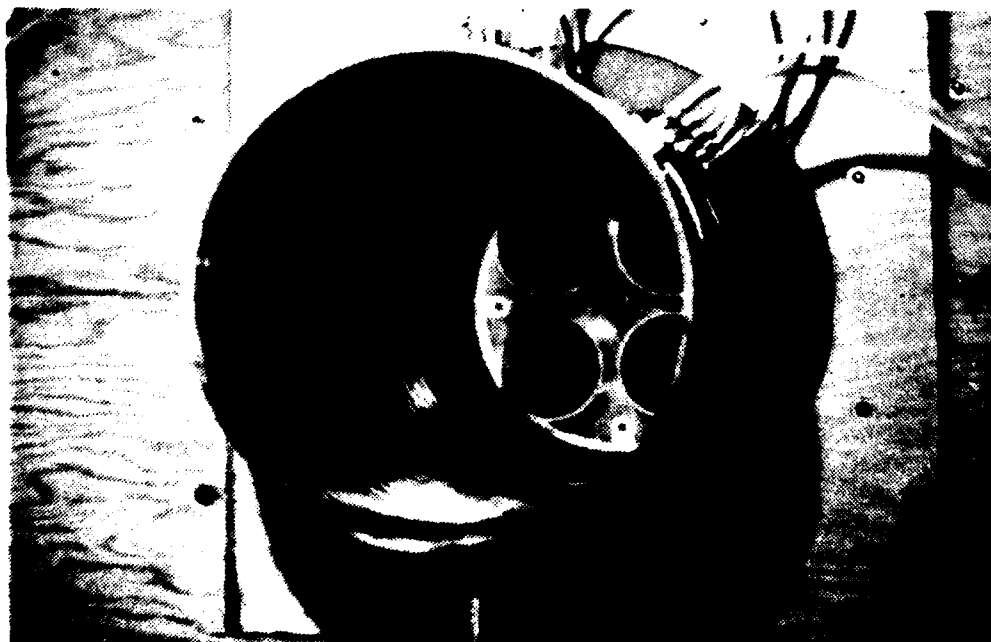
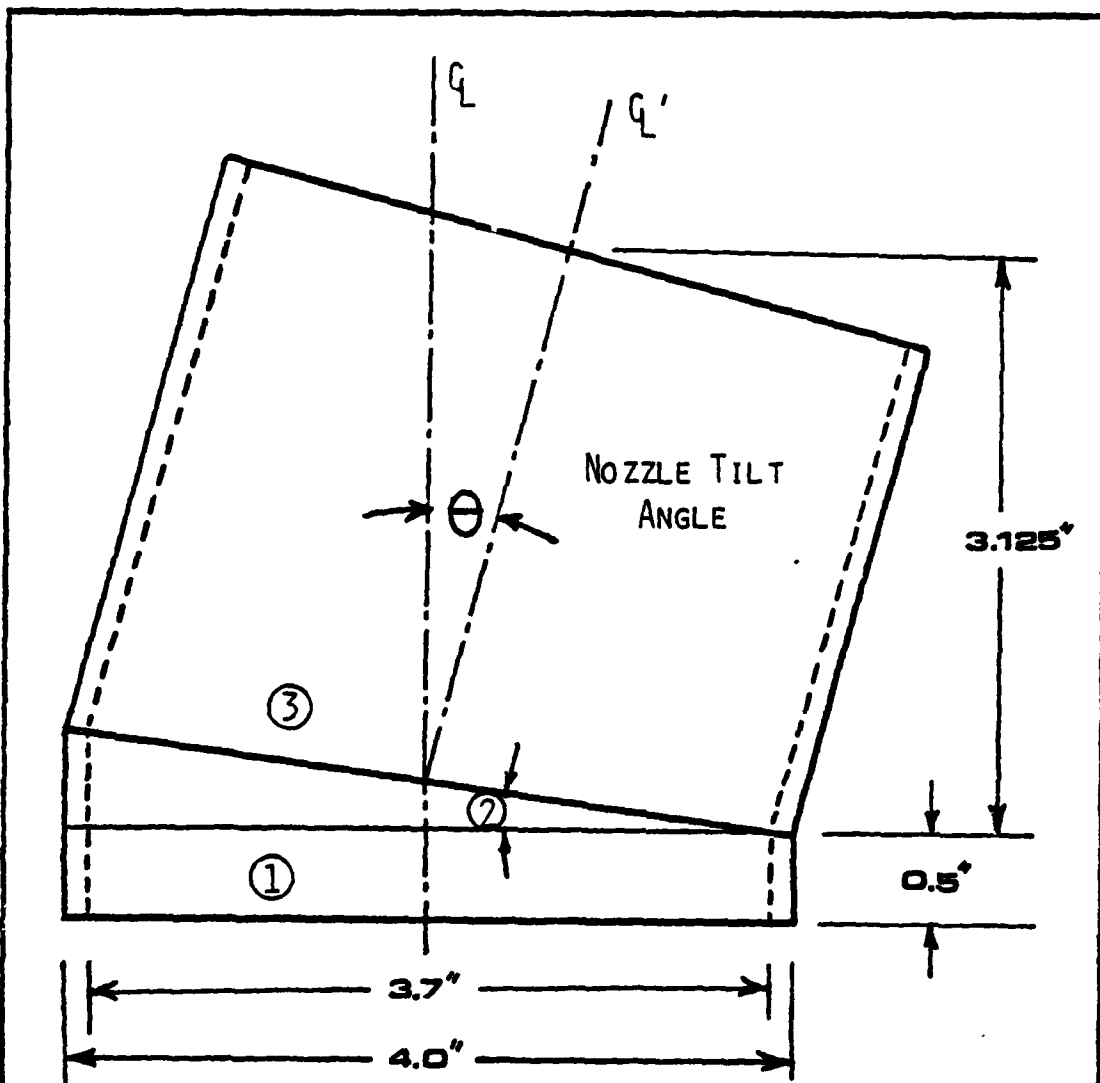


FIGURE 9 - MIXING STACK WITH PRESSURE TAPS AND AIR SEAL



- ① 0.5 INCH MACHINED SURFACE TO FIT THE NOZZLE BASE PLATE RECESSES
- ② MITER ANGLE - ONE-HALF OF THE TILT ANGLE
- ③ CUT AND JUNCTURE LINE

NOTE: FOUR SETS OF ANGLED NOZZLES WERE CONSTRUCTED WITH TILT ANGLES OF 10, 15, 20, AND 22.5 DEGREES.

FIGURE 10 - DIMENSIONS OF ANGLED NOZZLES AND NOZZLE TILT ANGLE



FIGURE 11 - ANGLED PRIMARY FLOW NOZZLE

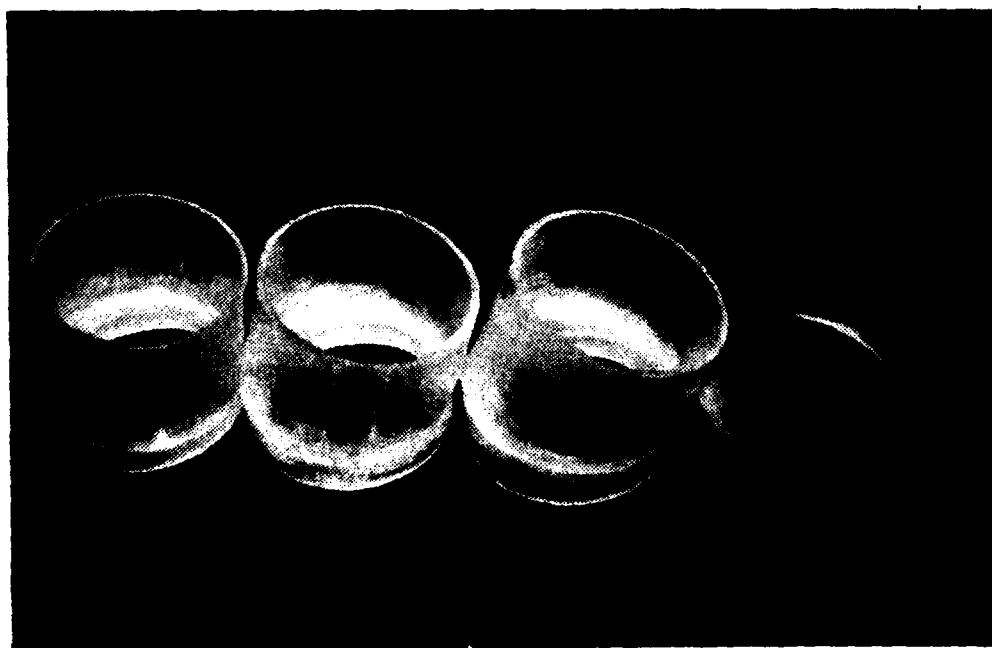


FIGURE 12 - ANGLED NOZZLES WITH TILT ANGLES 10 TO 22.5 DEGREES

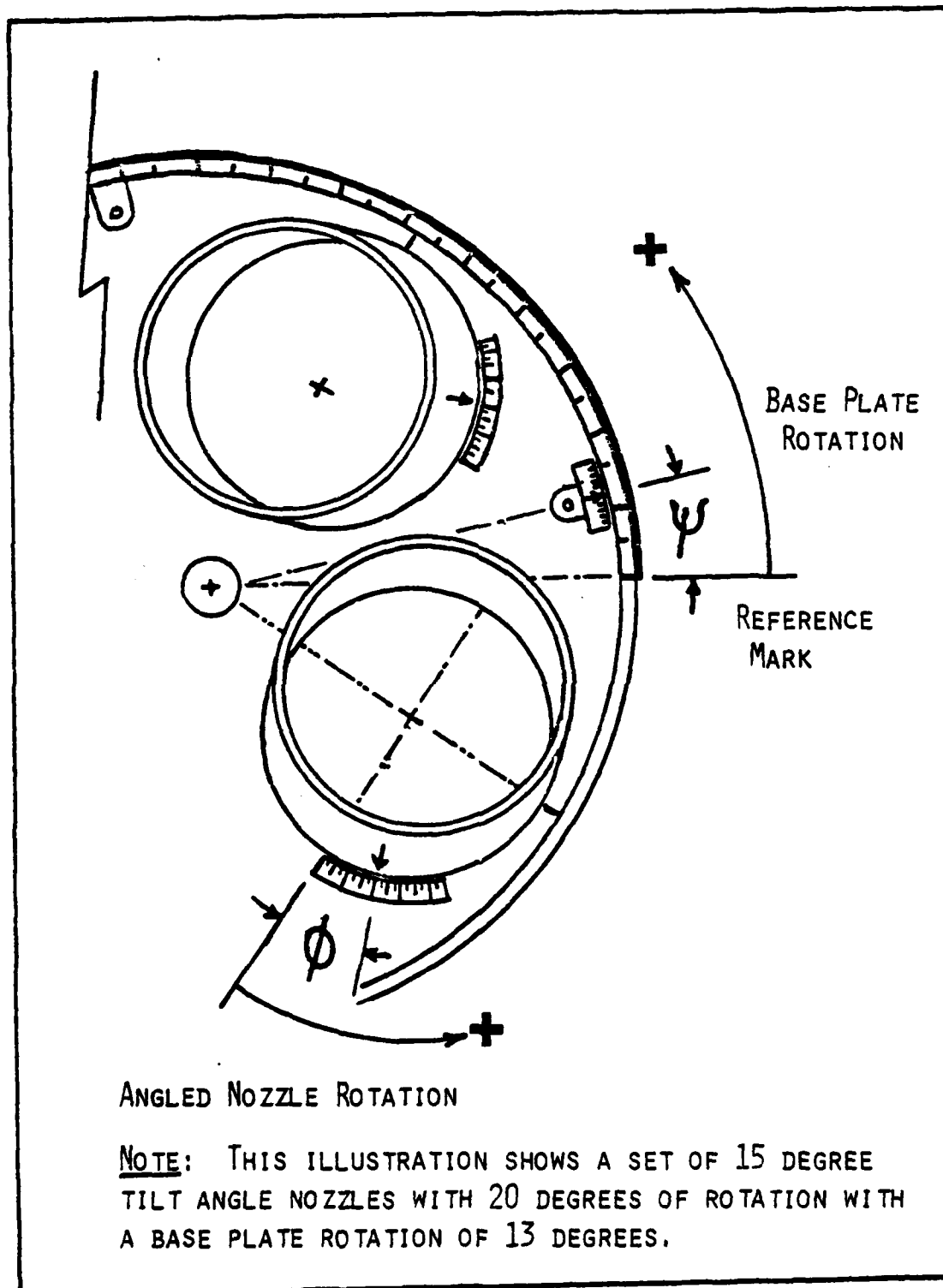


FIGURE 13 - BASE PLATE ROTATION ANGLE AND NOZZLE ROTATION ANGLE



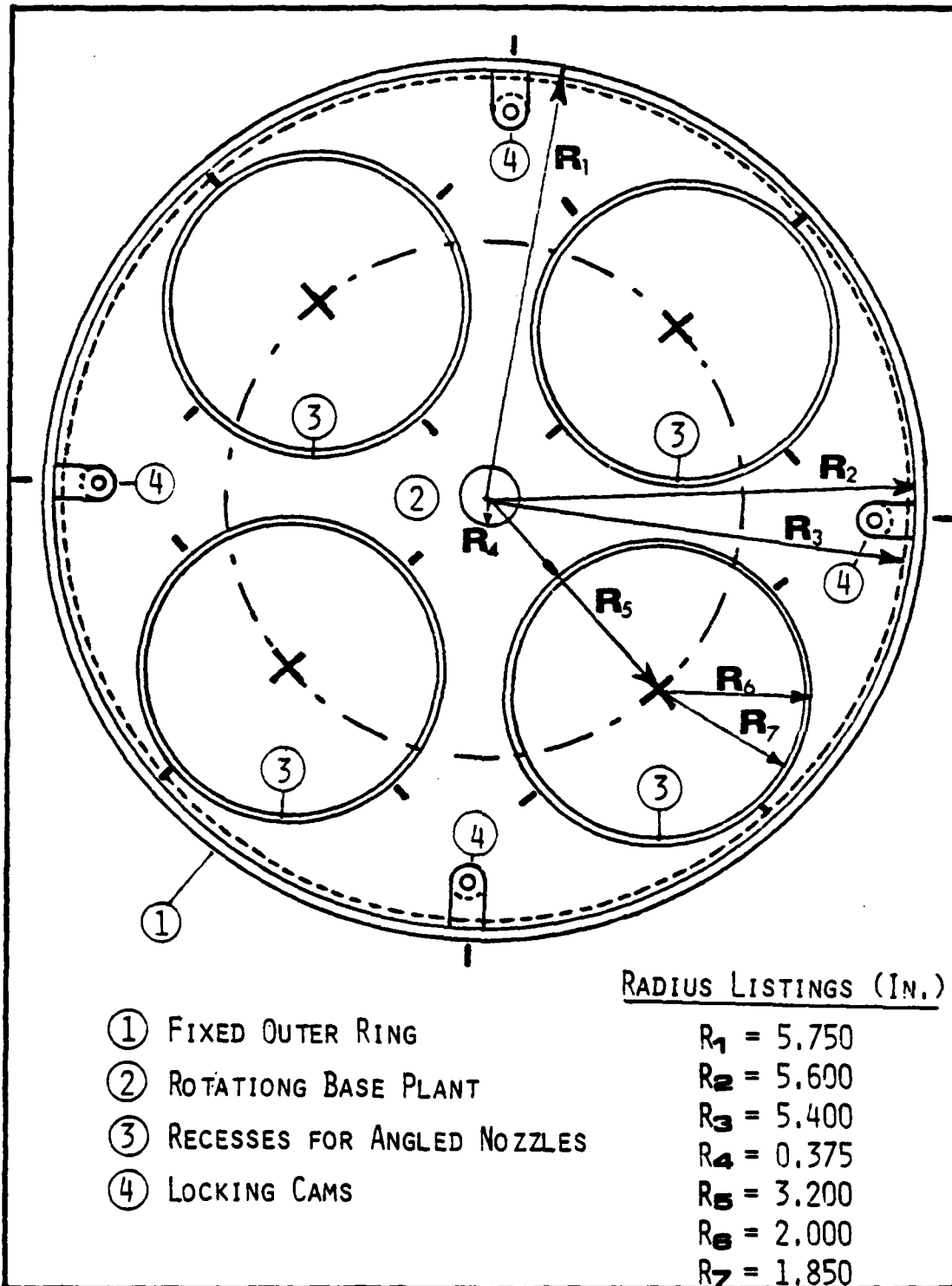


FIGURE 14 - DIMENSIONS FOR THE ROTATABLE NOZZLE BASE PLATE

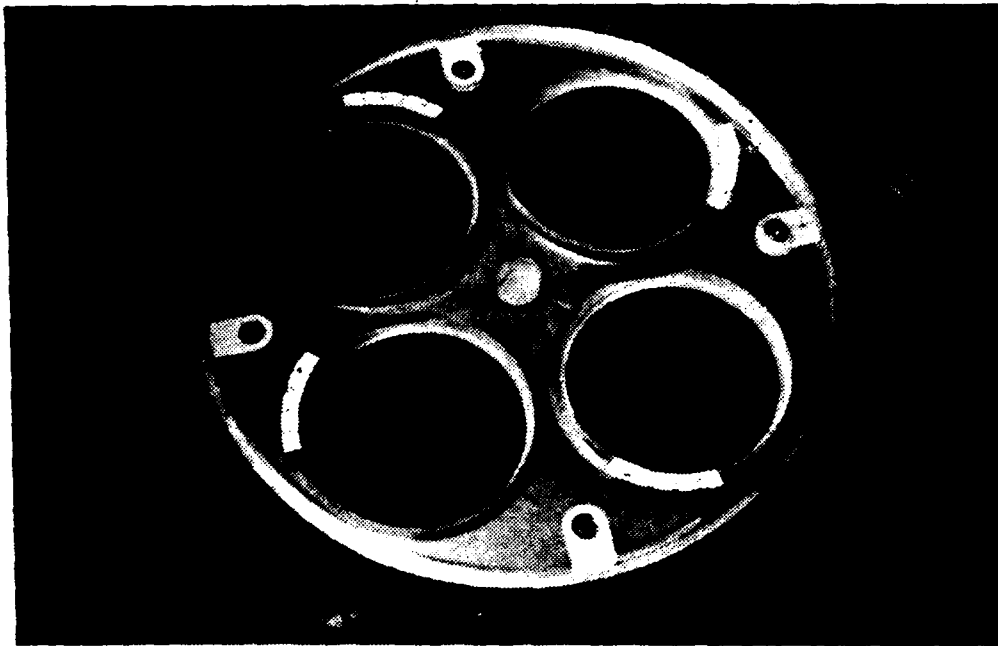


FIGURE 15 - ROTATABLE BASE PLATE FOR ANGLED NOZZLES

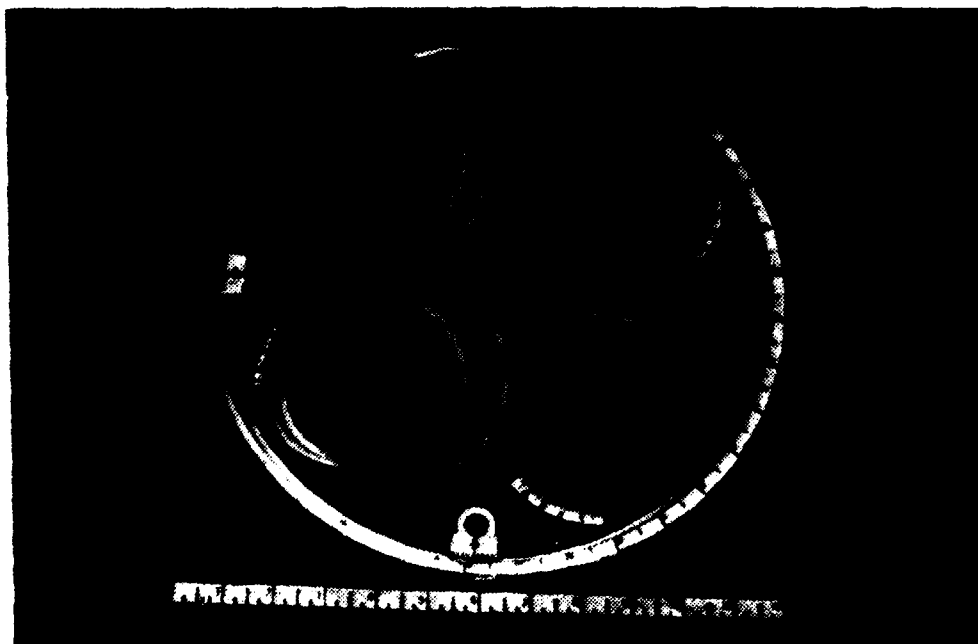


FIGURE 16 - BASE PLATE WITH A 20/20 NOZZLE COMBINATION

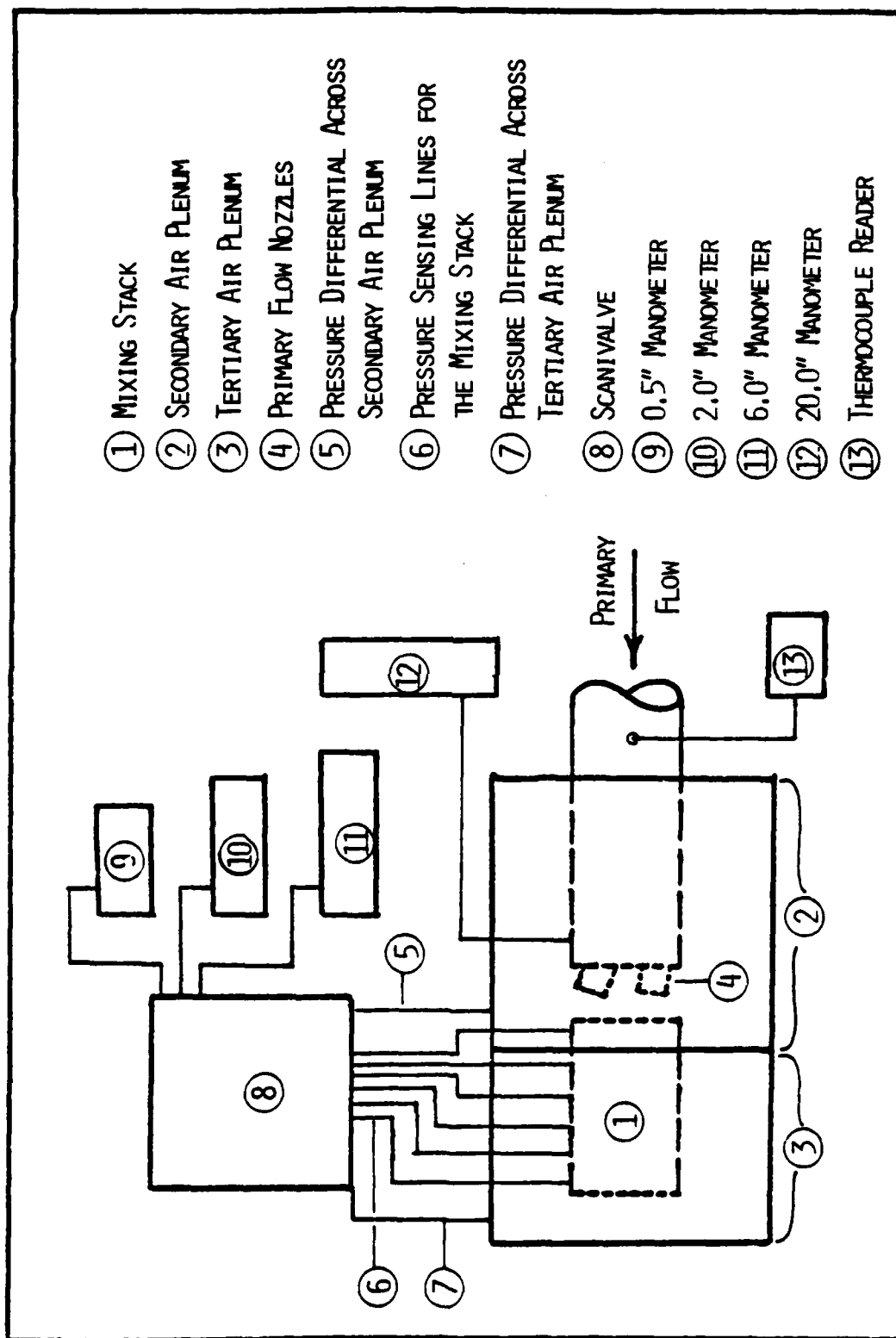


FIGURE 17 - SCHEMATIC OF INSTRUMENTATION

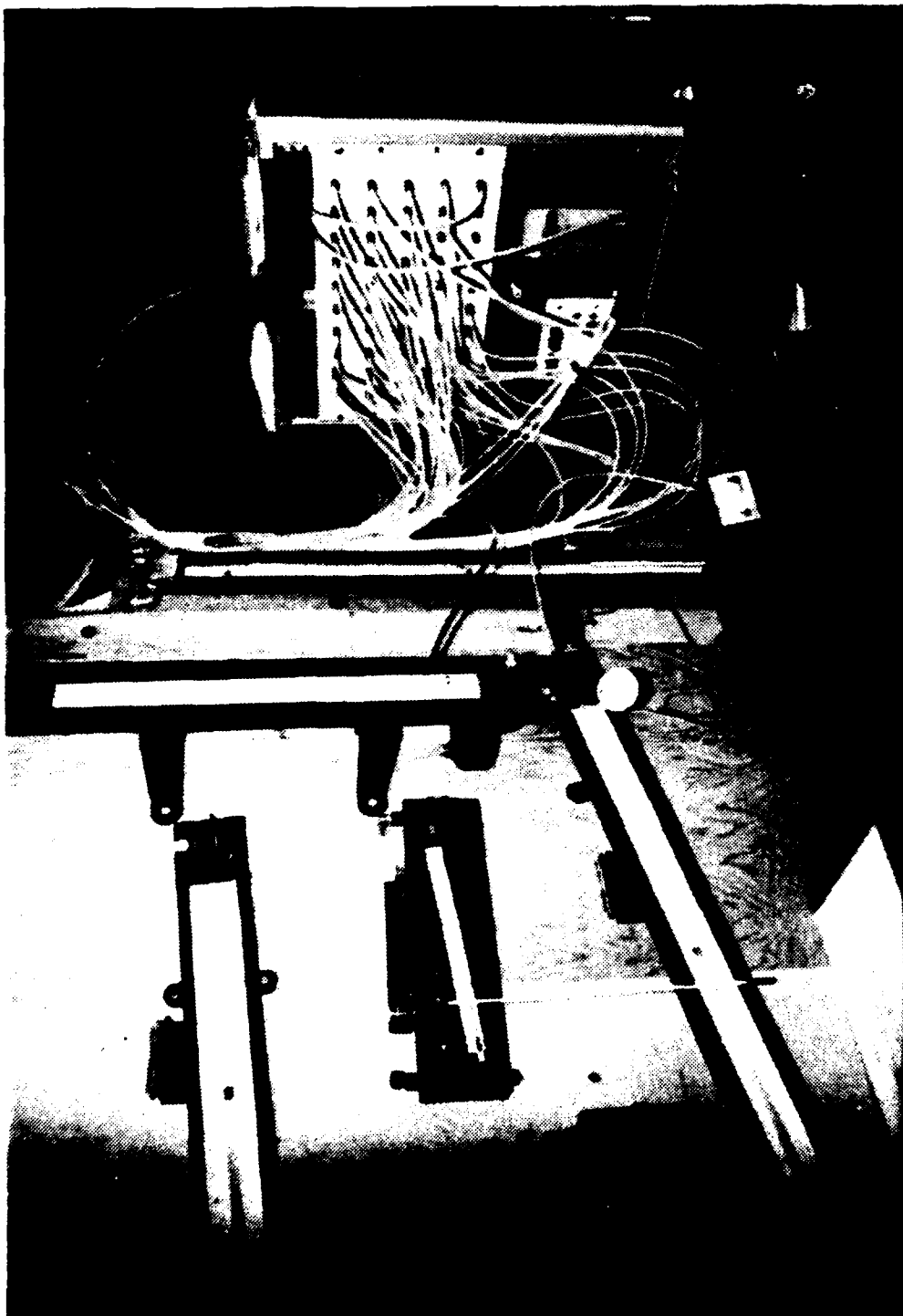


FIGURE 18 - INSTRUMENTATION

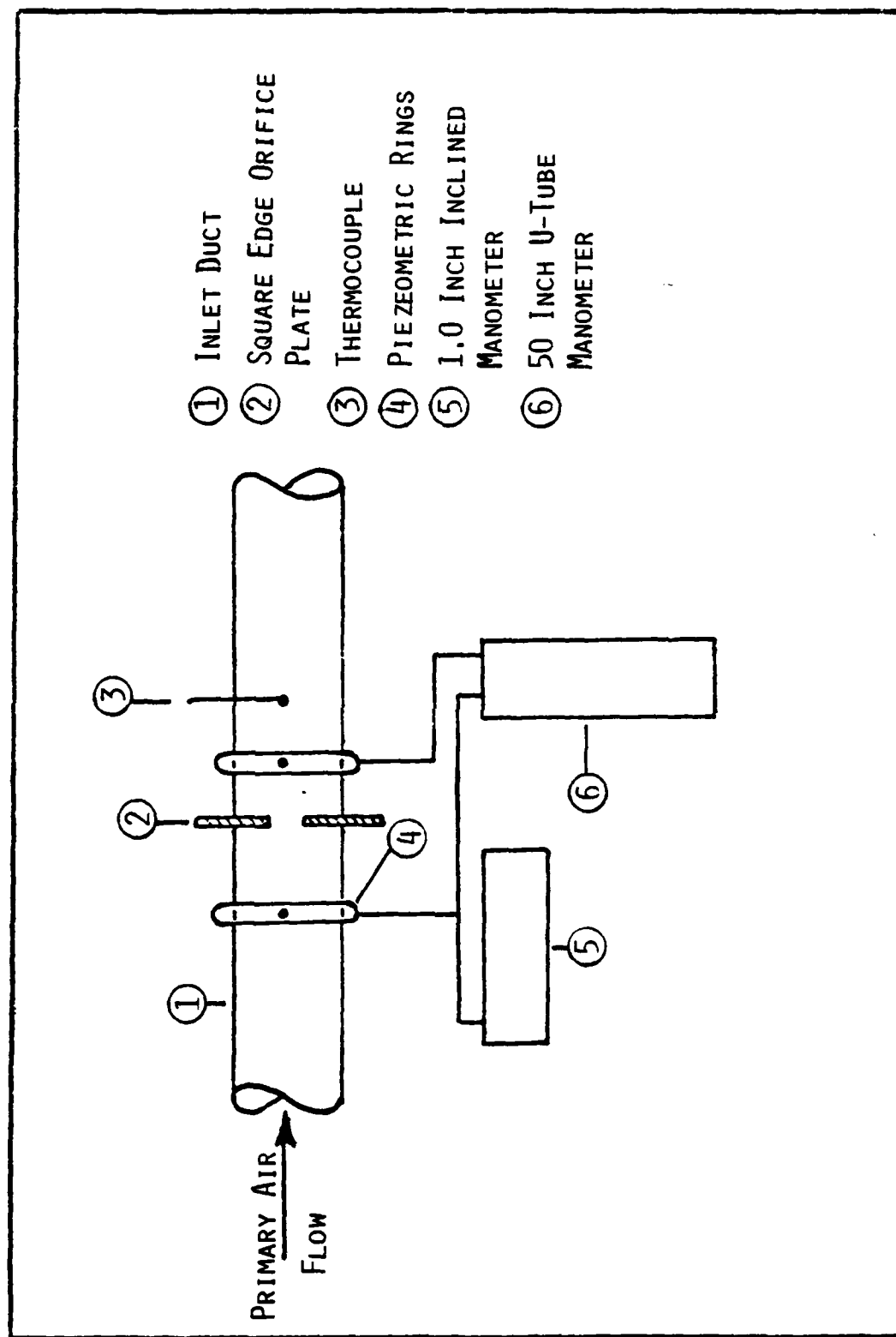


FIGURE 19 - SCHEMATIC OF INSTRUMENTATION FOR PRIMARY AIR FLOW MEASUREMENT

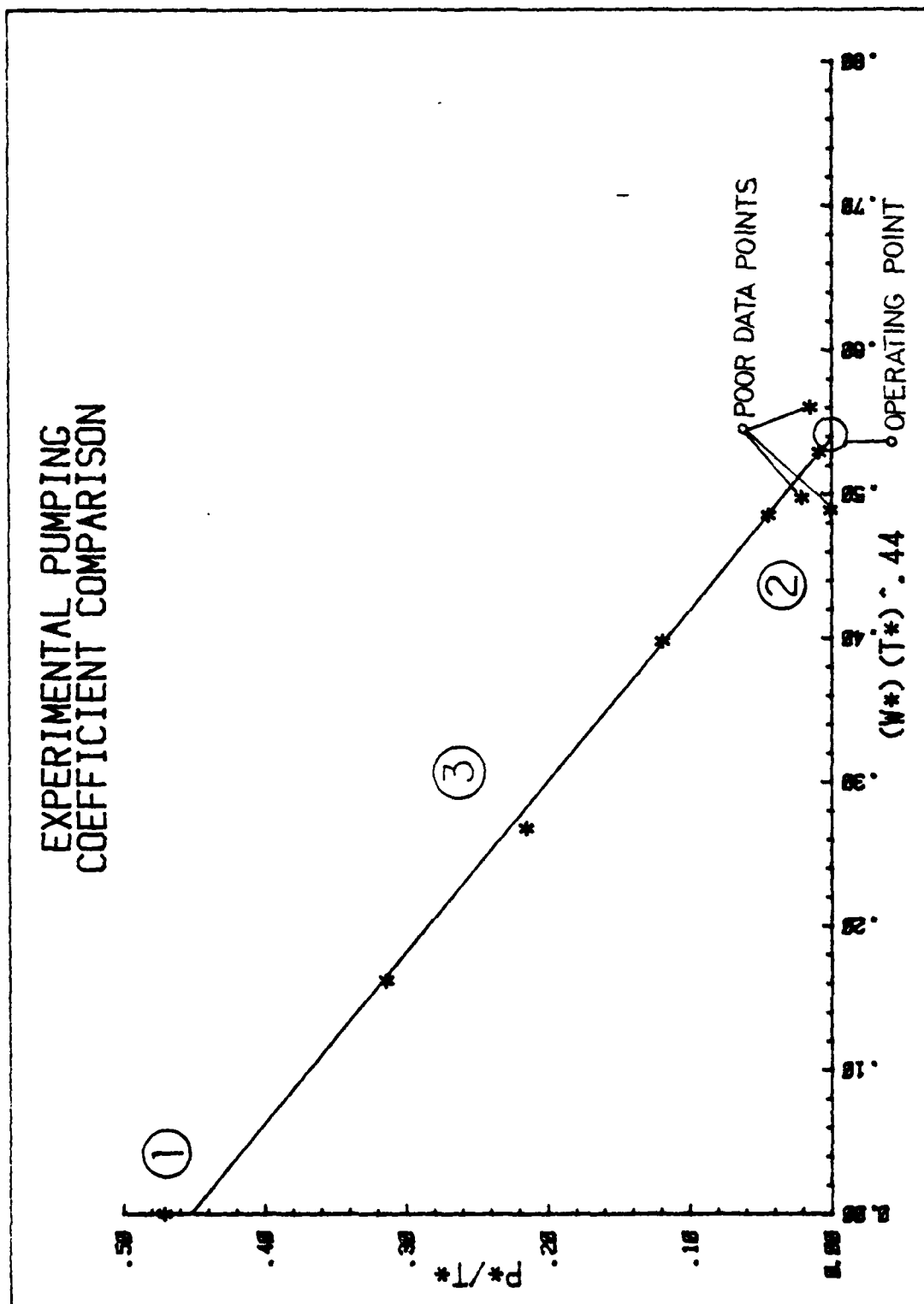


FIGURE 20 - SAMPLE PUMPING COEFFICIENT PLOT

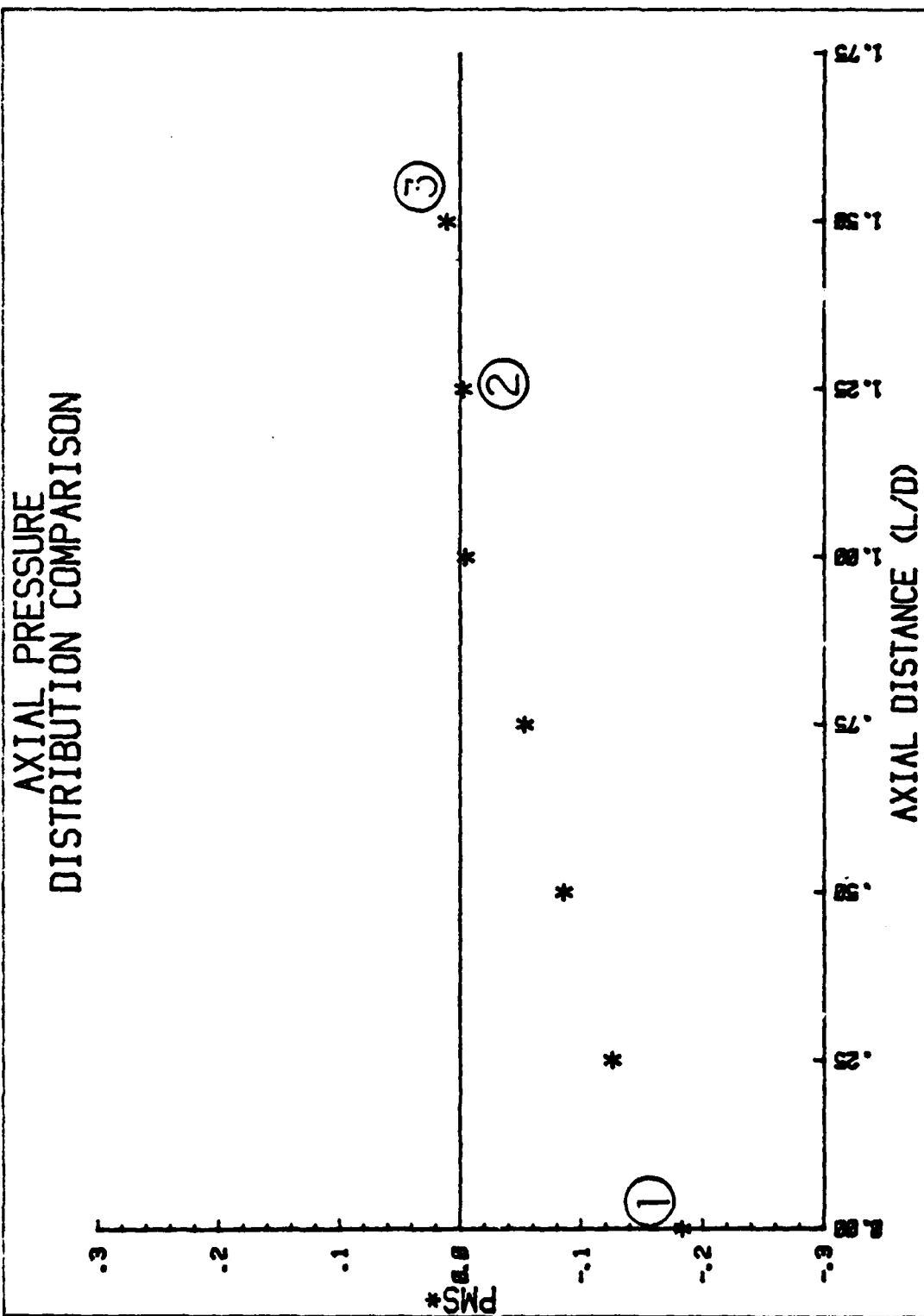


FIGURE 21 - SAMPLE MIXING STACK PRESSURE DISTRIBUTION PLOT

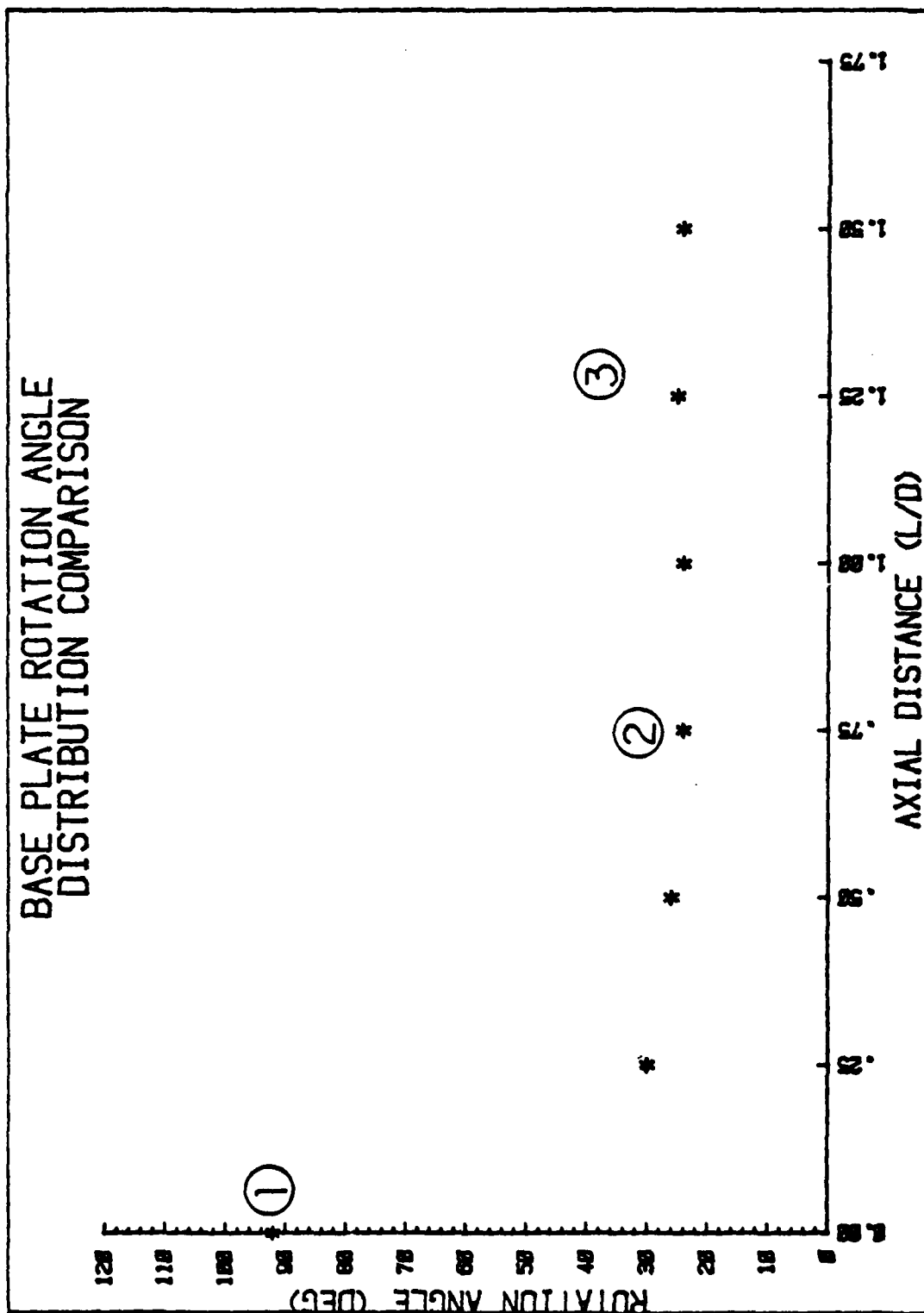


FIGURE 22 -- SAMPLE BASE PLATE ROTATION ANGLE DISTRIBUTION PLOT



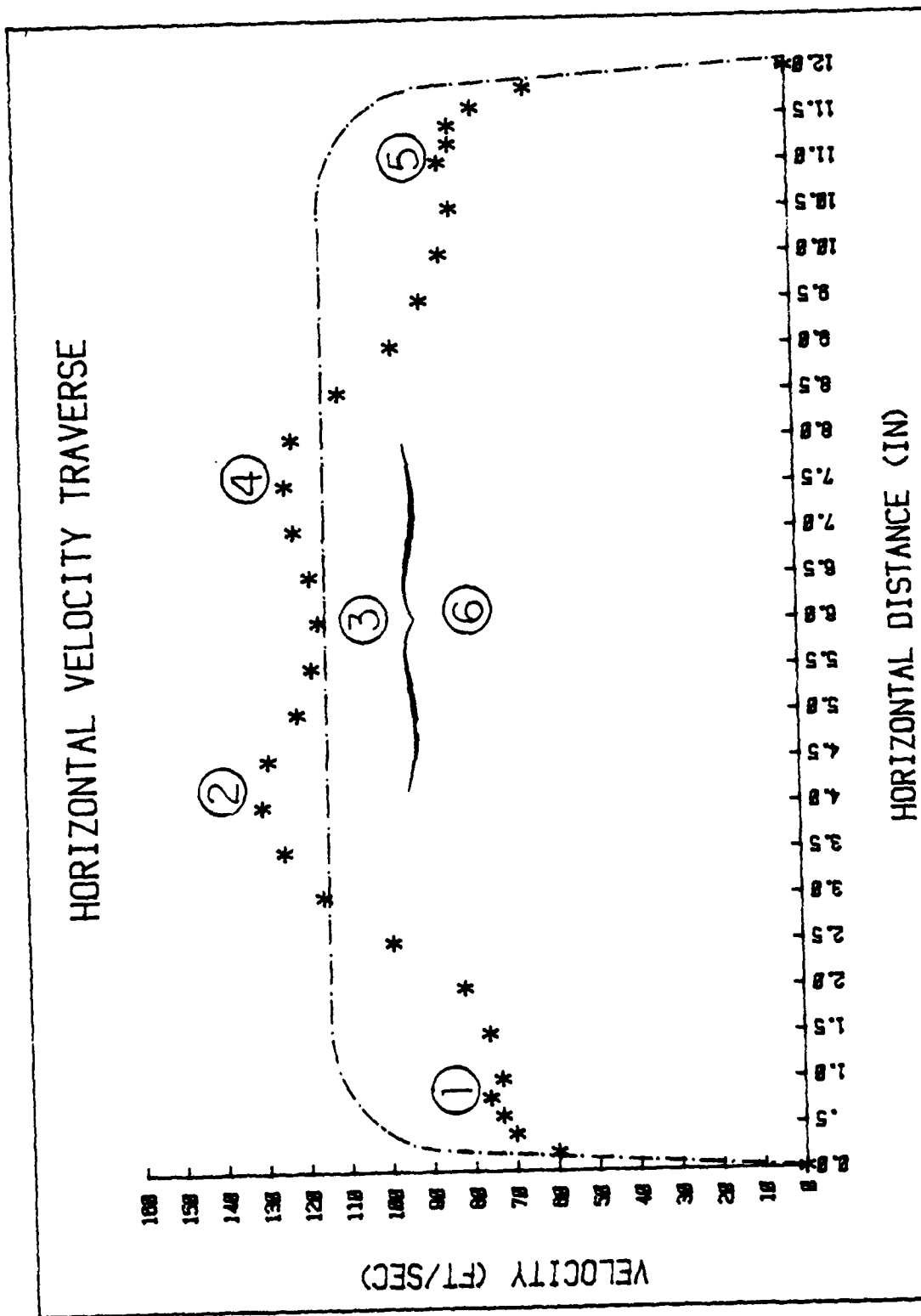


FIGURE 23 - SAMPLE HORIZONTAL VELOCITY PROFILE PLOT

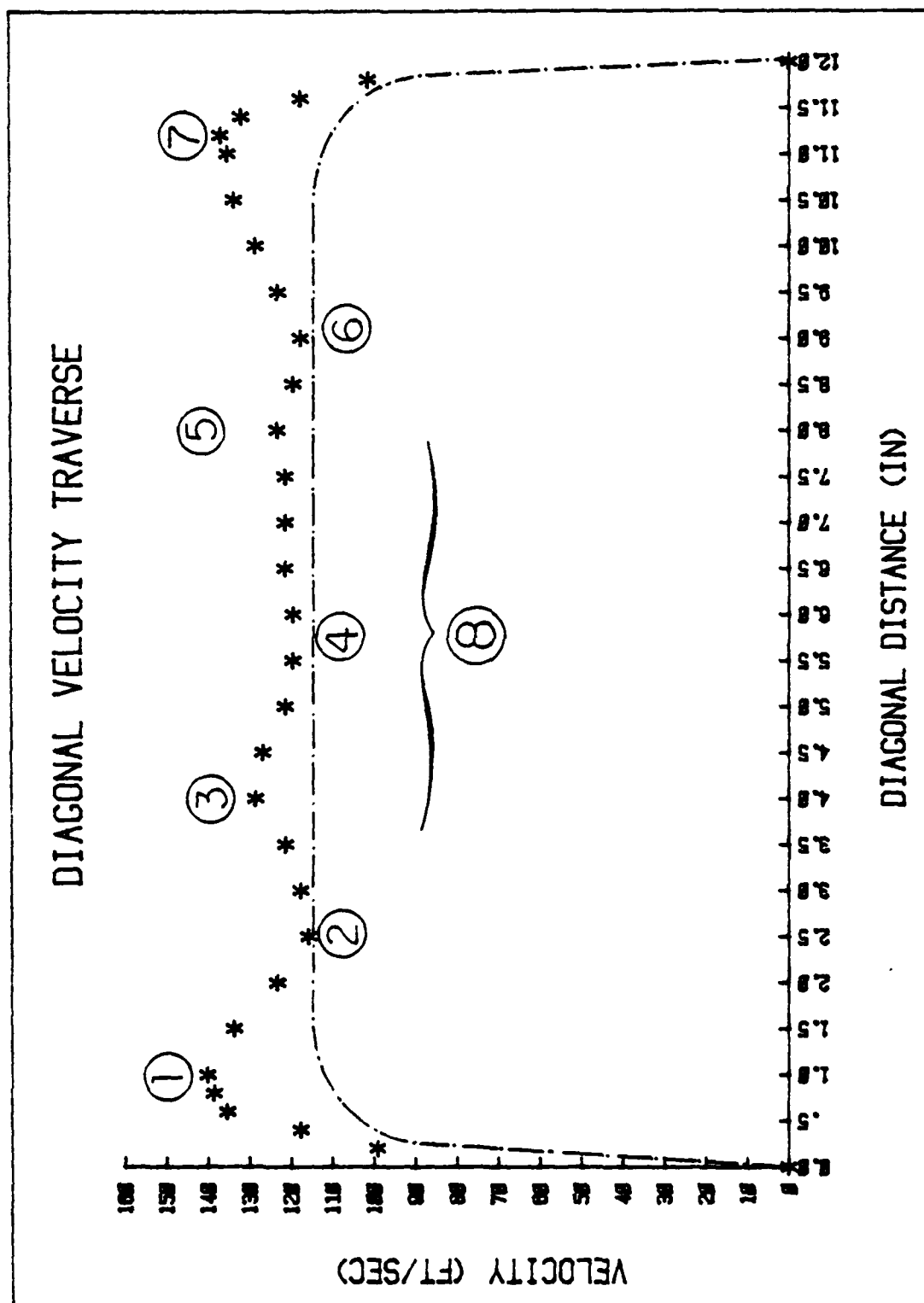


FIGURE 24 - SAMPLE DIAGONAL VELOCITY PROFILE PLOT

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

L/D=1.75  
S/D=0.5

\*-DATA TAKEN BY DAVIS/DRUCKER  
O-DATA TAKEN BY LEMKE/STAEHLI

STRAIGHT NOZZLES  
CALIBRATION RUN

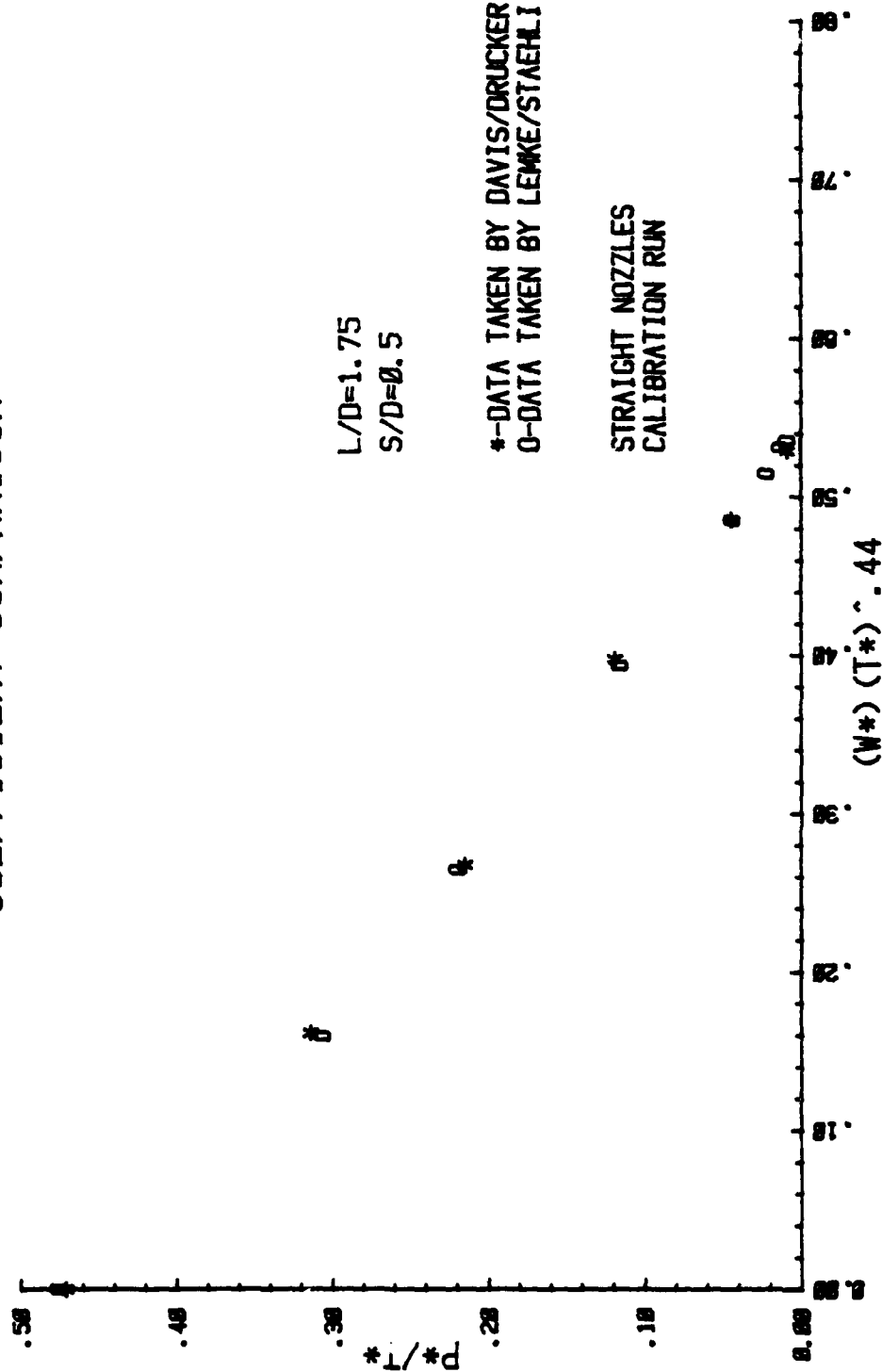


FIGURE 25

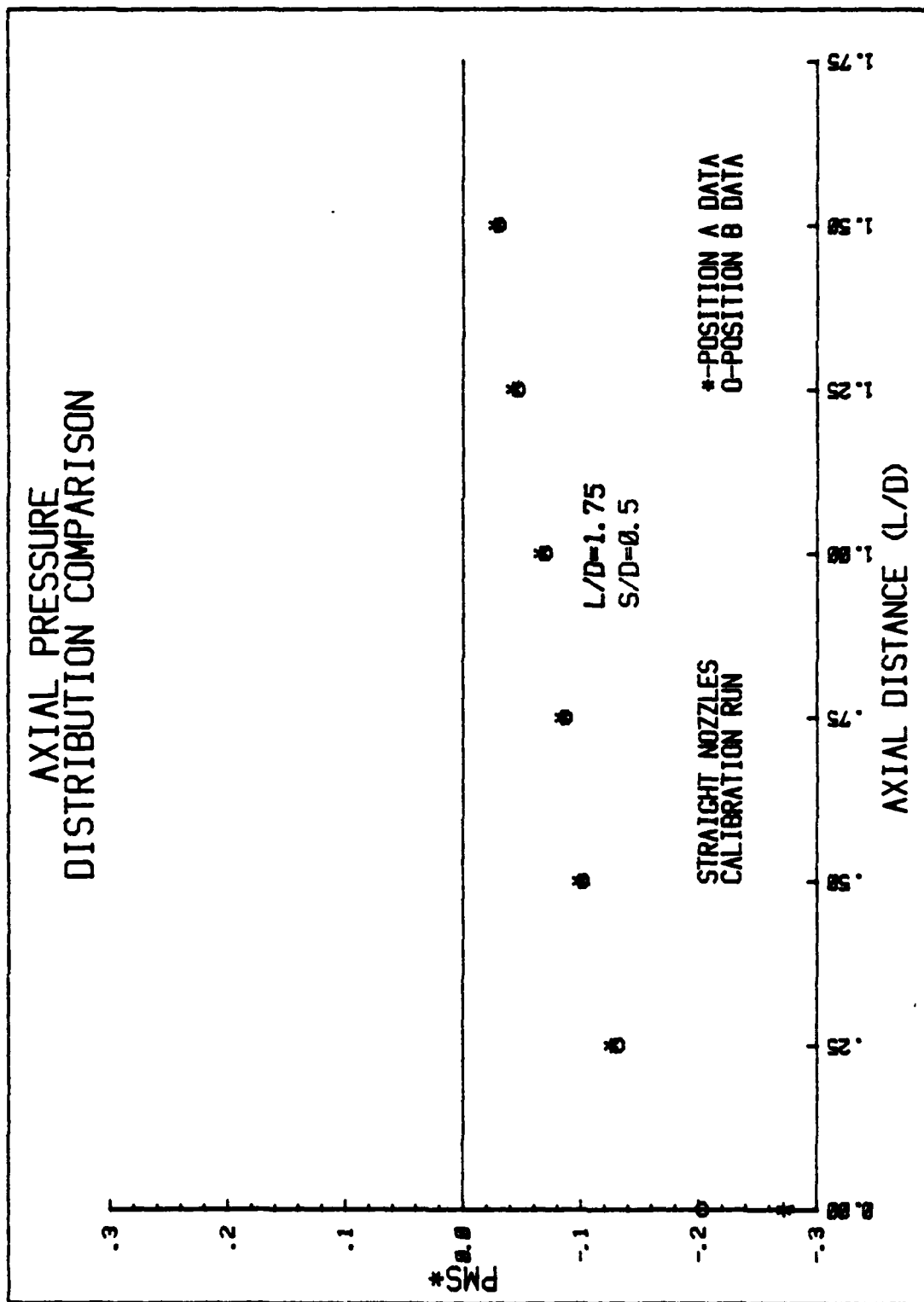


FIGURE 25.1

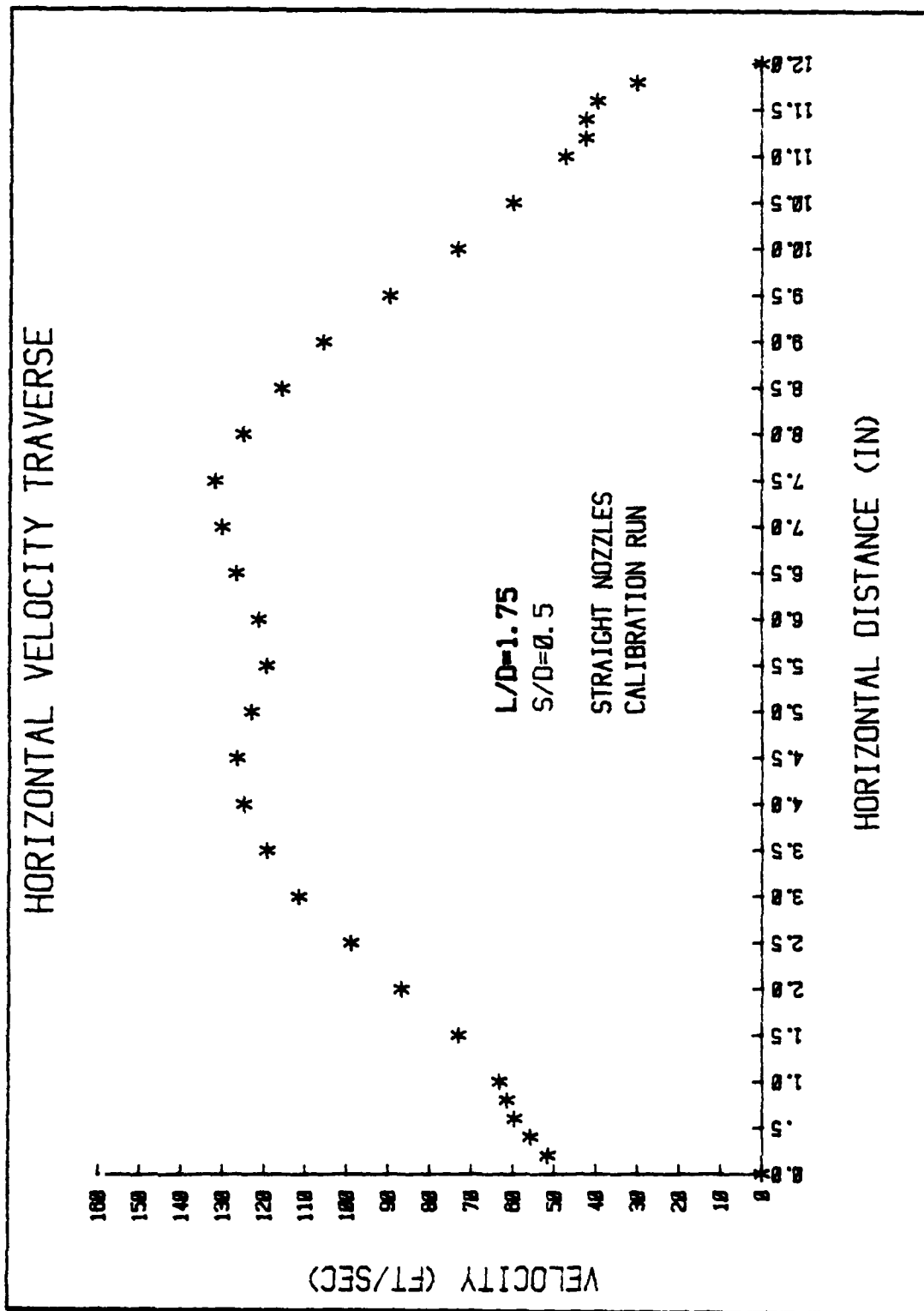


FIGURE 25.2

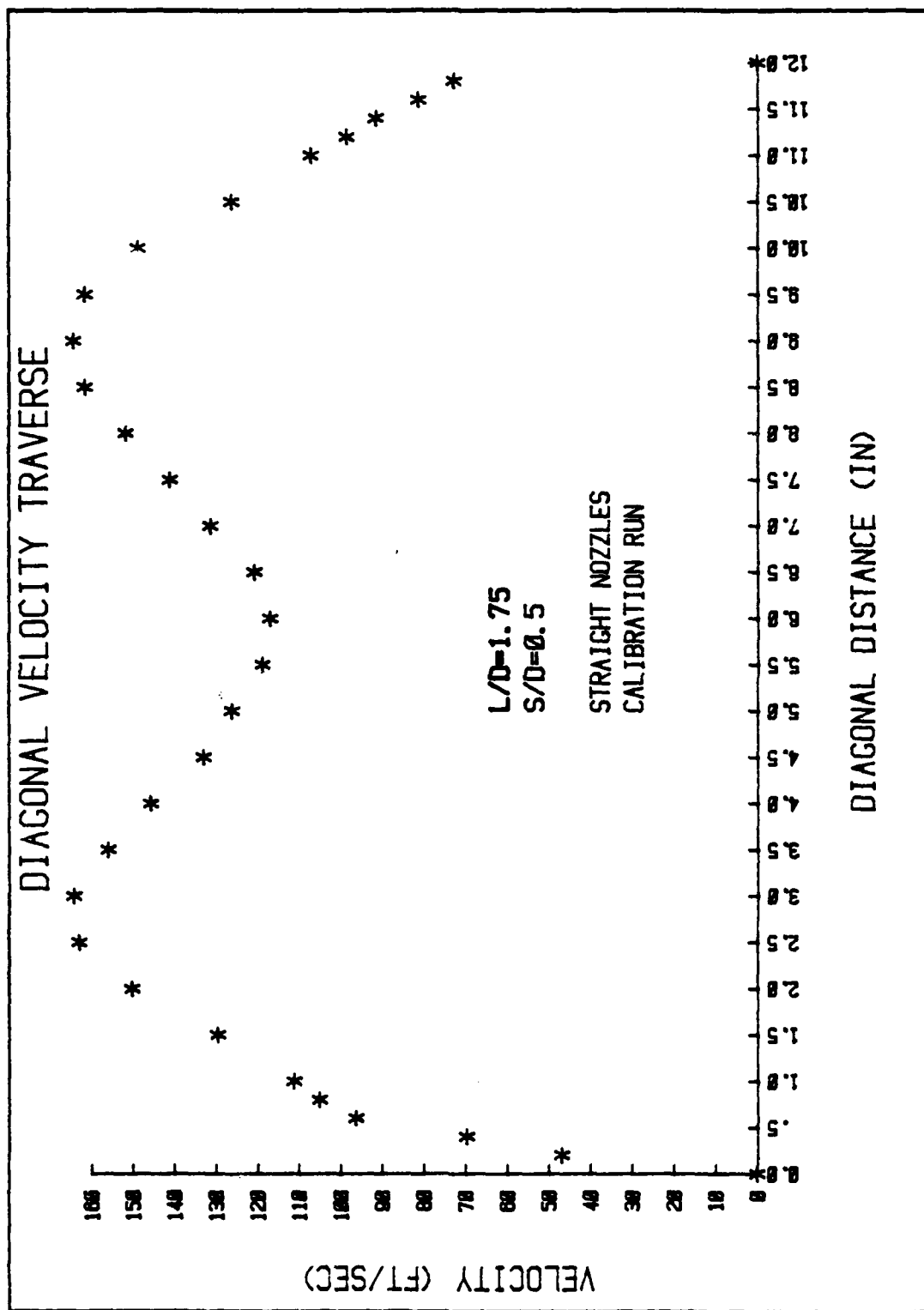


FIGURE 25.3

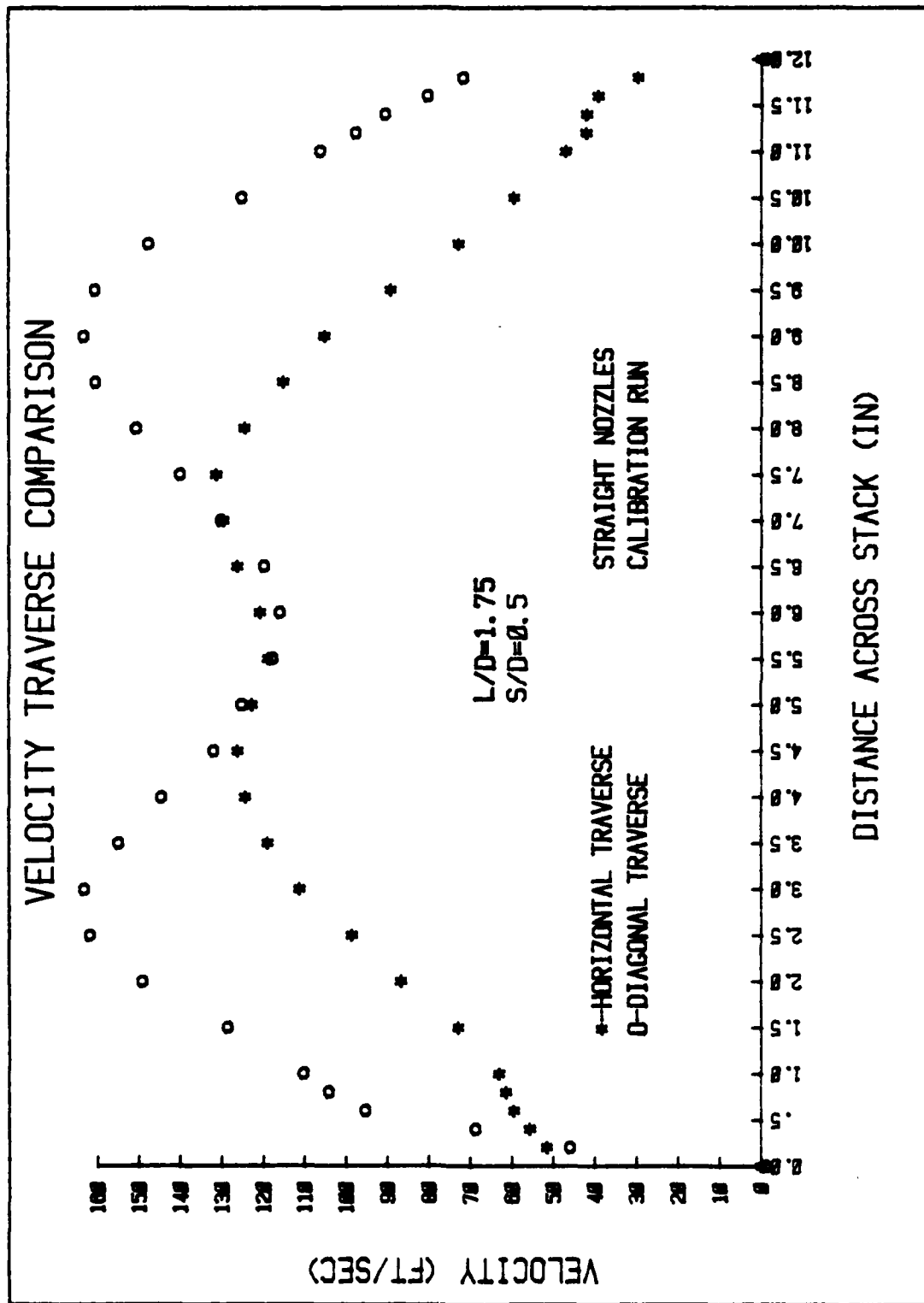


FIGURE 25.4

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

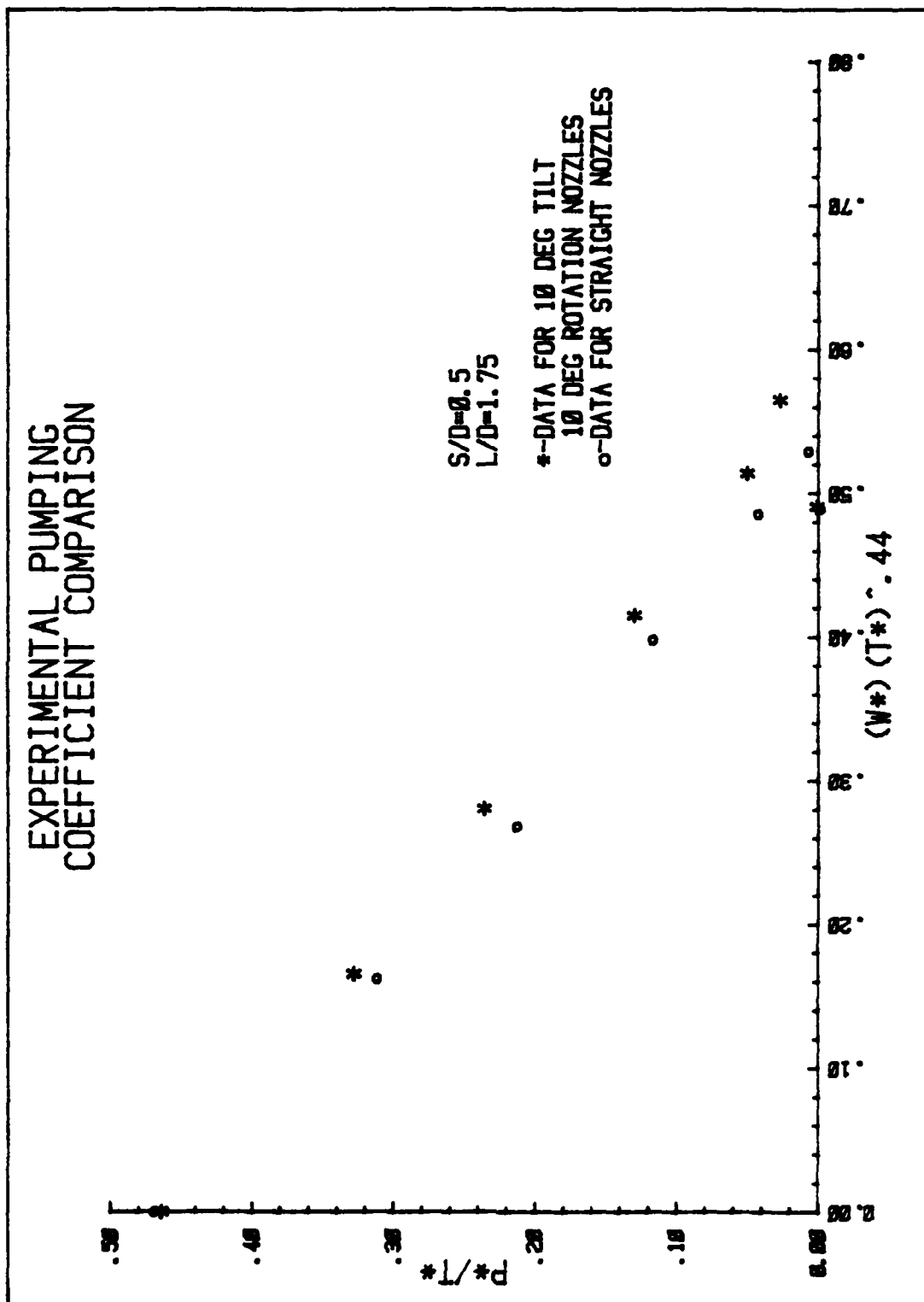


FIGURE 26



# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

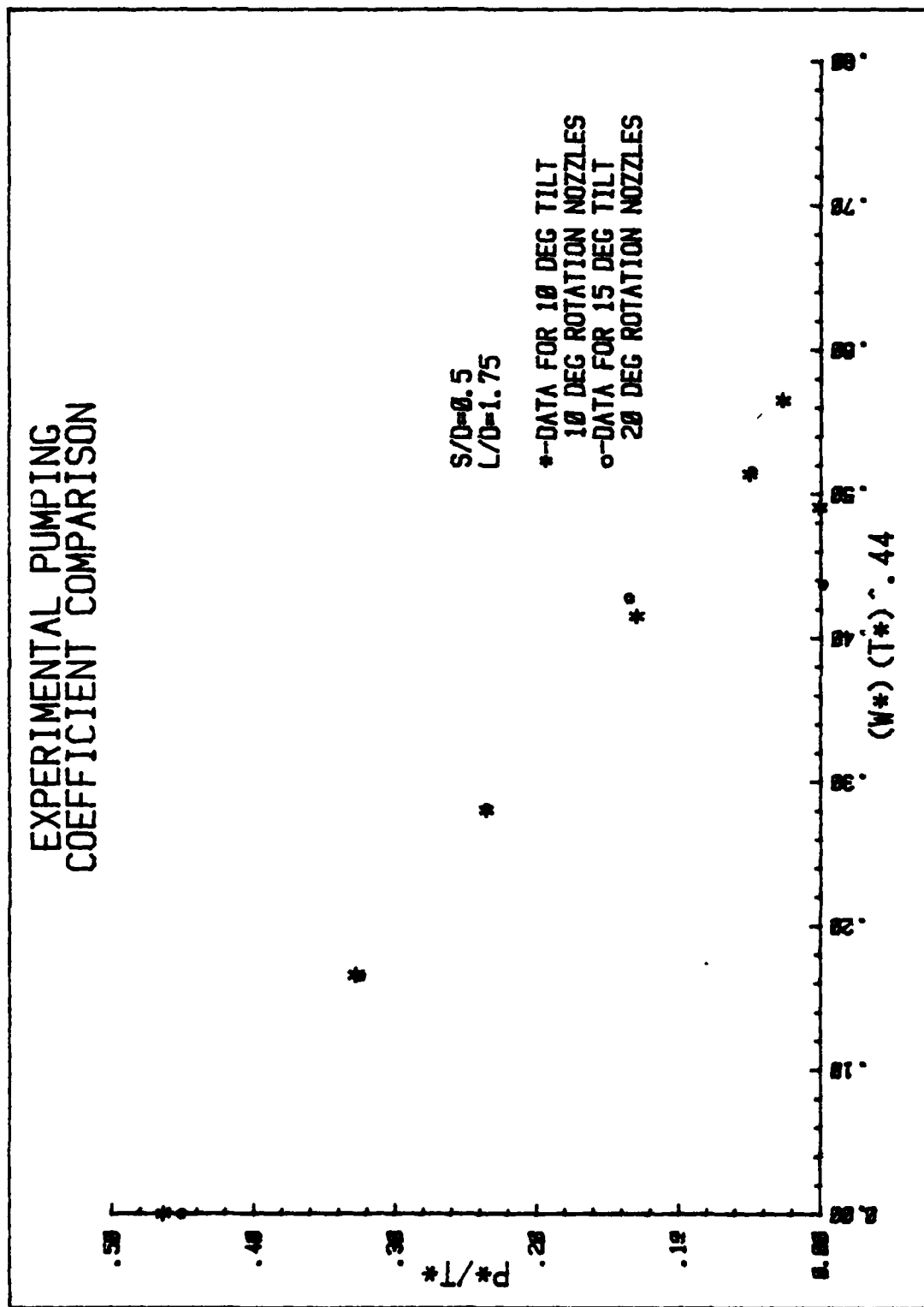


FIGURE 28.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

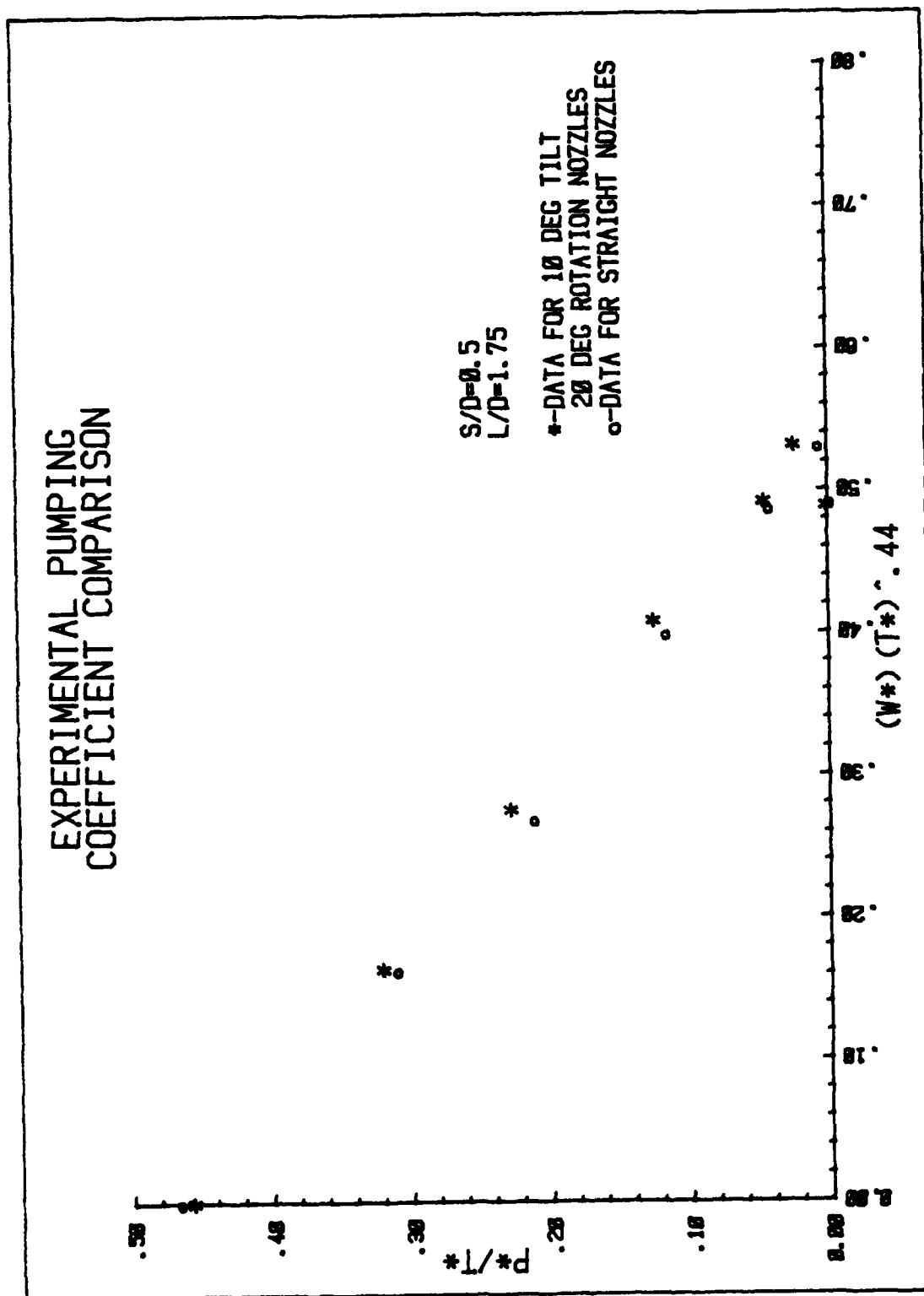


FIGURE 27

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

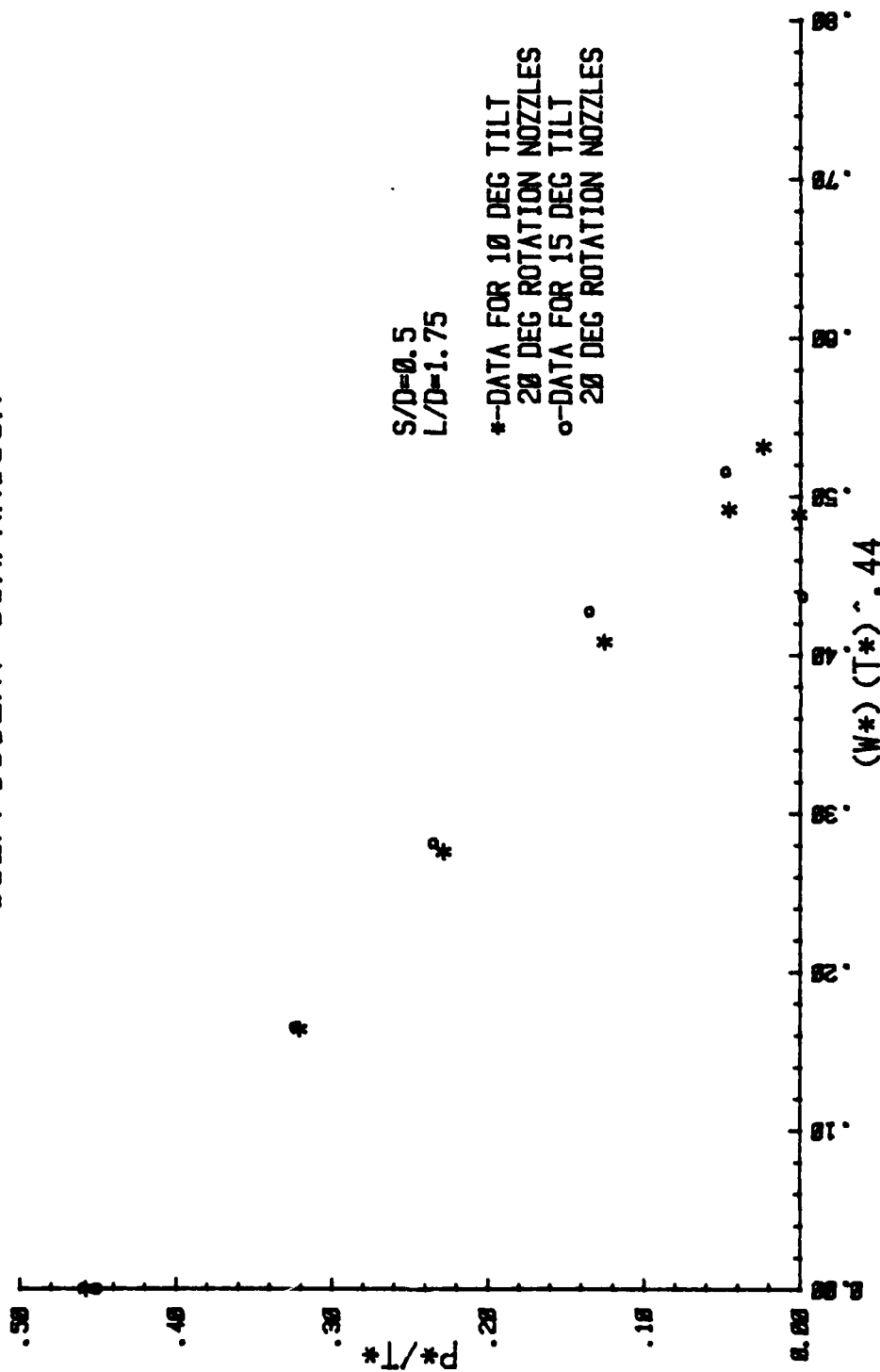


FIGURE 27.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

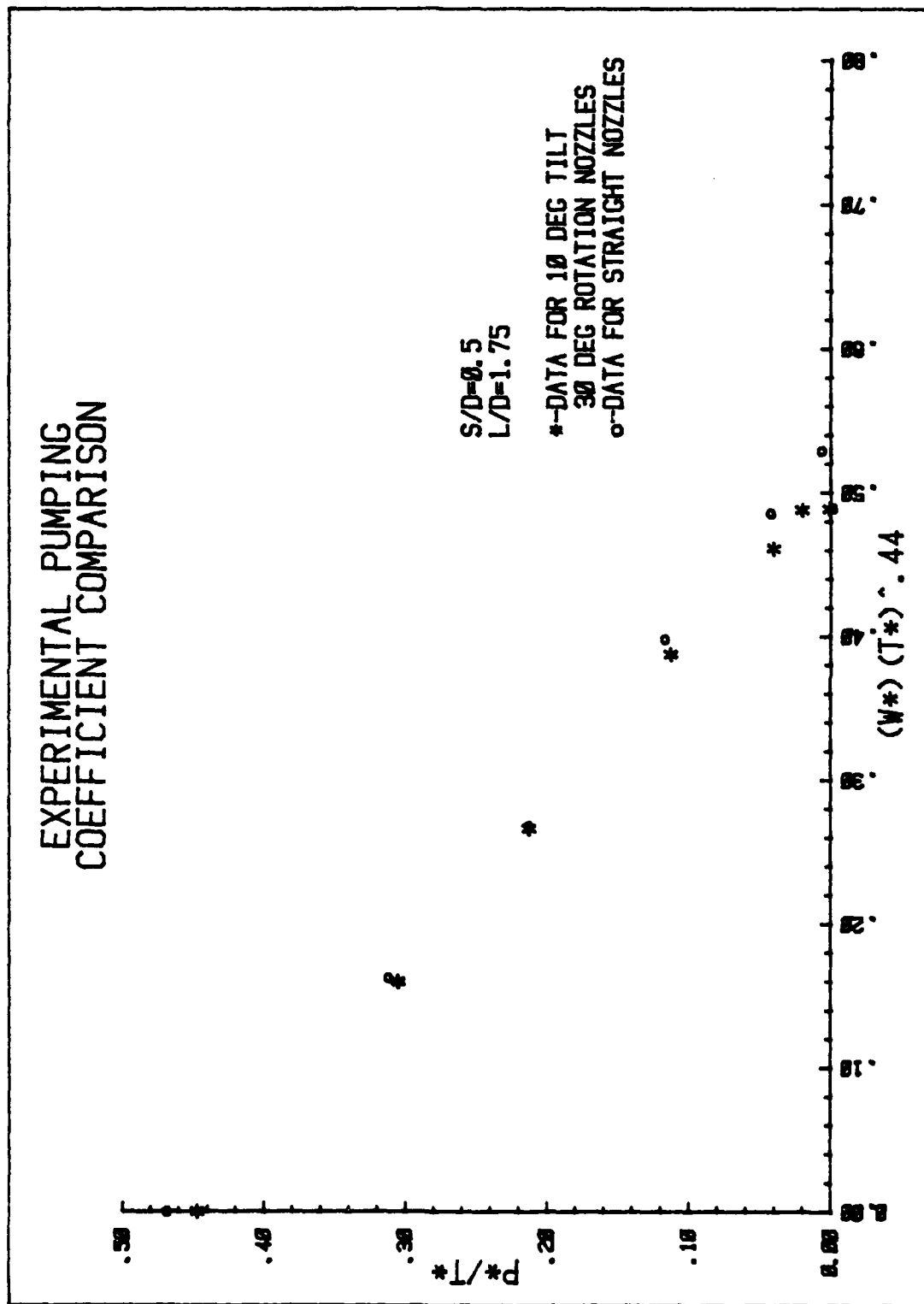


FIGURE 28

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

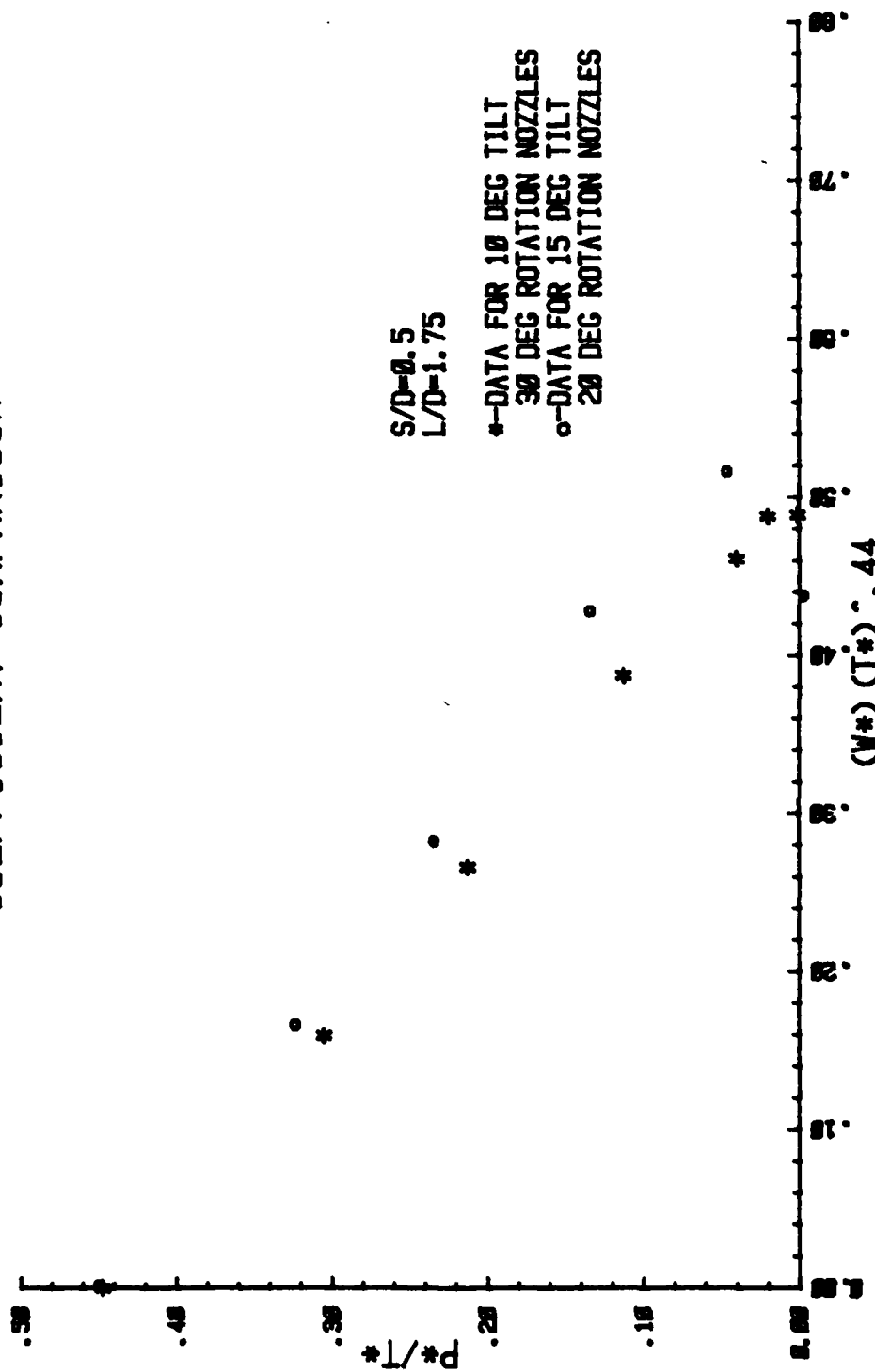


FIGURE 28.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

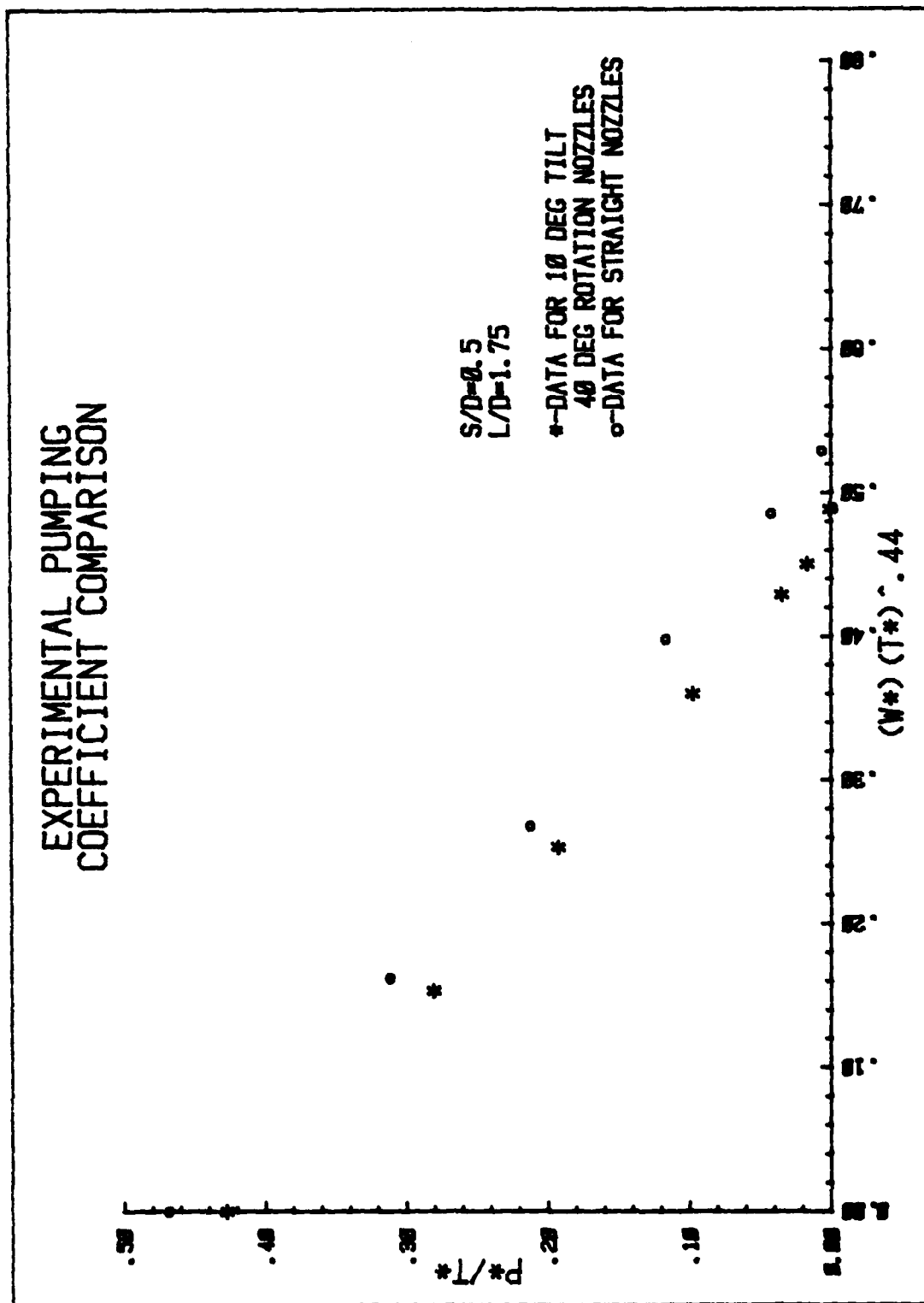


FIGURE 29

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

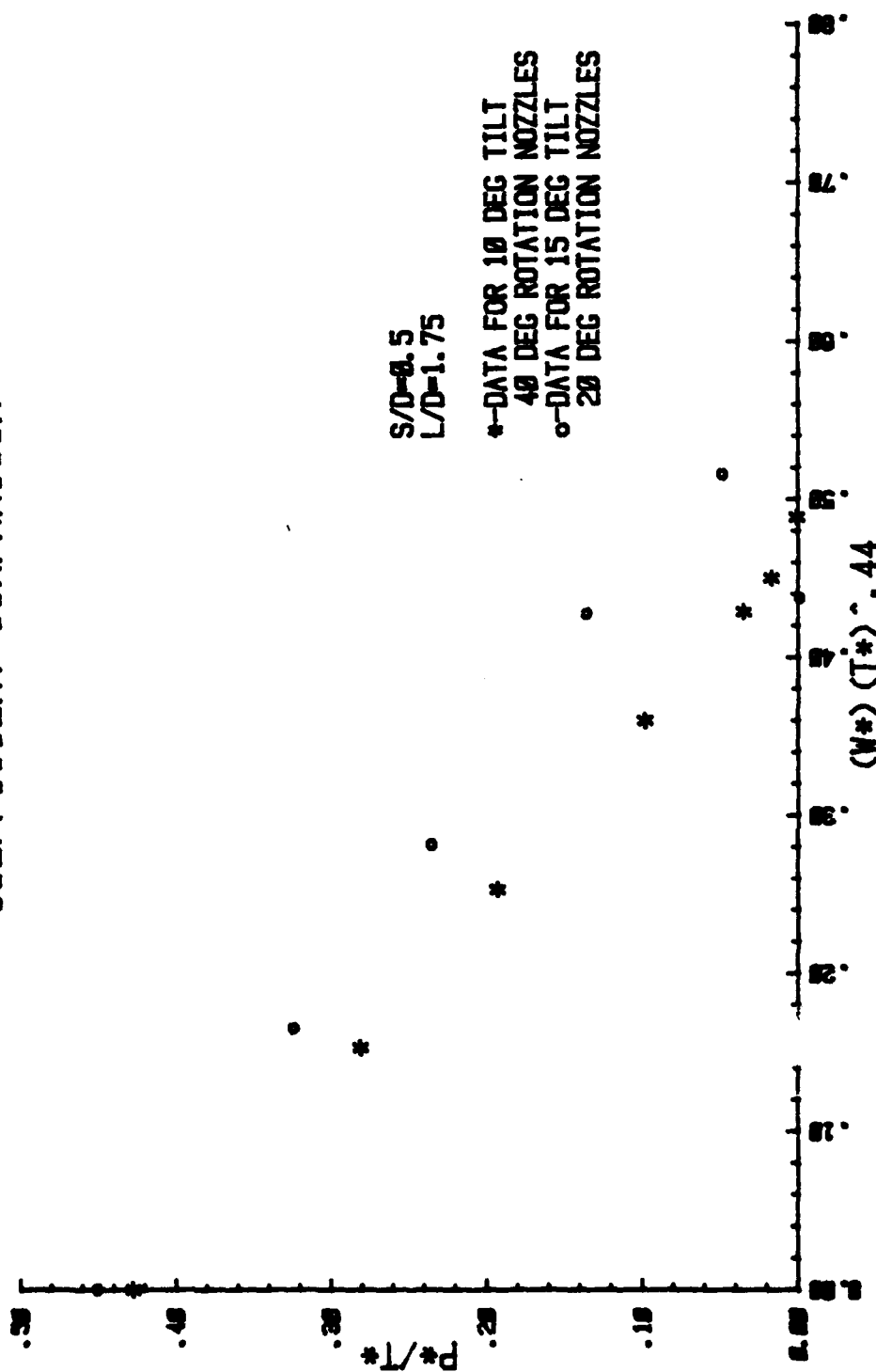


FIGURE 29.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

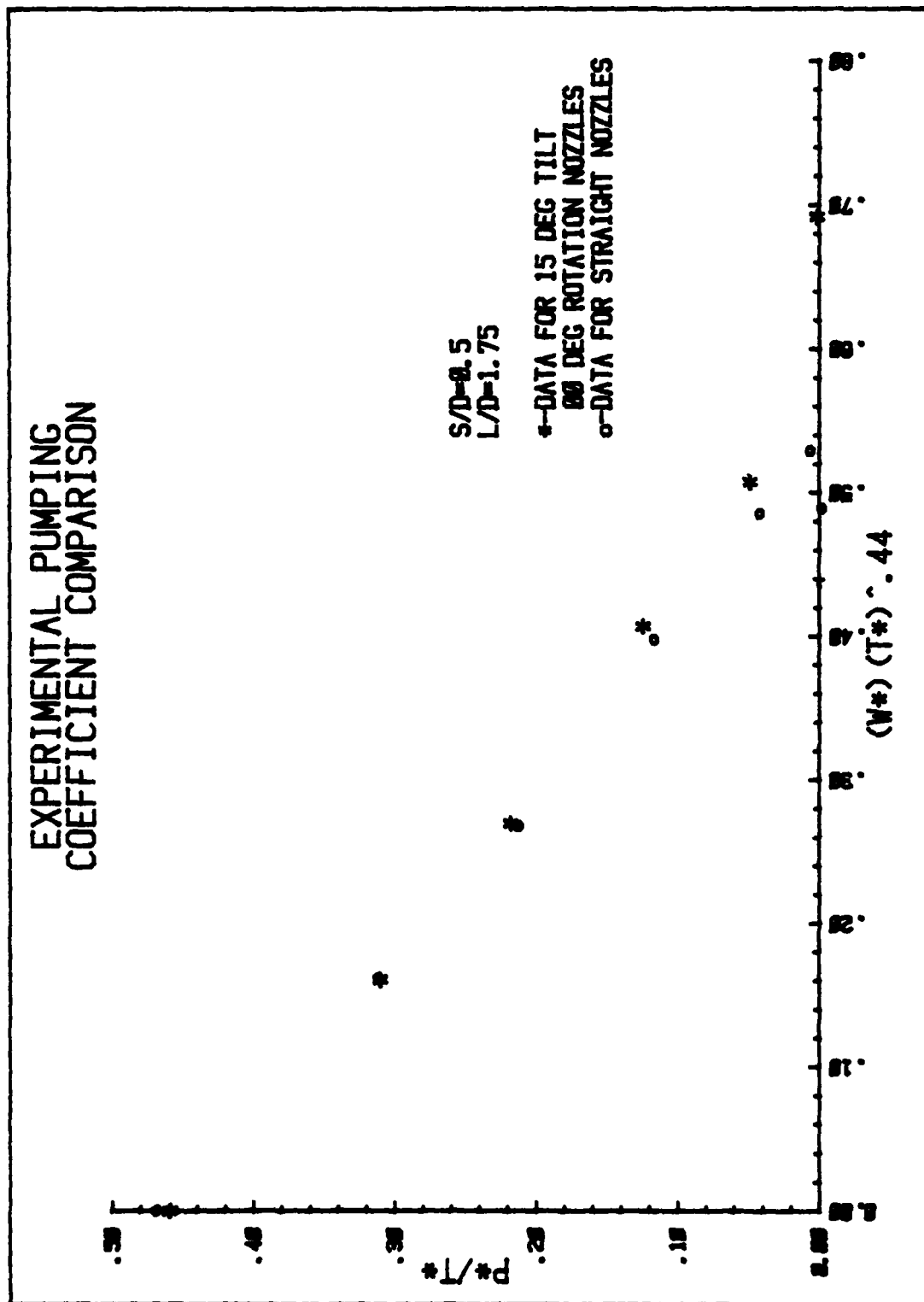


FIGURE 30



# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

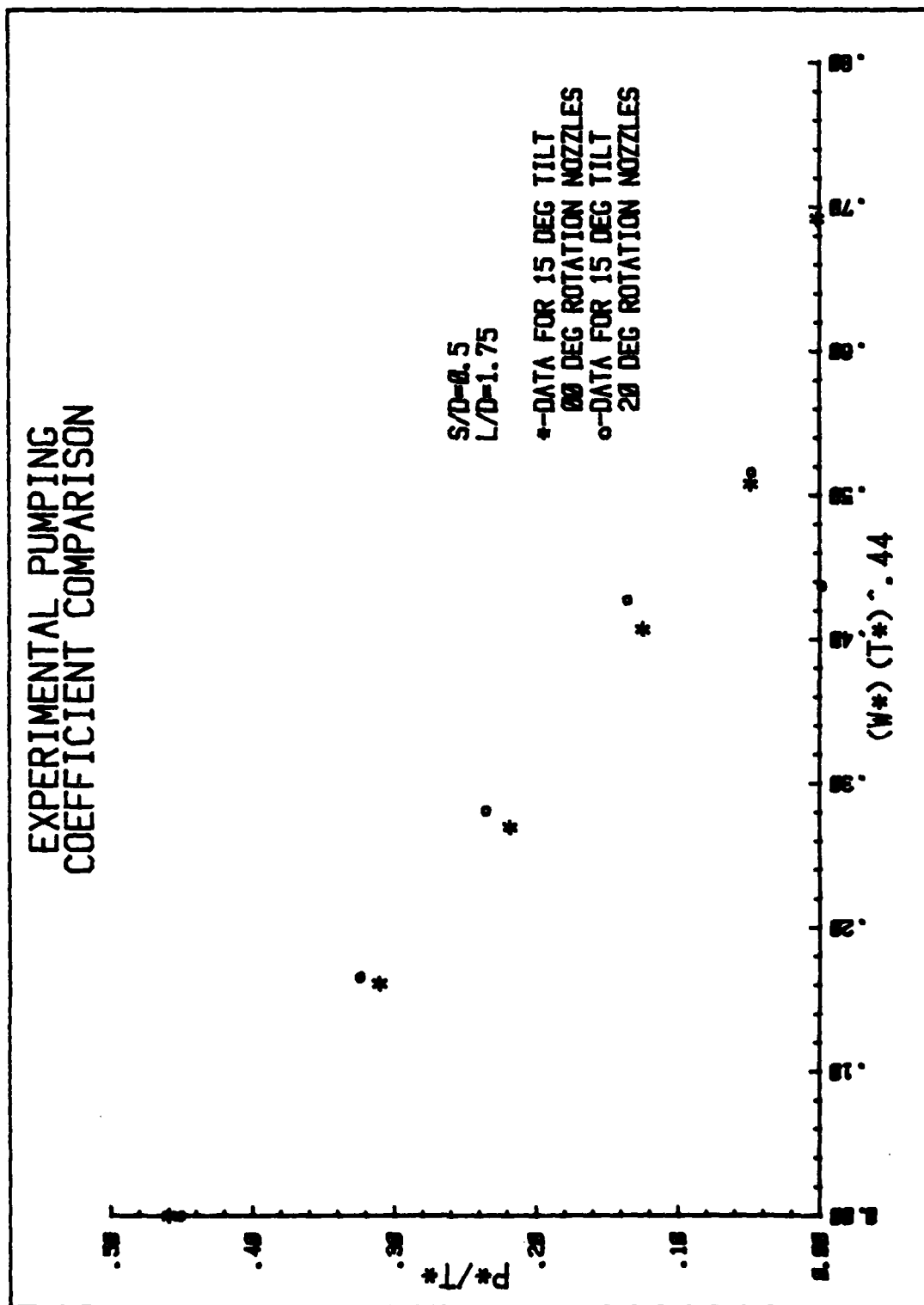


FIGURE 30.1

# AXIAL PRESSURE DISTRIBUTION COMPARISON

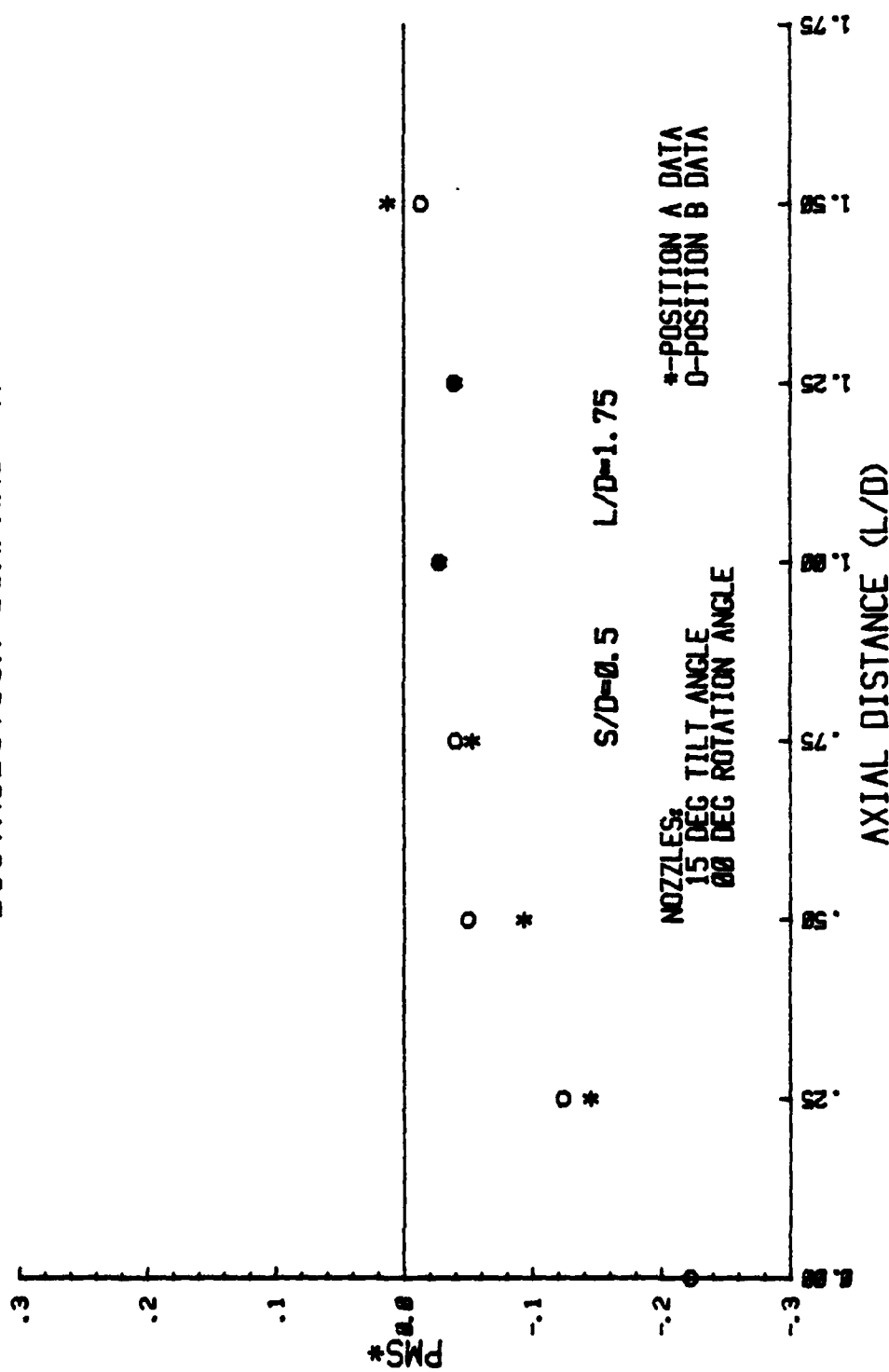


FIGURE 30.2

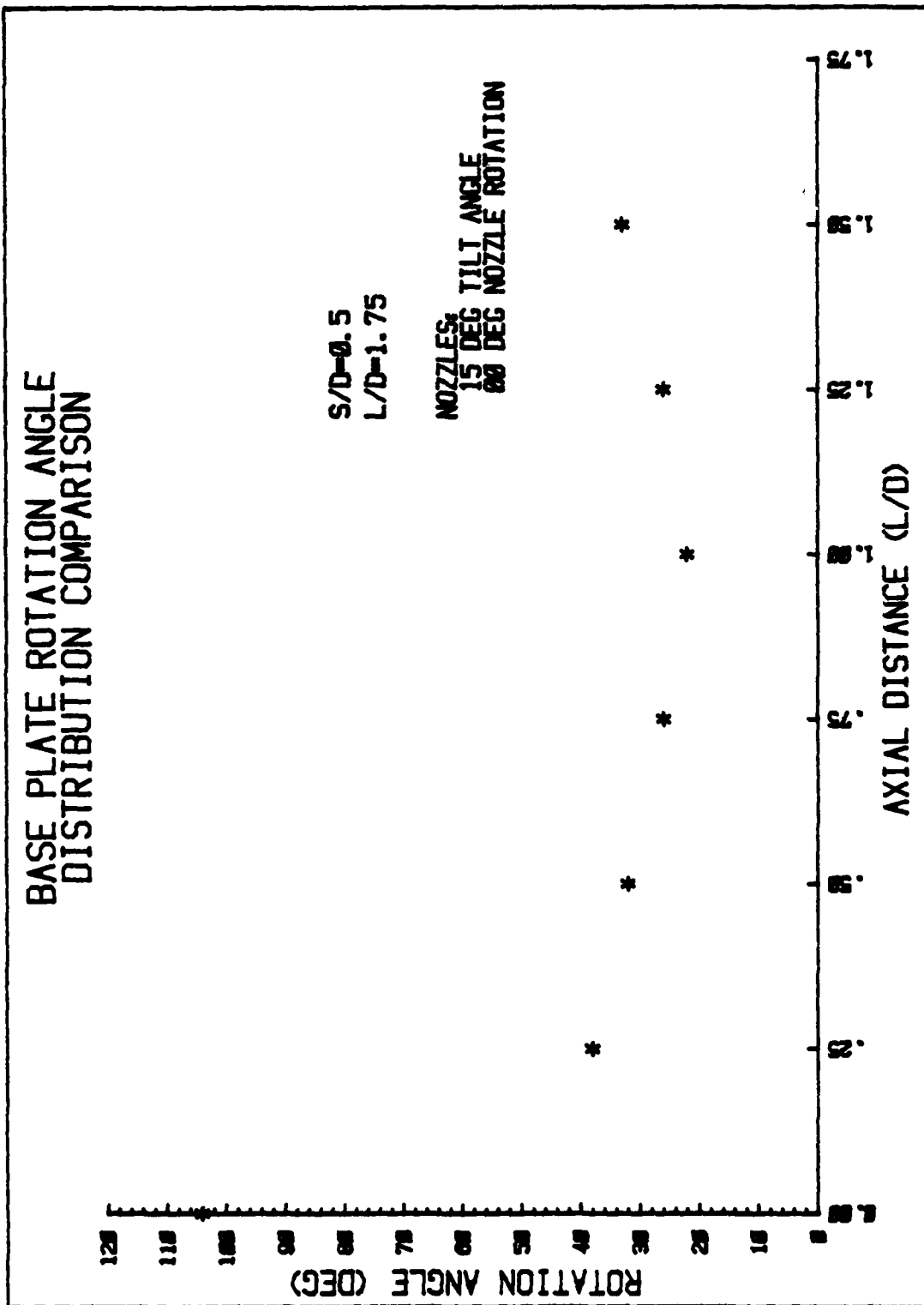


FIGURE 30.3

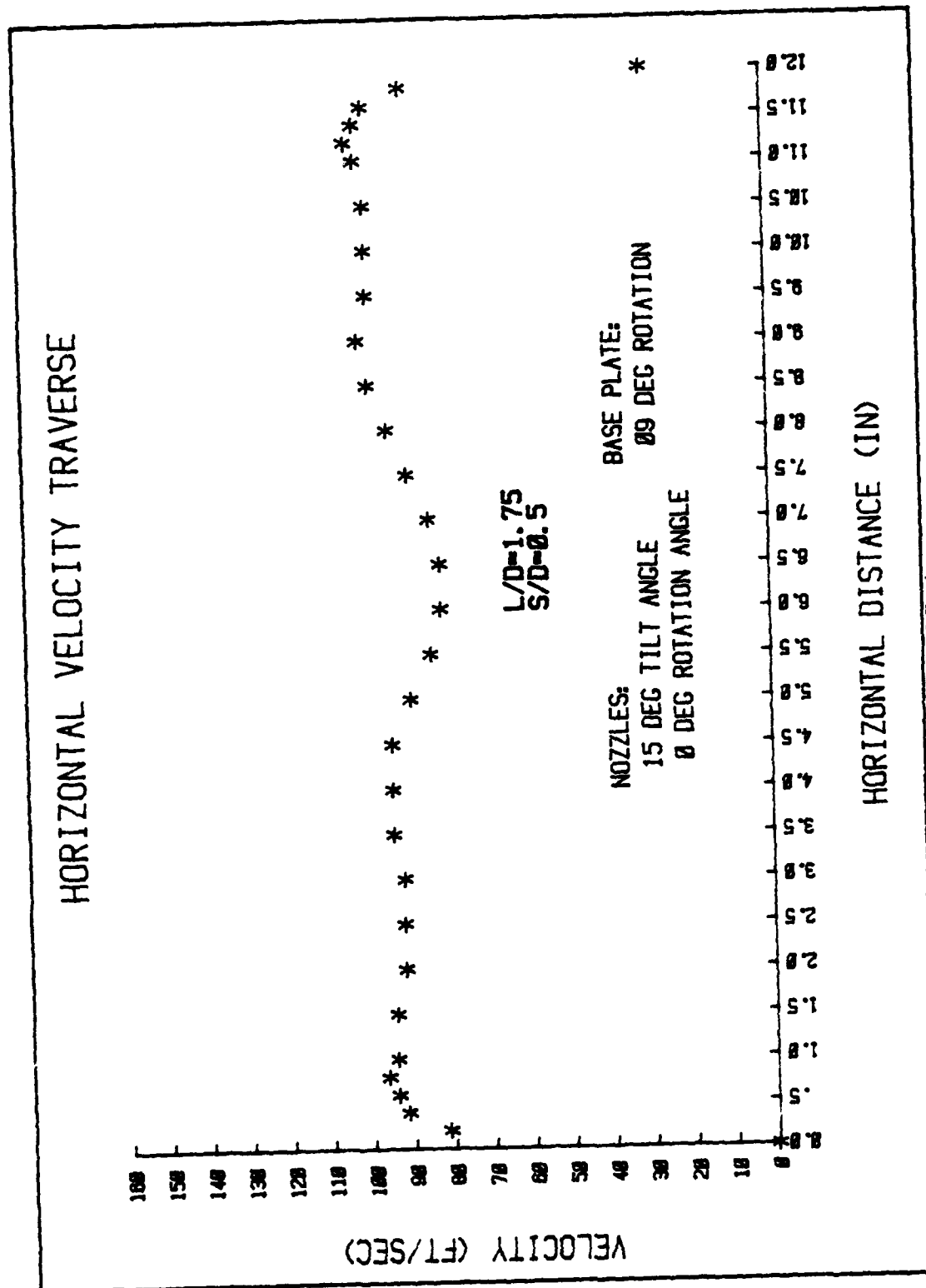


FIGURE 30.4

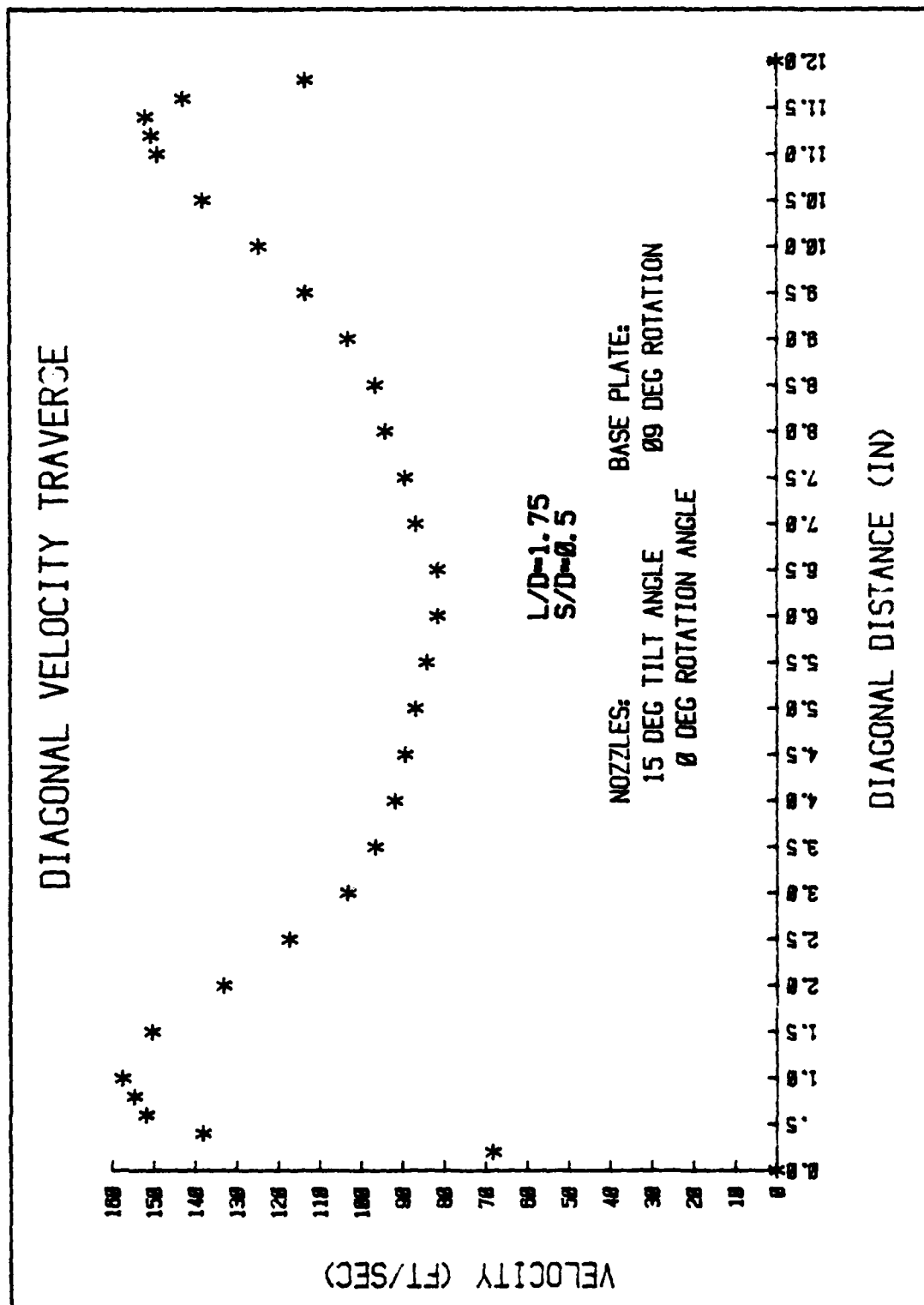


FIGURE 30.5

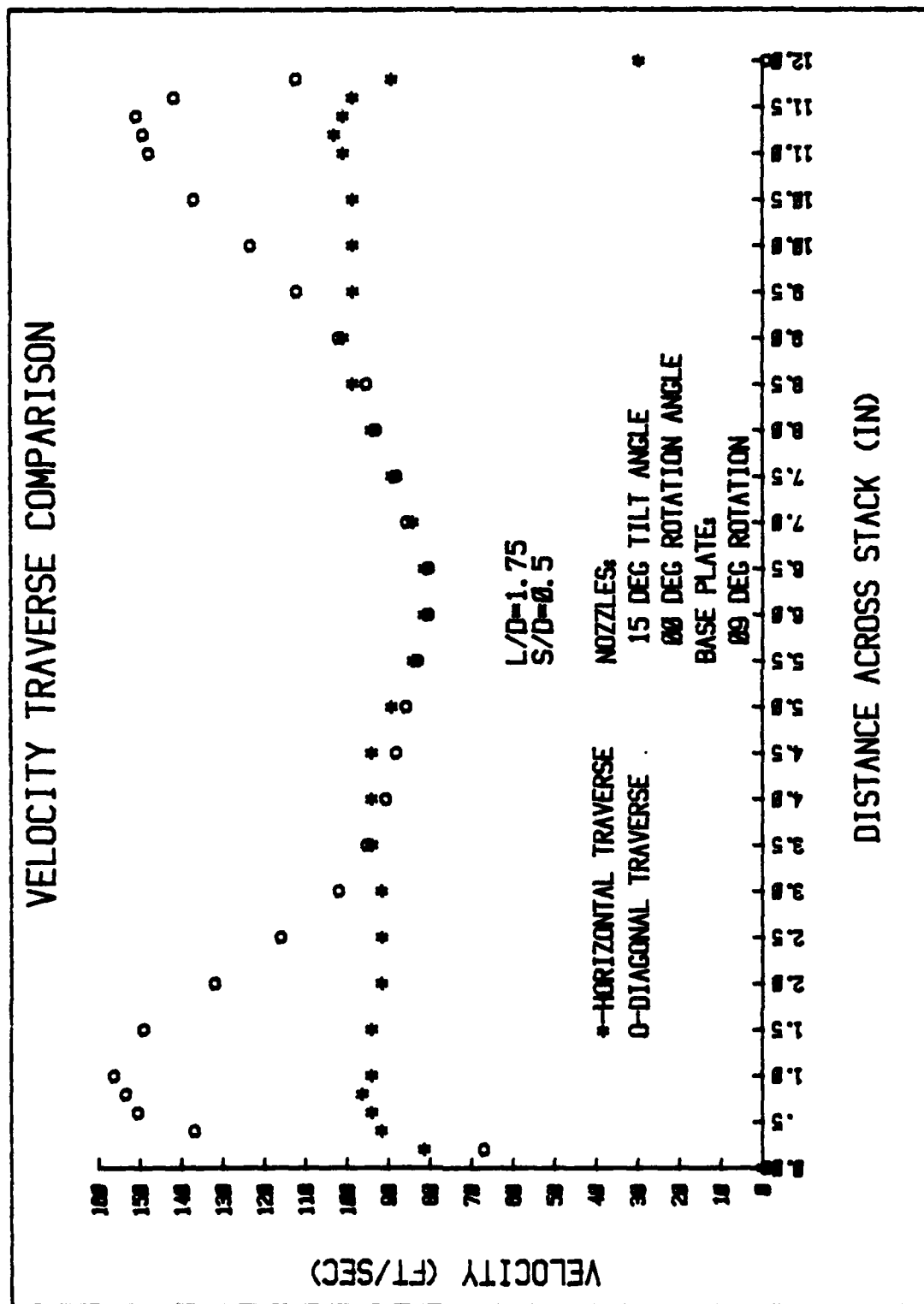


FIGURE 30.6

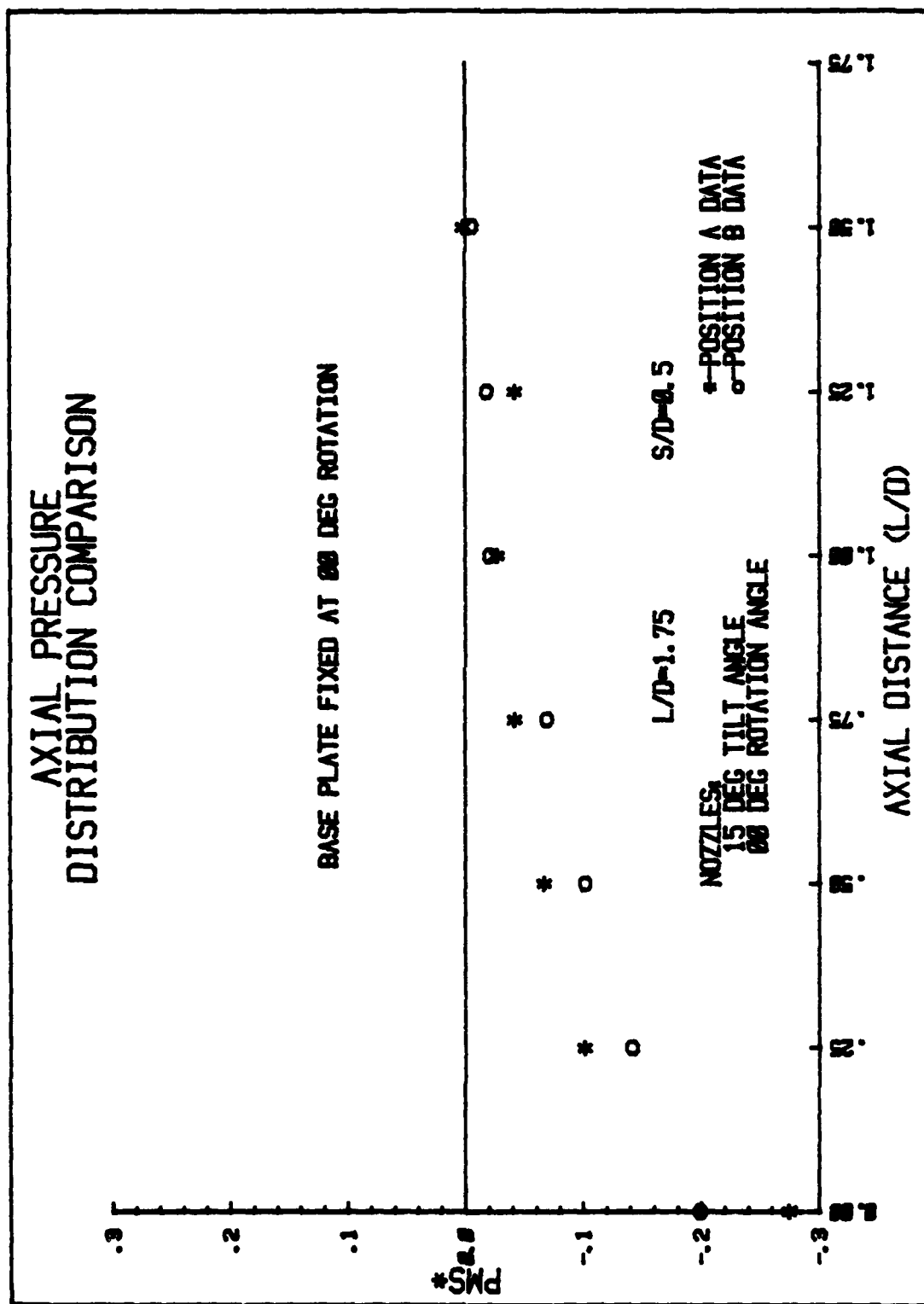


FIGURE 31

# AXIAL PRESSURE DISTRIBUTION COMPARISON

BASE PLATE FIXED AT THE FIRST PEAK POSITION A READING

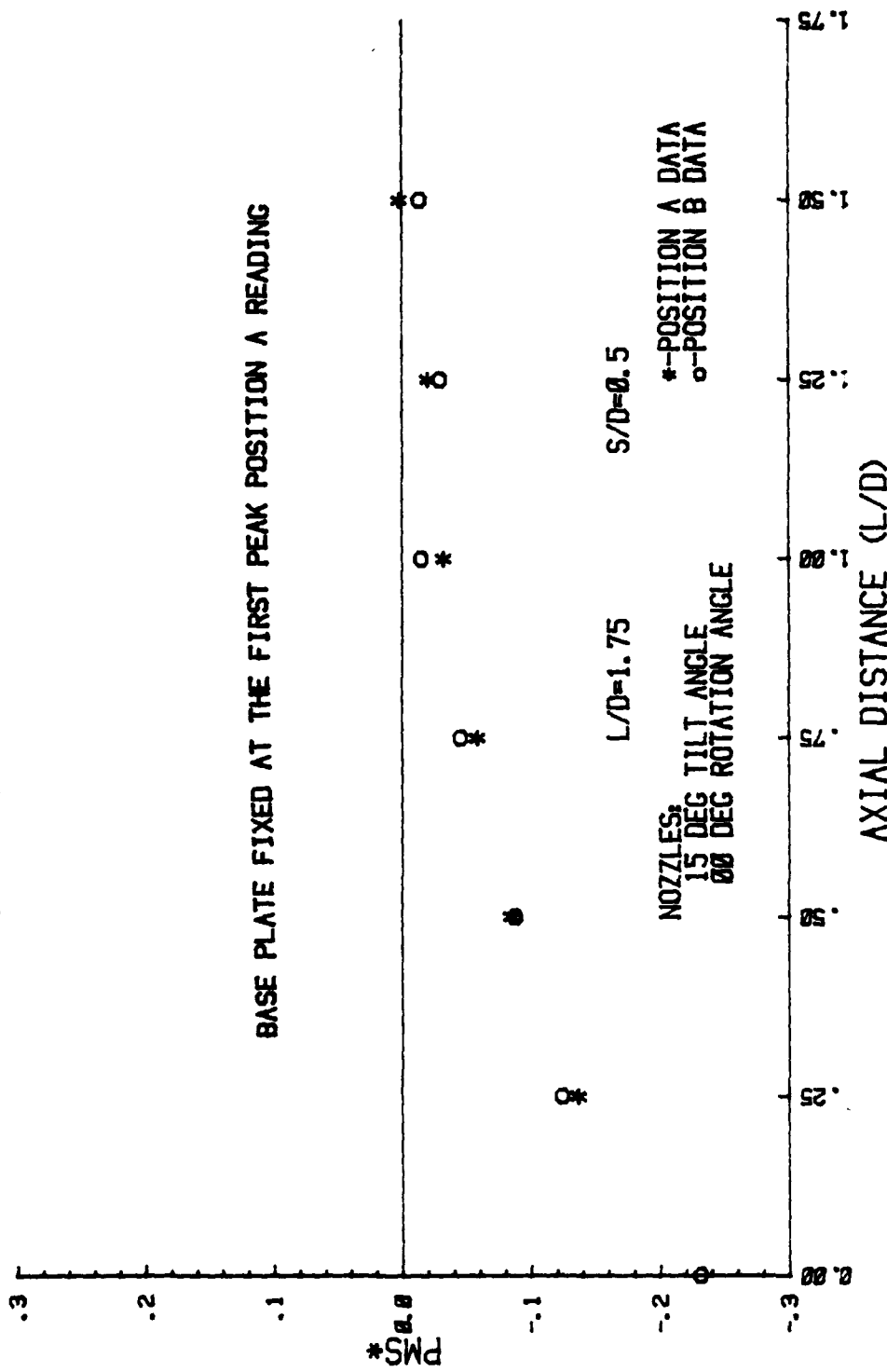


FIGURE 32



# AXIAL PRESSURE DISTRIBUTION COMPARISON

BASE PLATE ROTATED FOR PEAK POSITION A READINGS

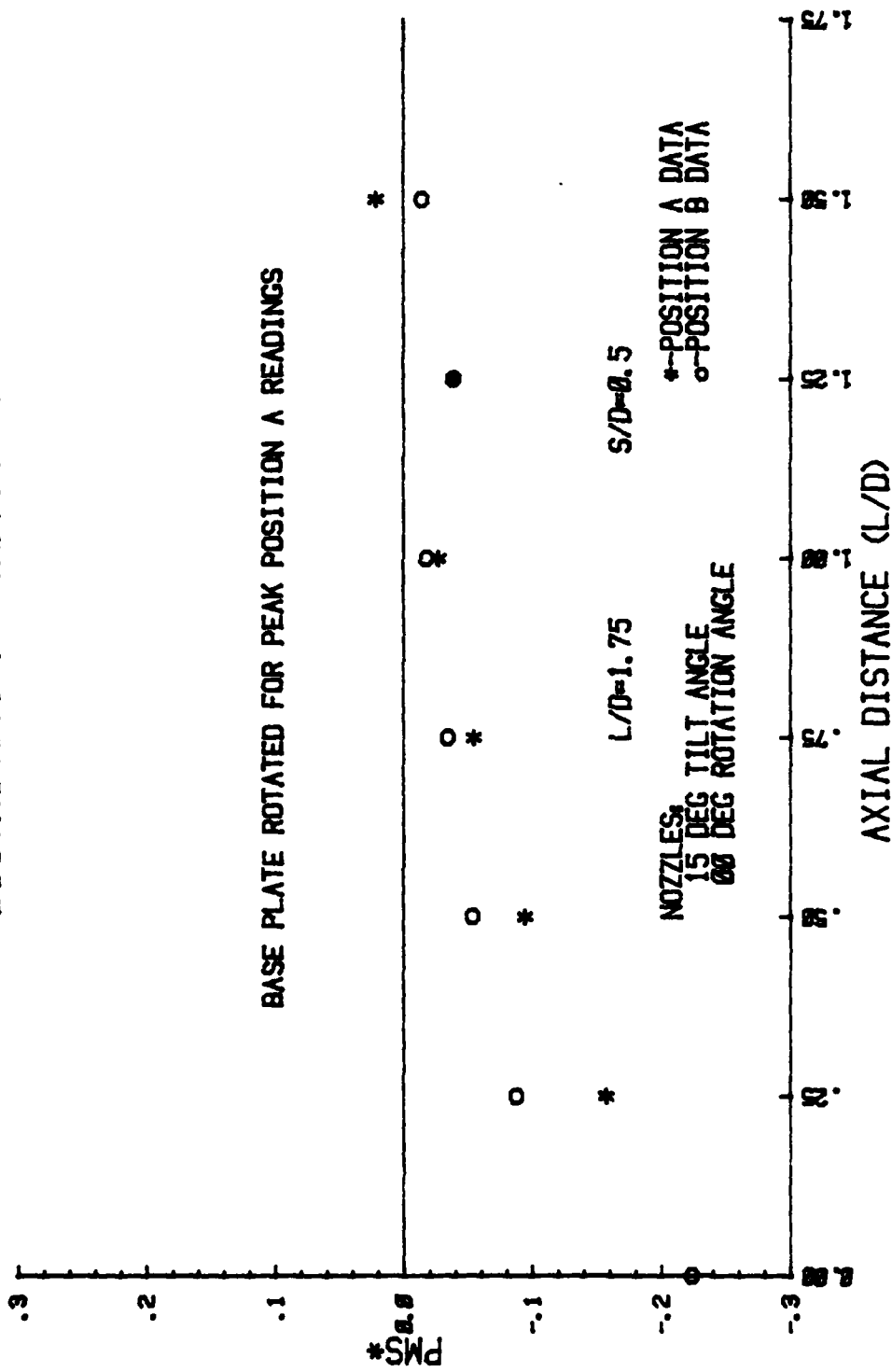


FIGURE 33

# AXIAL PRESSURE DISTRIBUTION COMPARISON

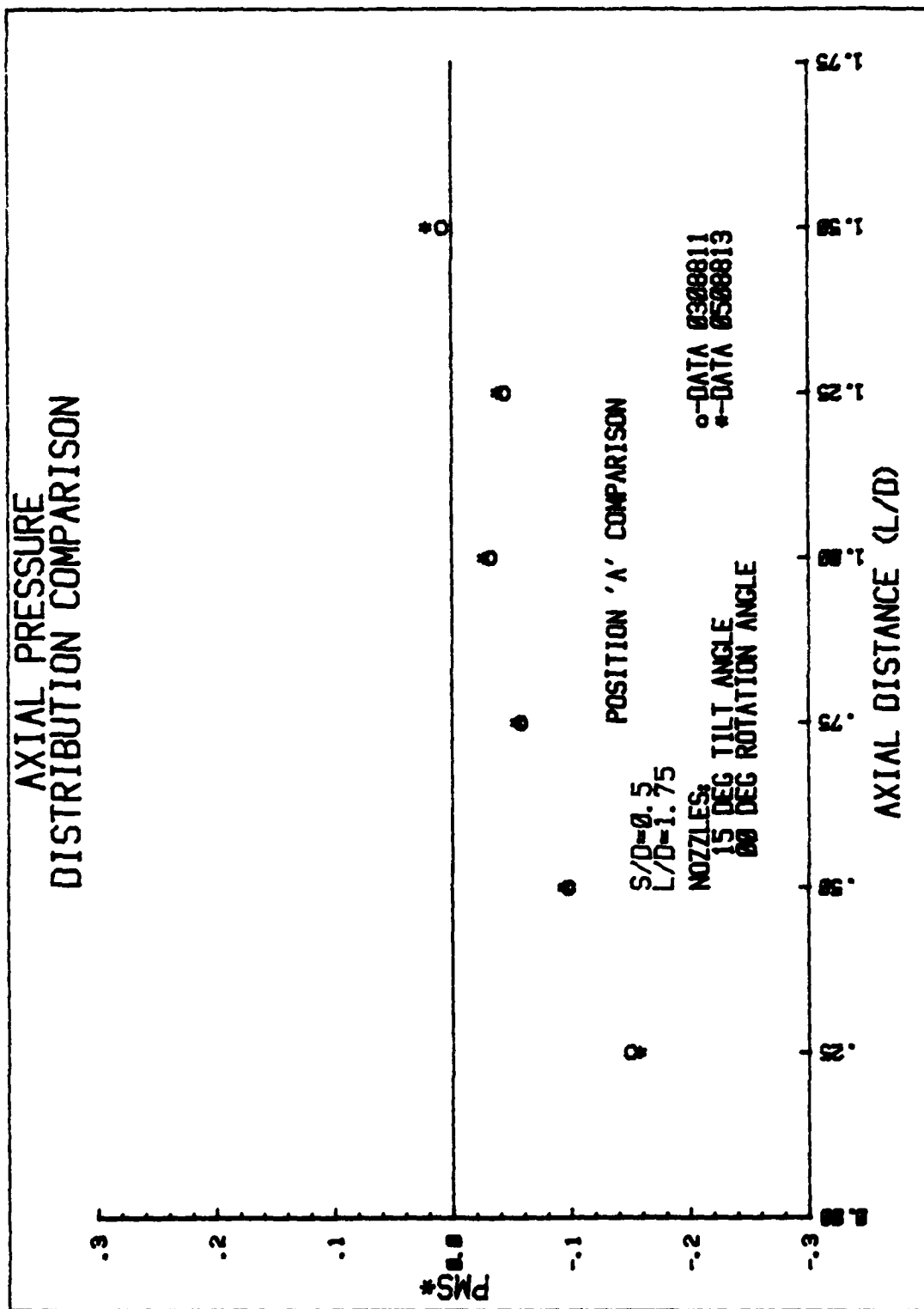


FIGURE 33.1

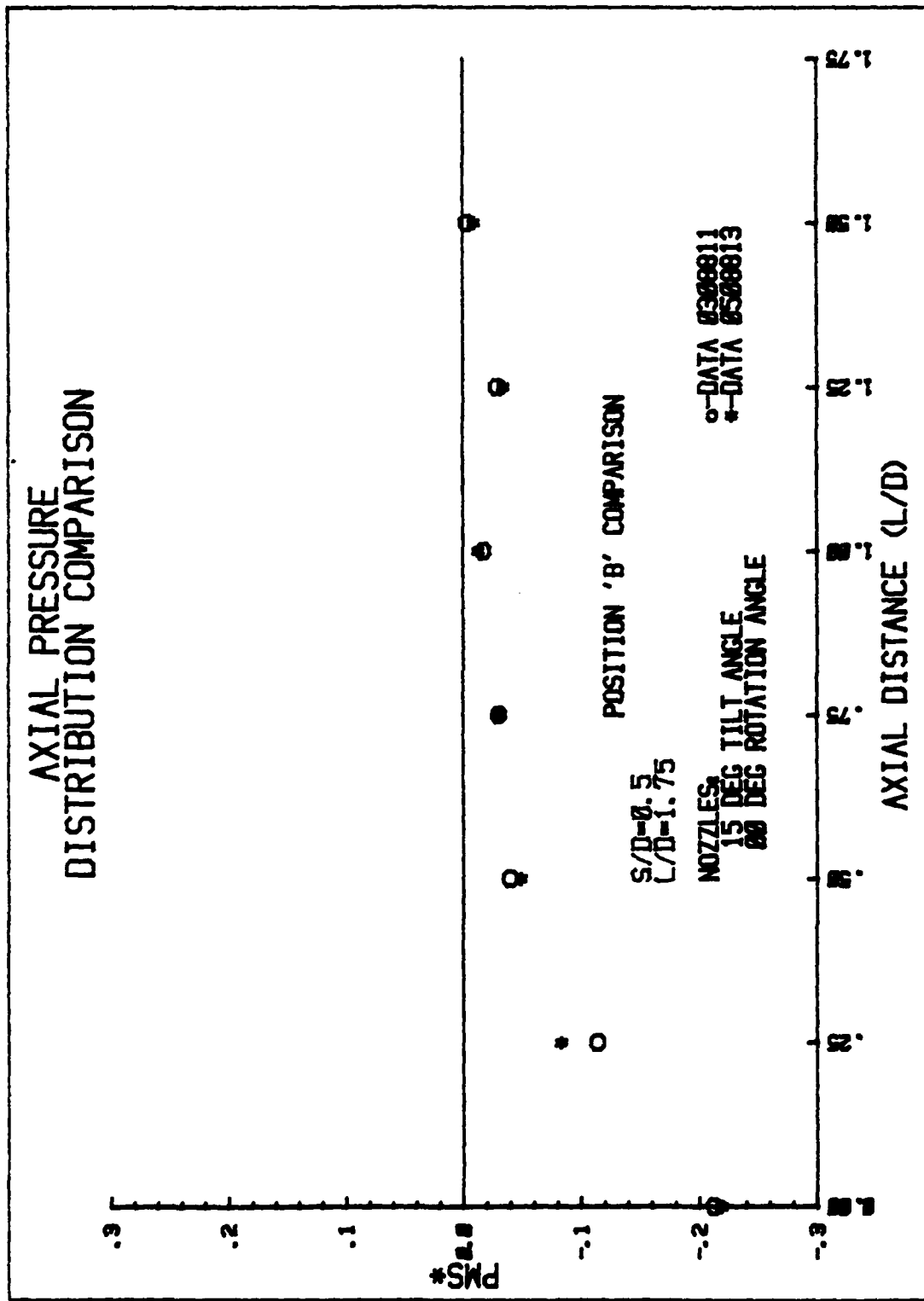


FIGURE 33.2

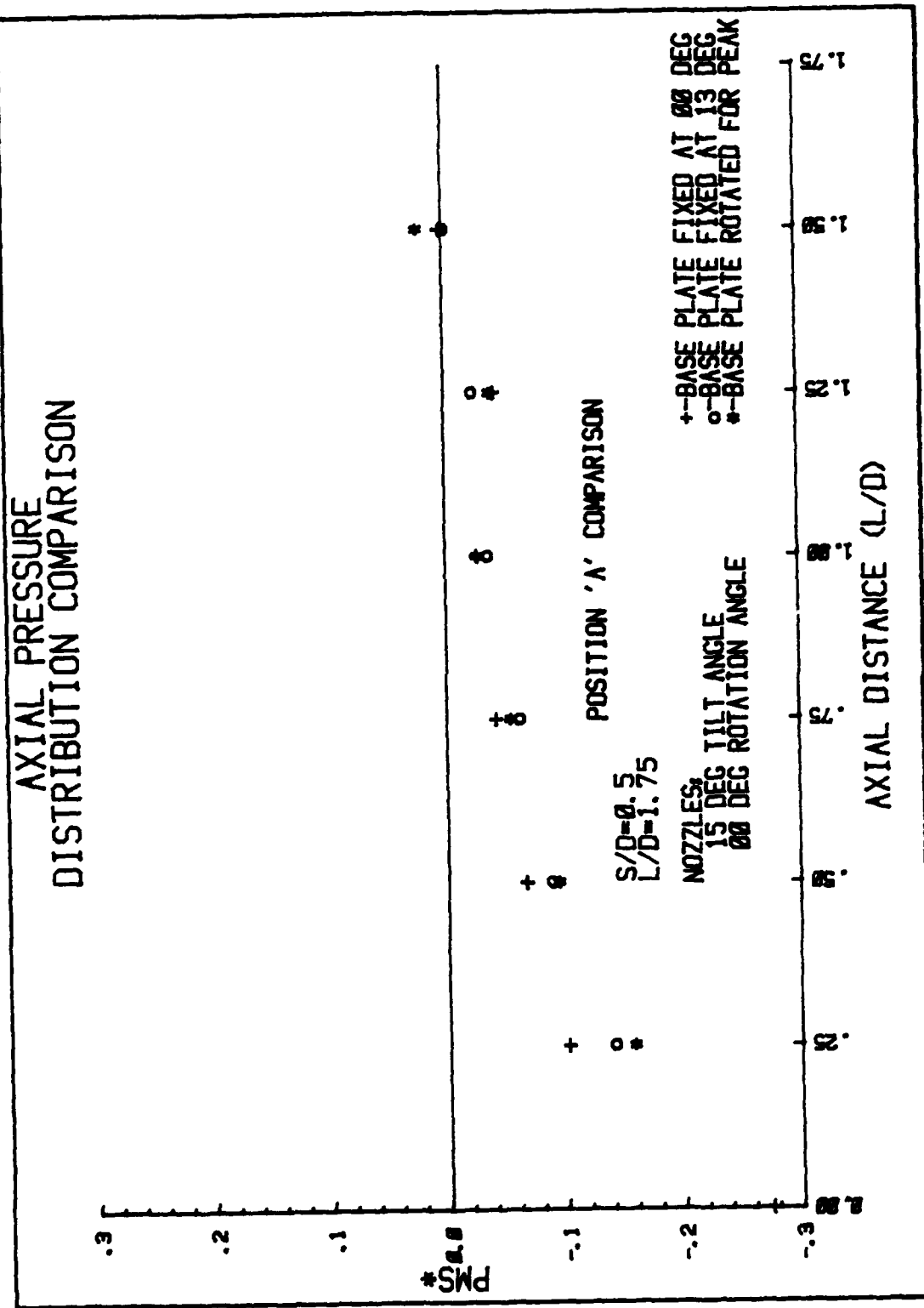


FIGURE 33.3

# AXIAL PRESSURE DISTRIBUTION COMPARISON

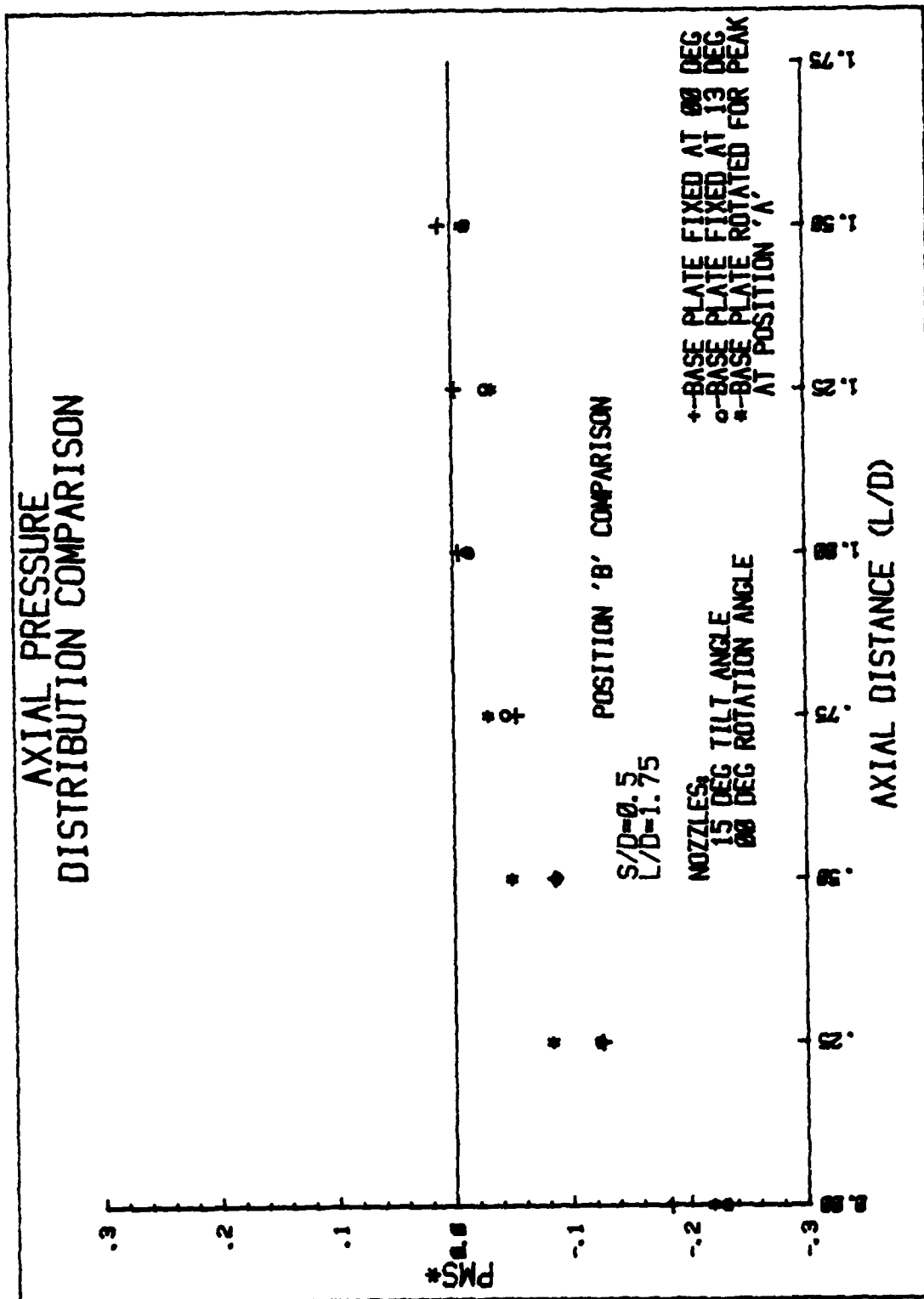


FIGURE 33.4

# AXIAL PRESSURE DISTRIBUTION COMPARISON

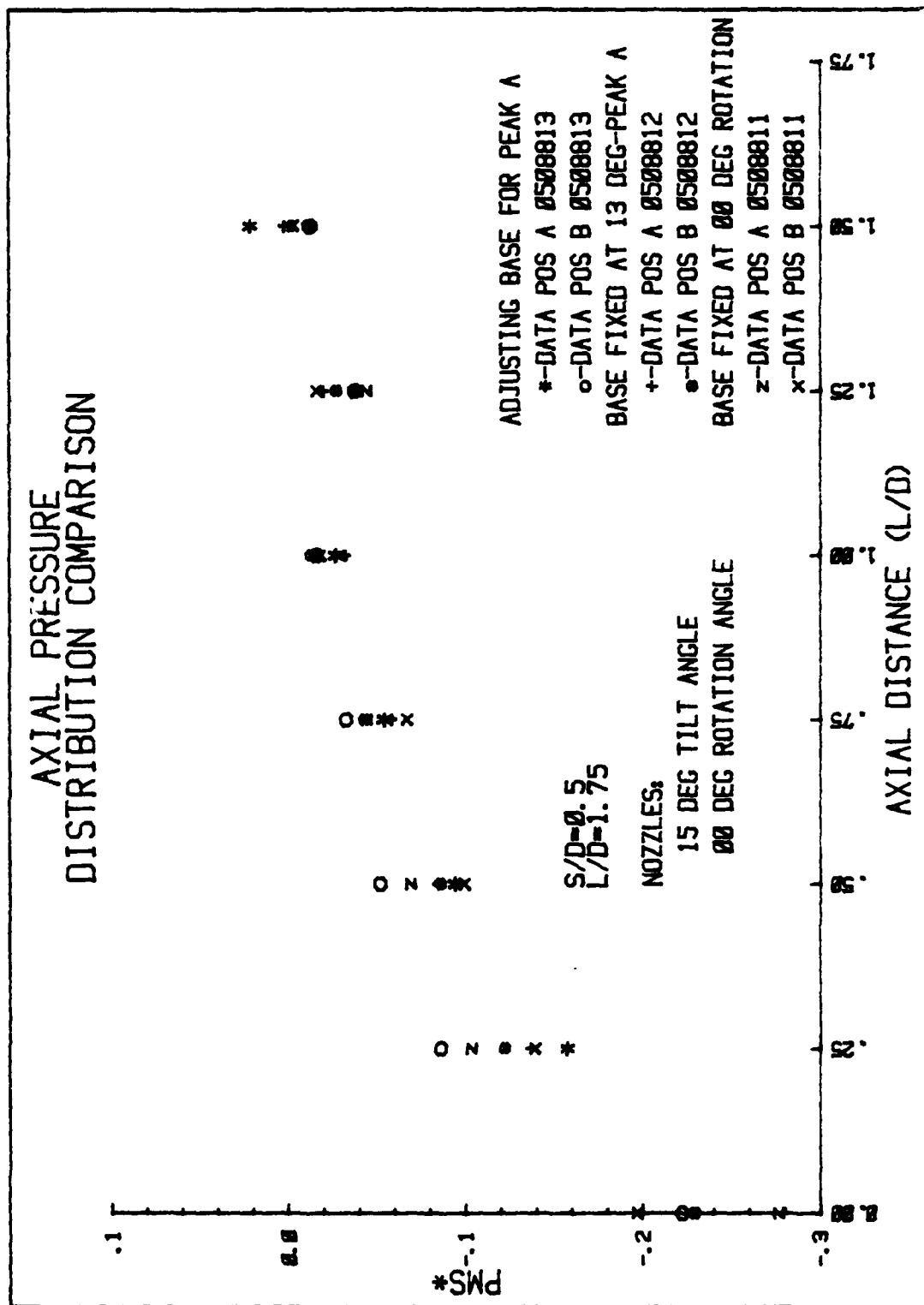


FIGURE 33.5

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

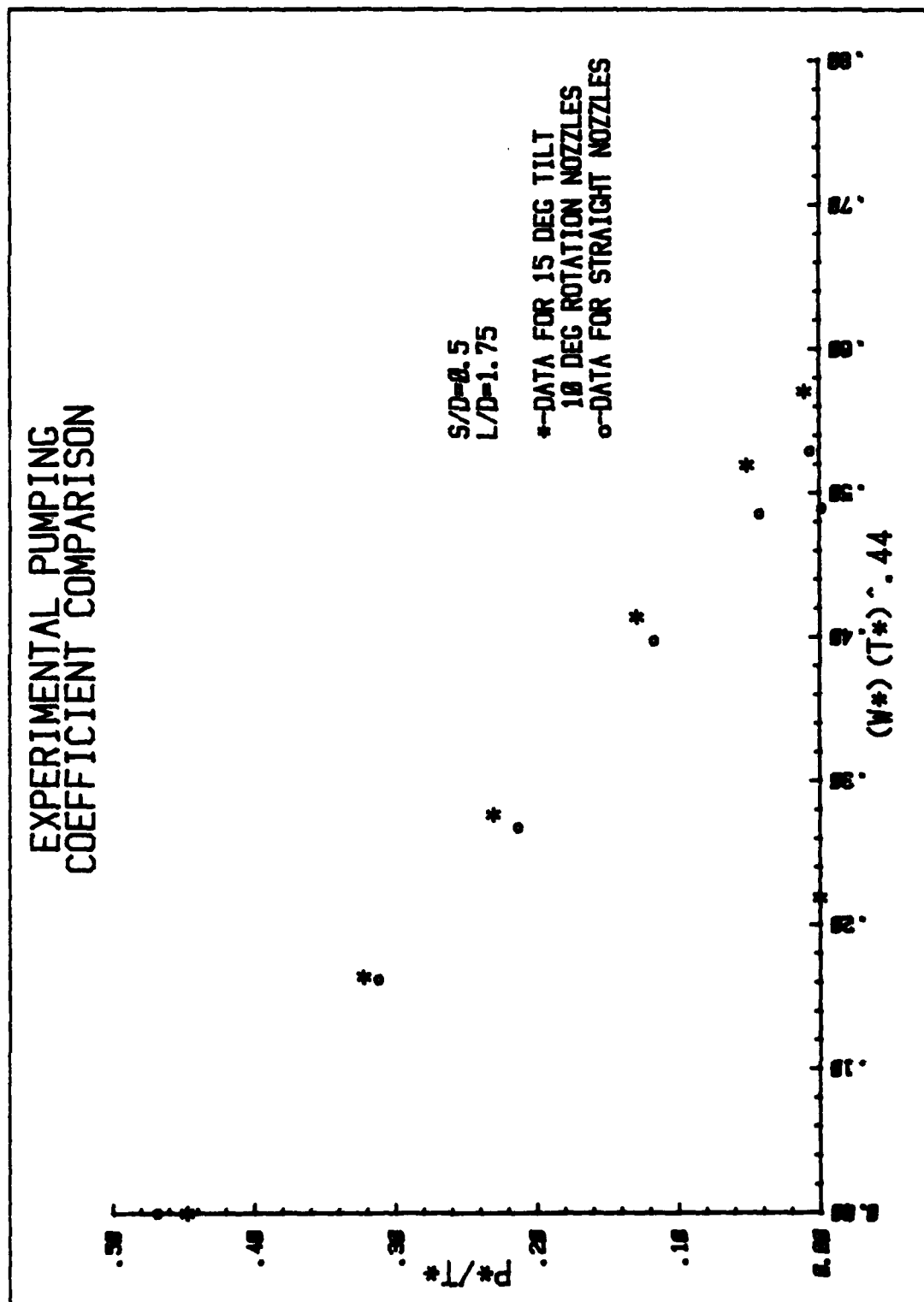


FIGURE 34

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

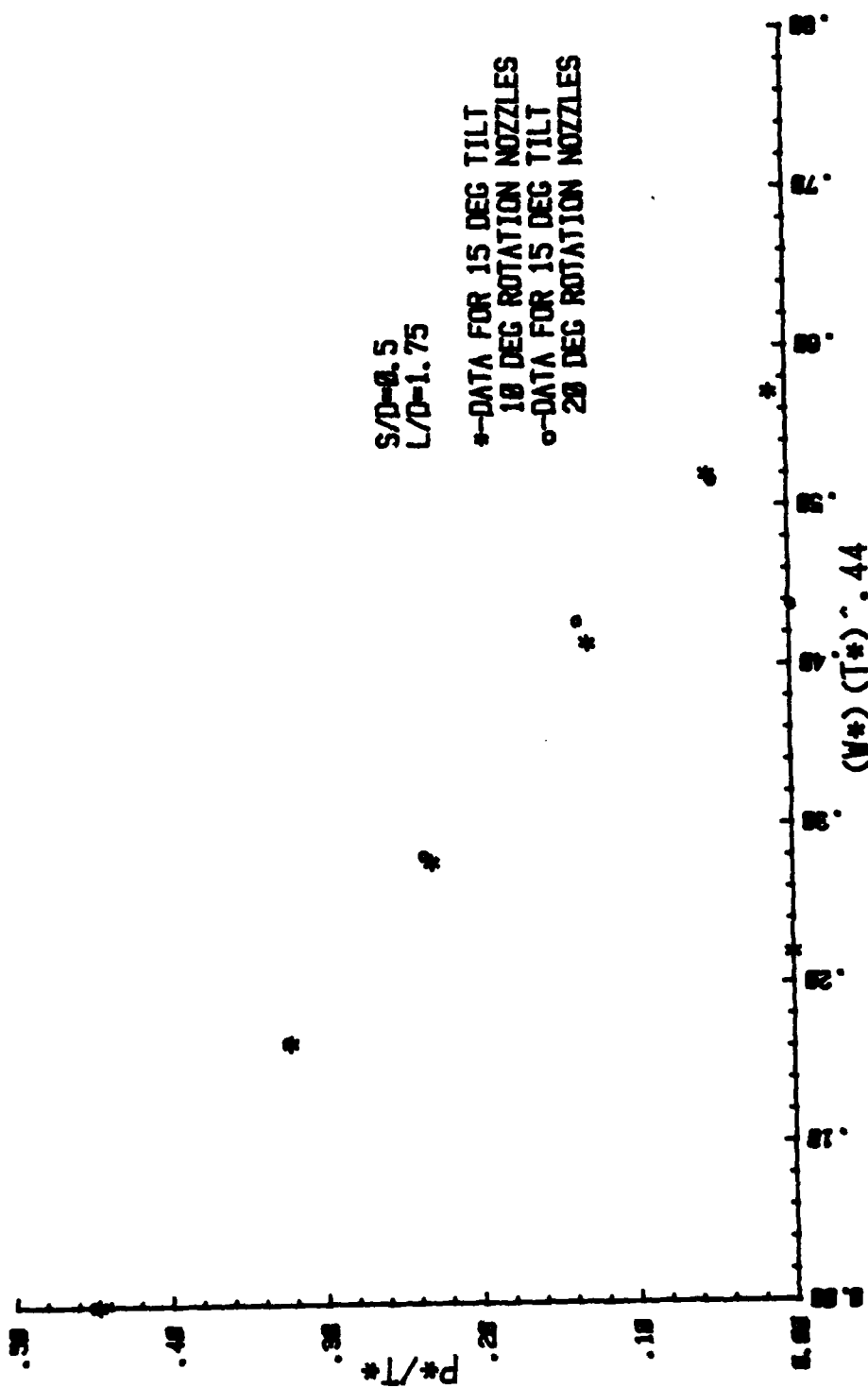


FIGURE 34.1



# AXIAL PRESSURE DISTRIBUTION COMPARISON

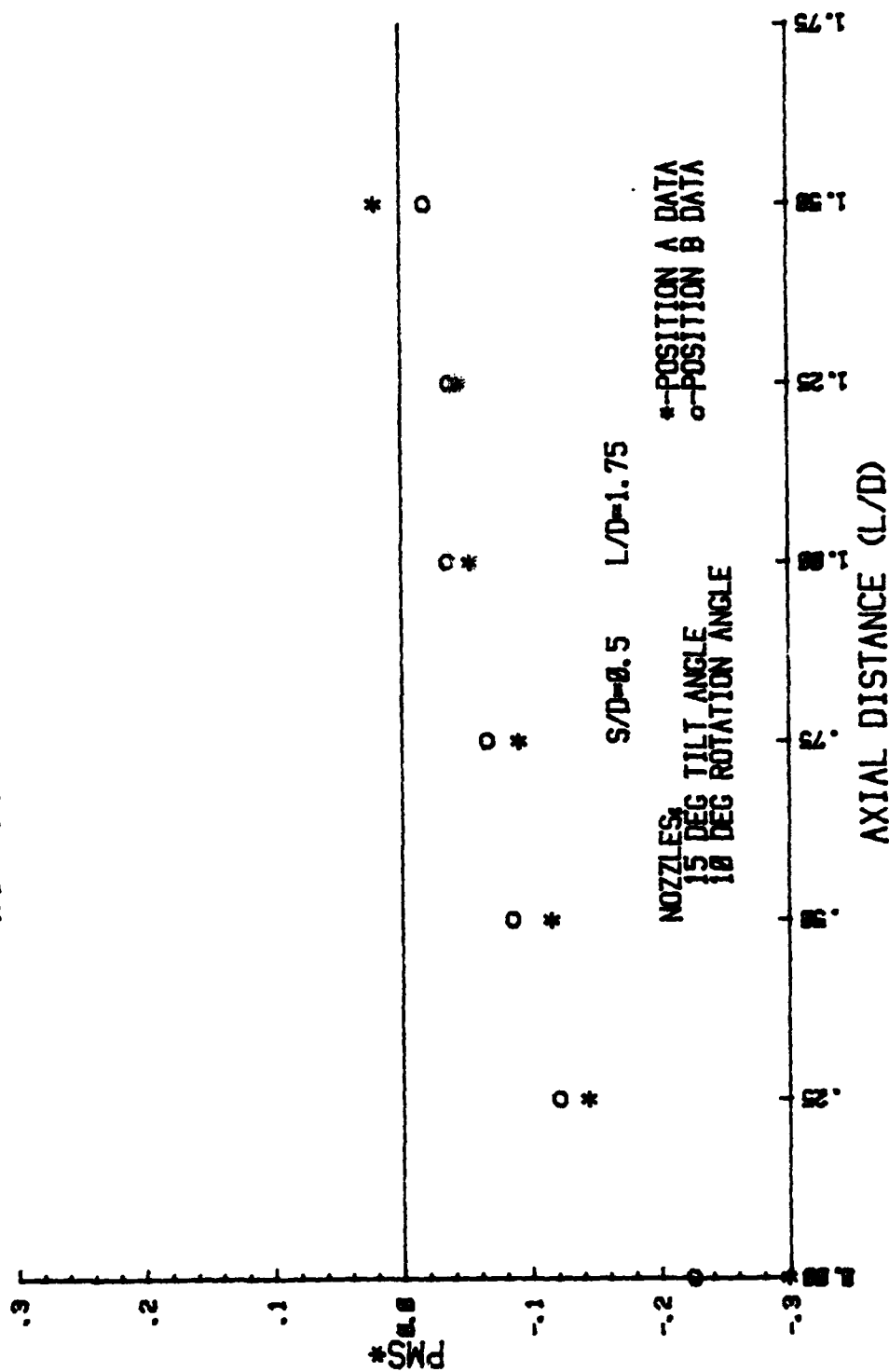


FIGURE 34.2

# BASE PLATE ROTATION ANGLE DISTRIBUTION COMPARISON

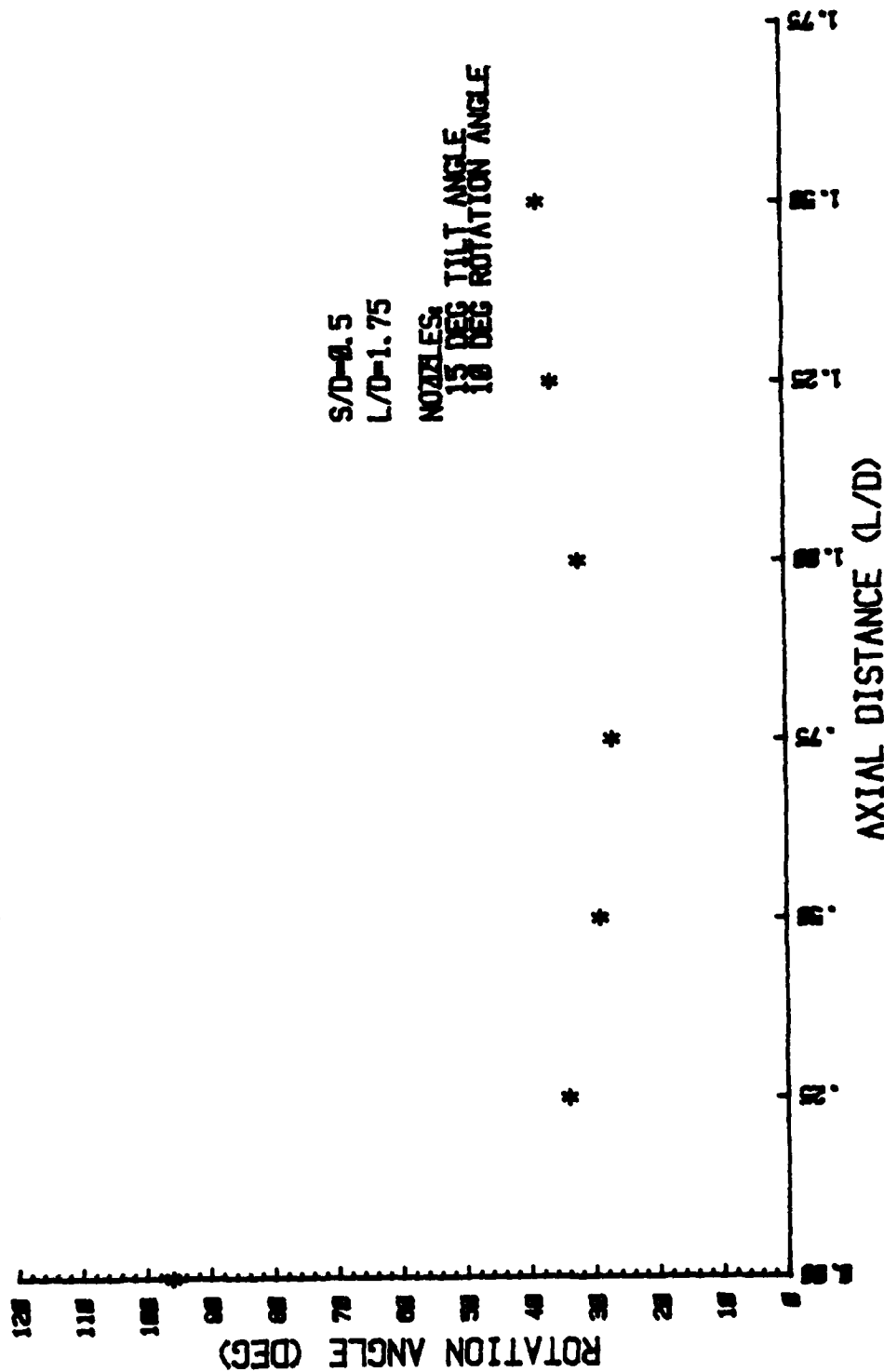


FIGURE 34.3

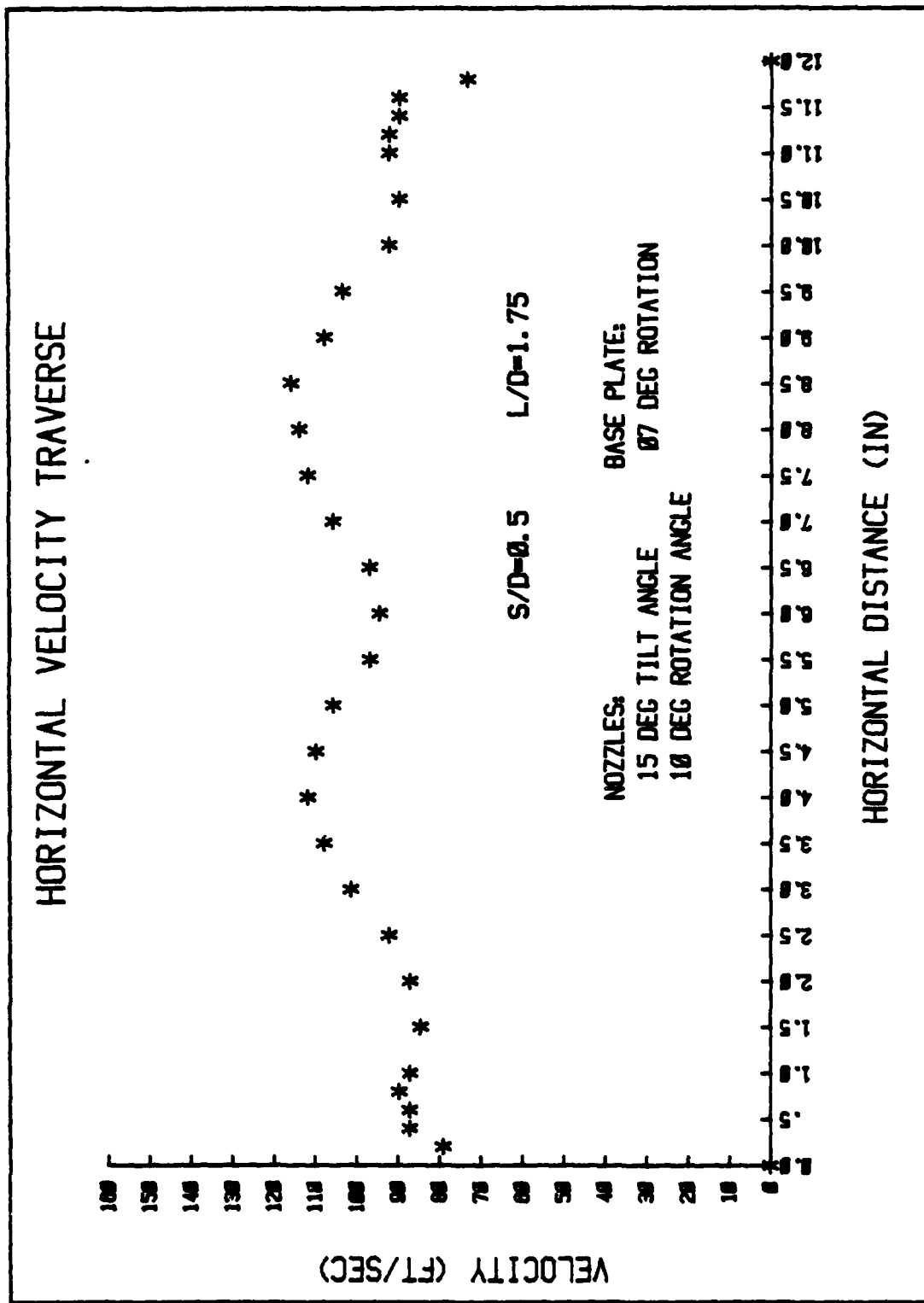
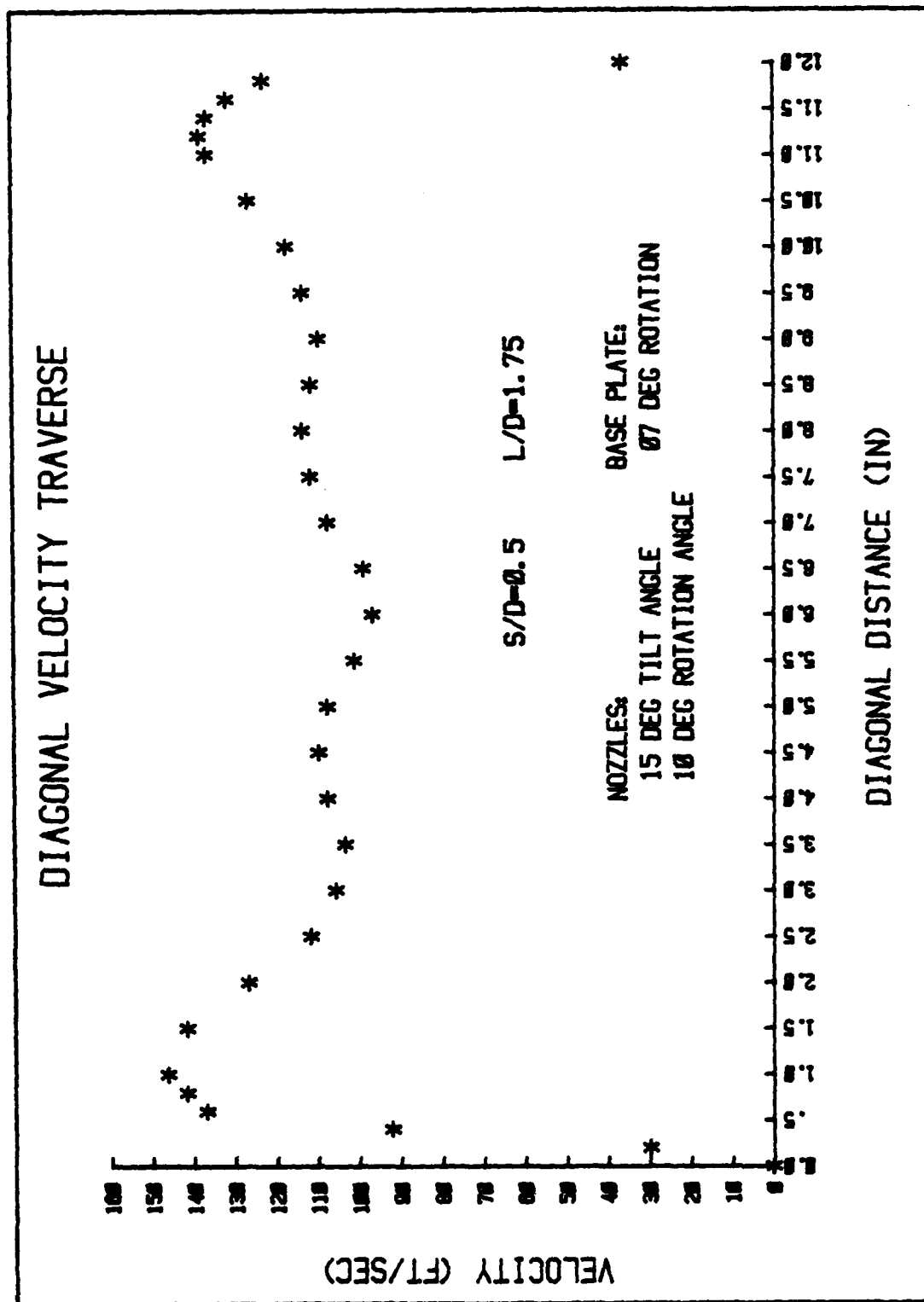


FIGURE 34.4



**FIGURE 34.5**

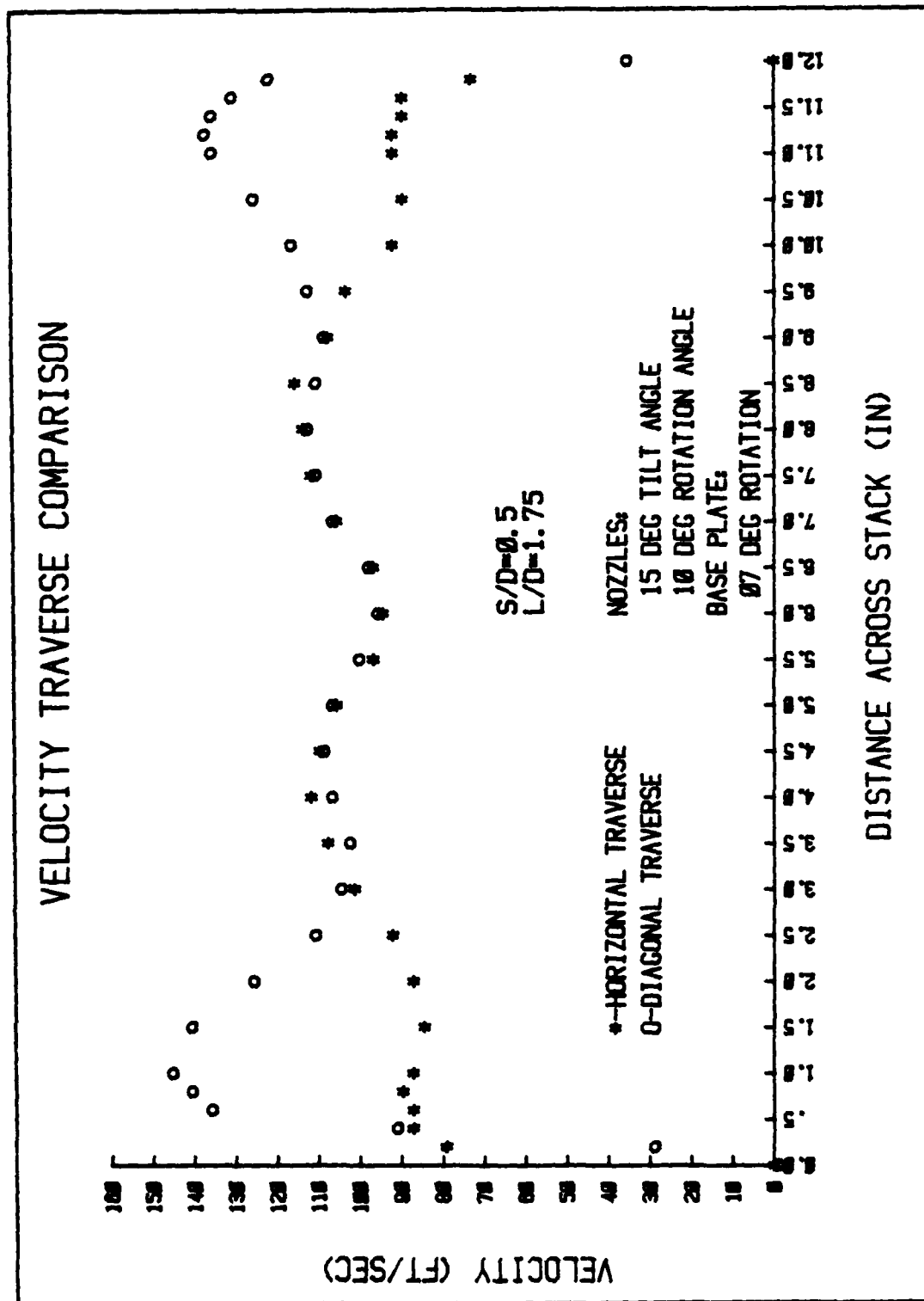


FIGURE 34.6

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

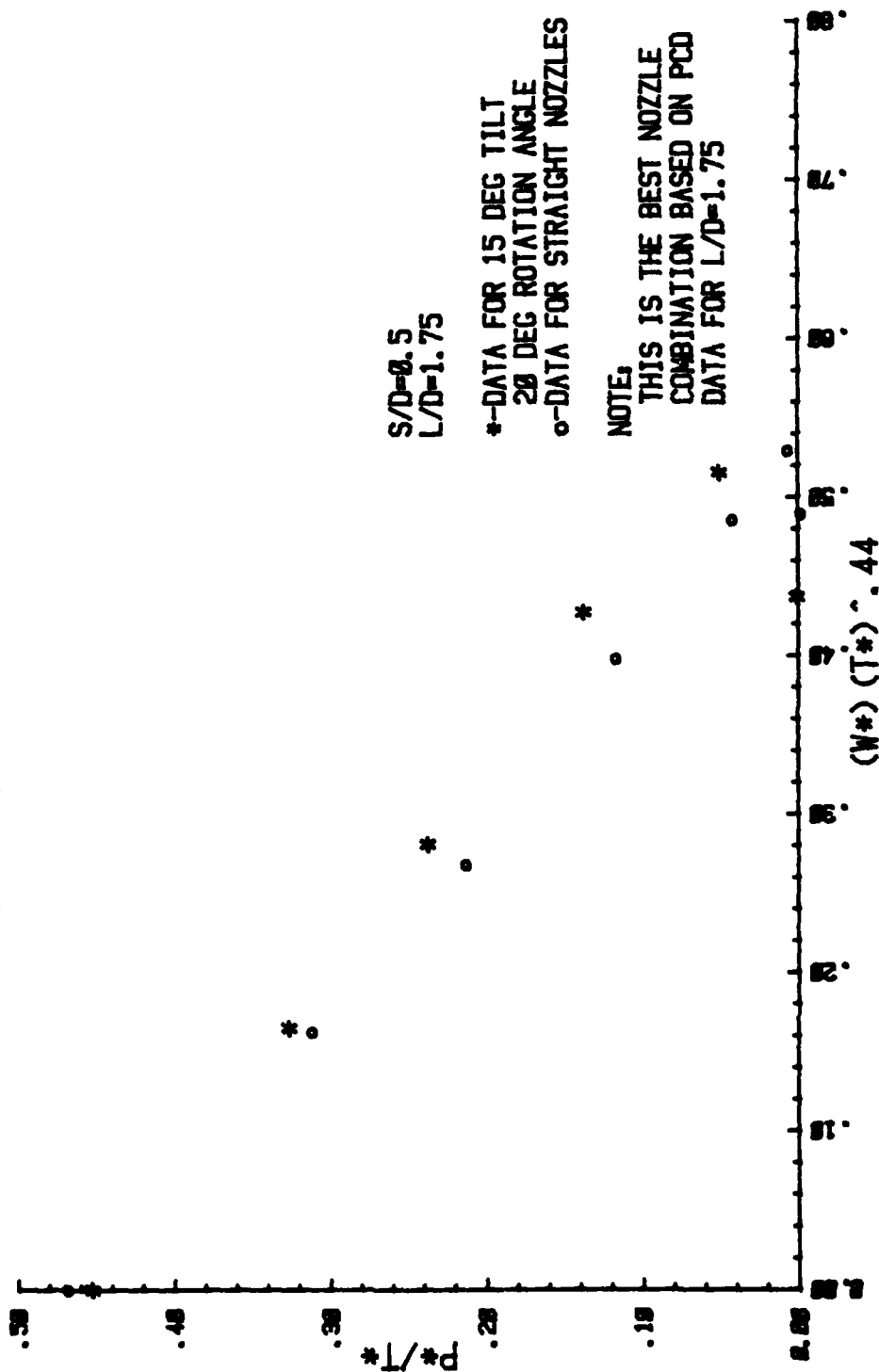


FIGURE 35

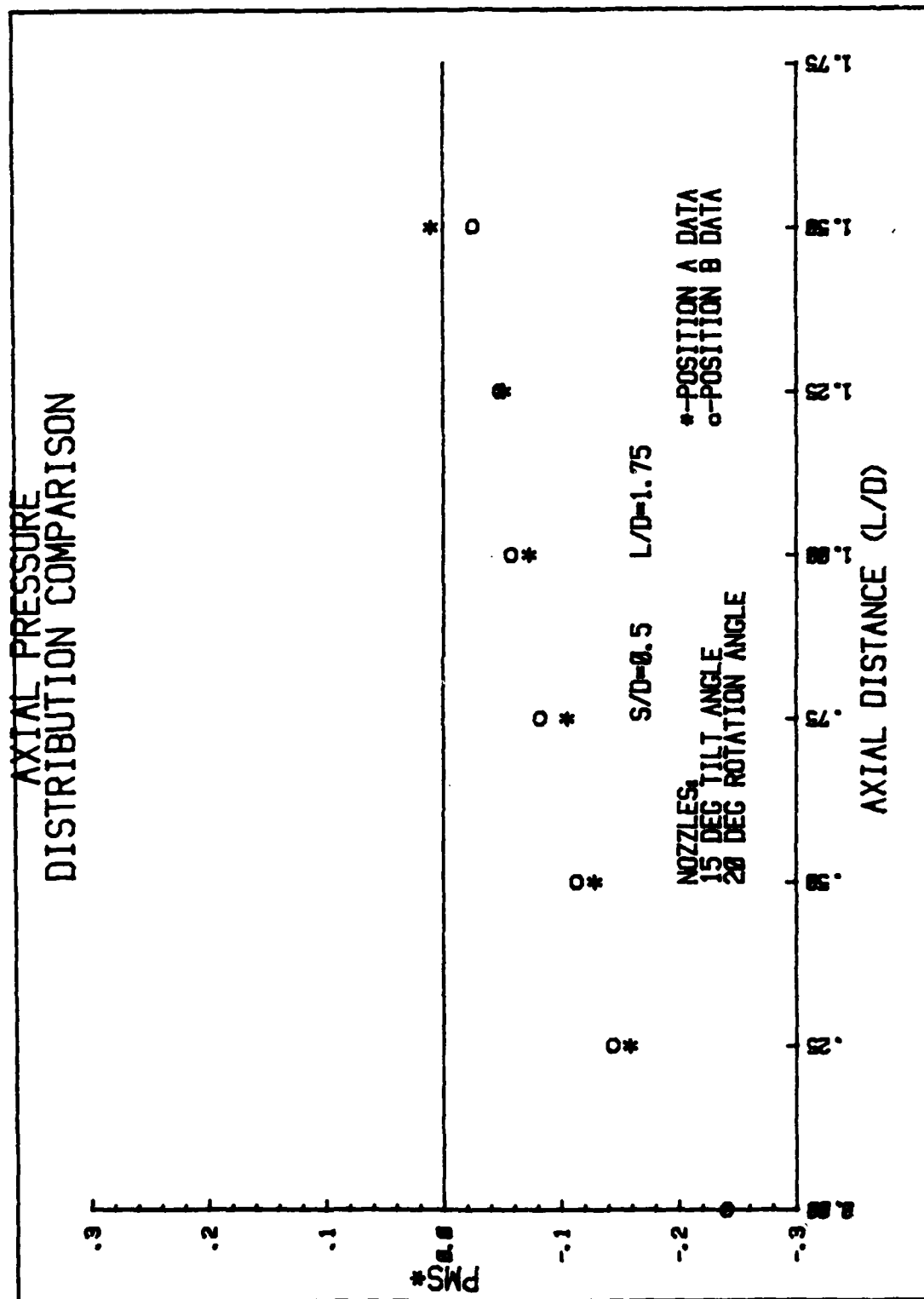


FIGURE 35.1

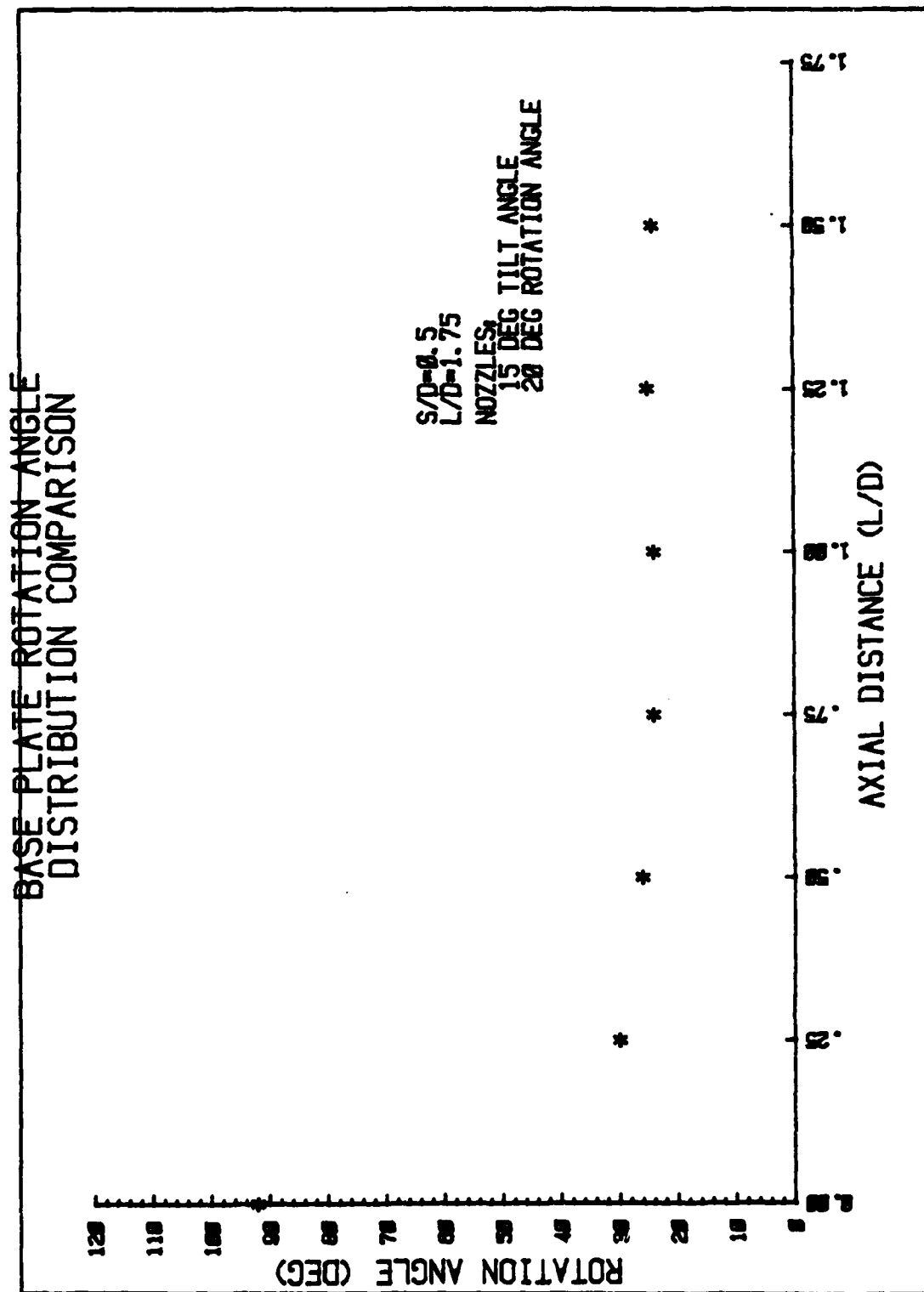


FIGURE 35.2



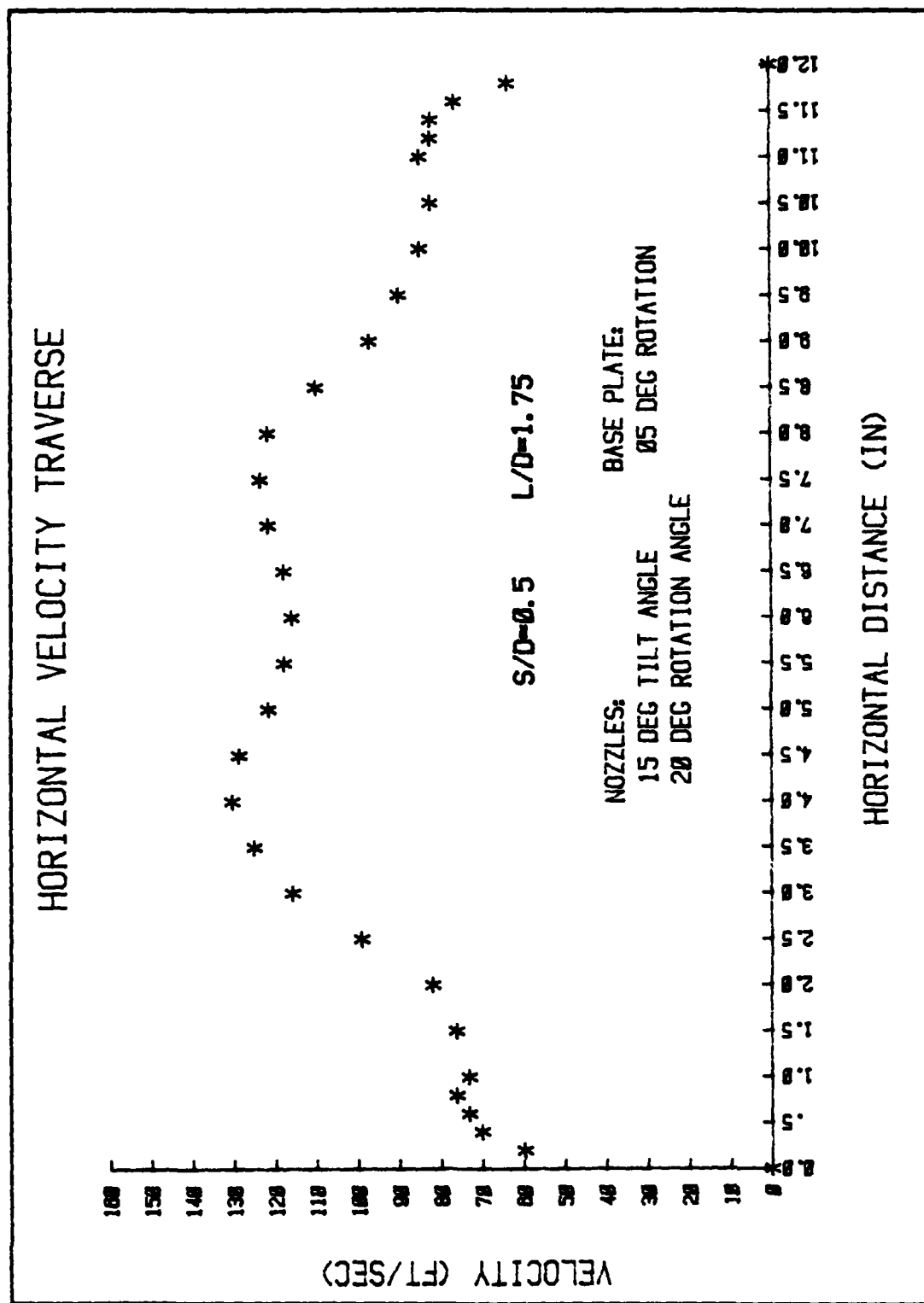


FIGURE 35.3

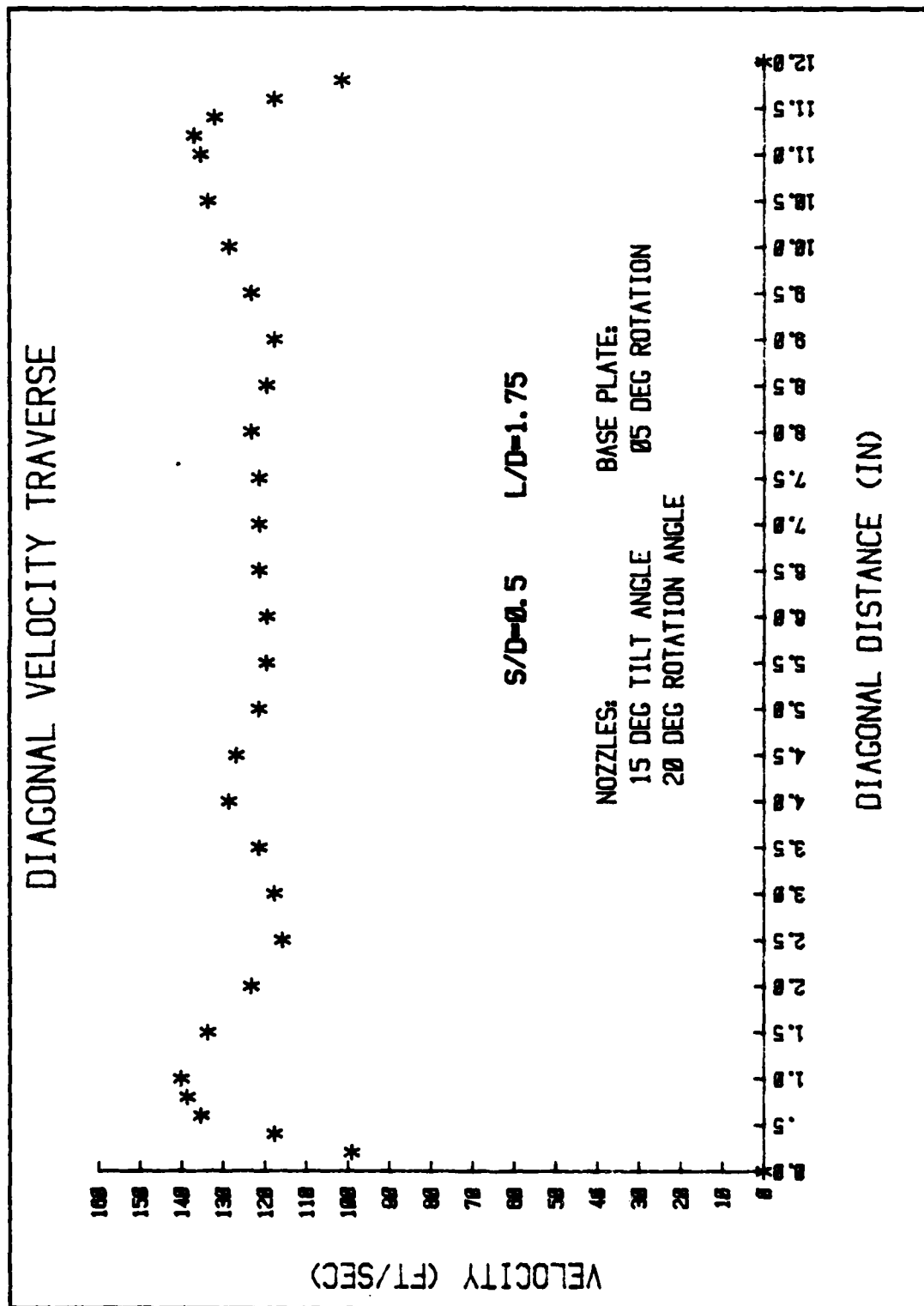


FIGURE 35.4

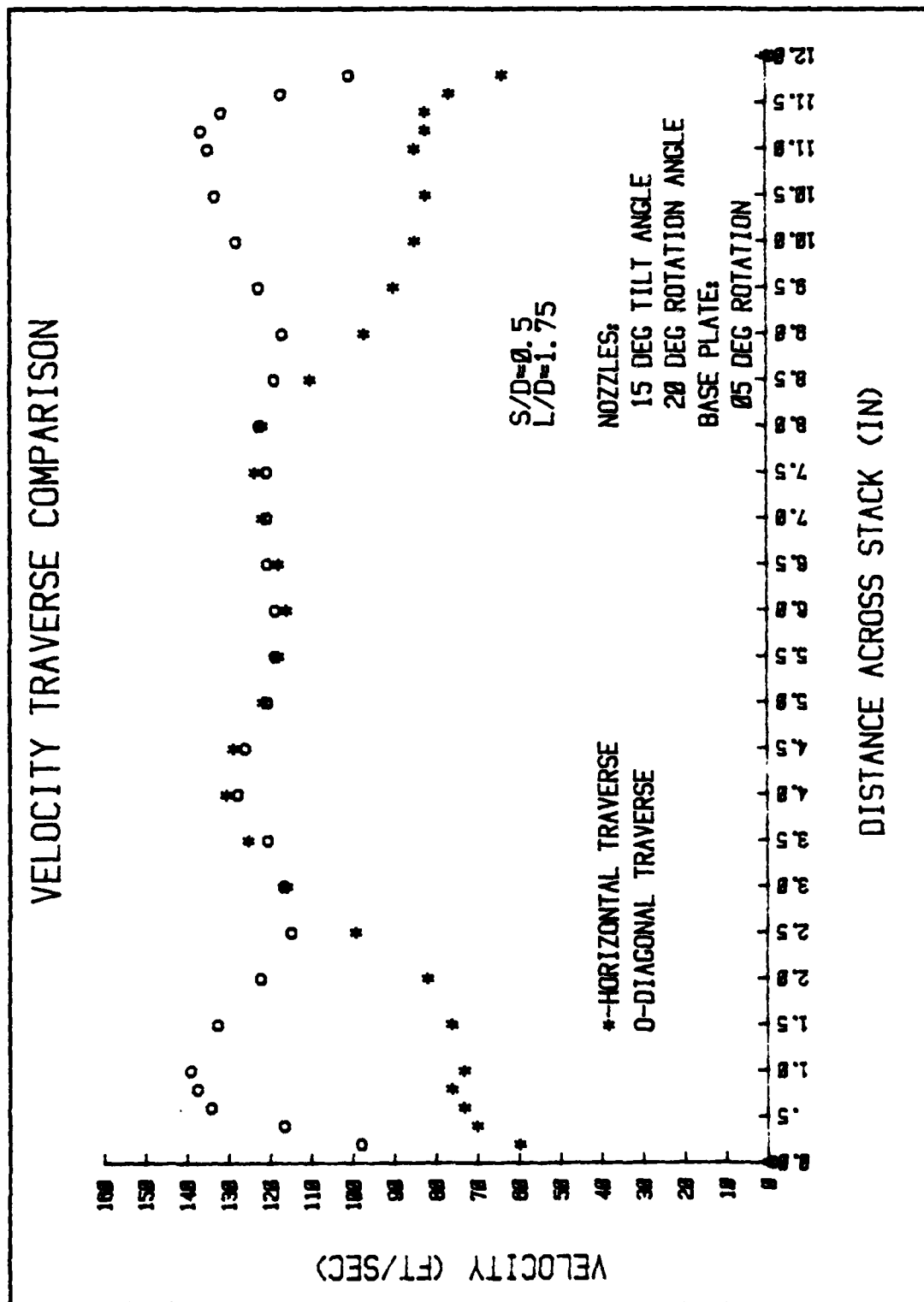


FIGURE 35.5

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

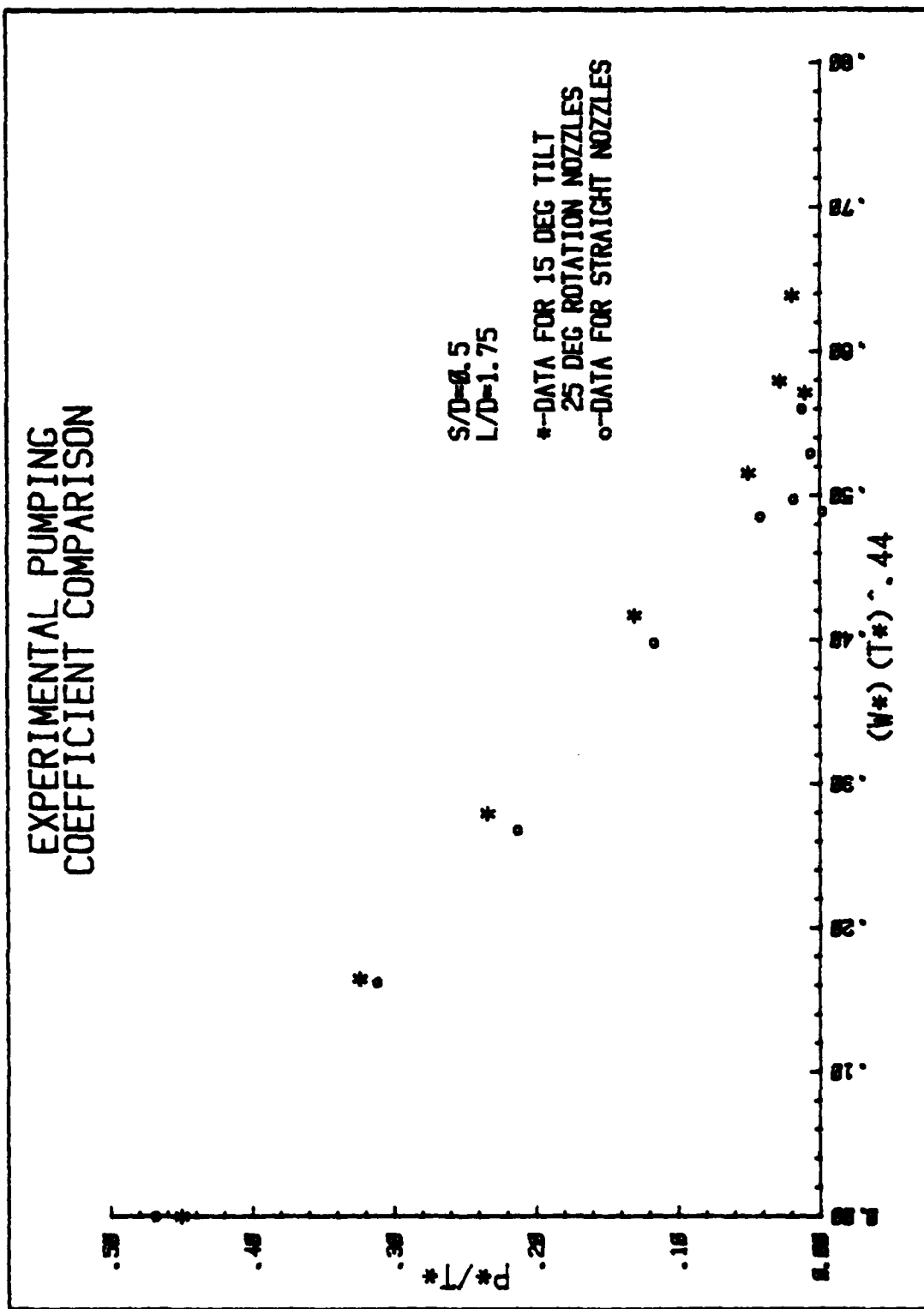


FIGURE 36

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

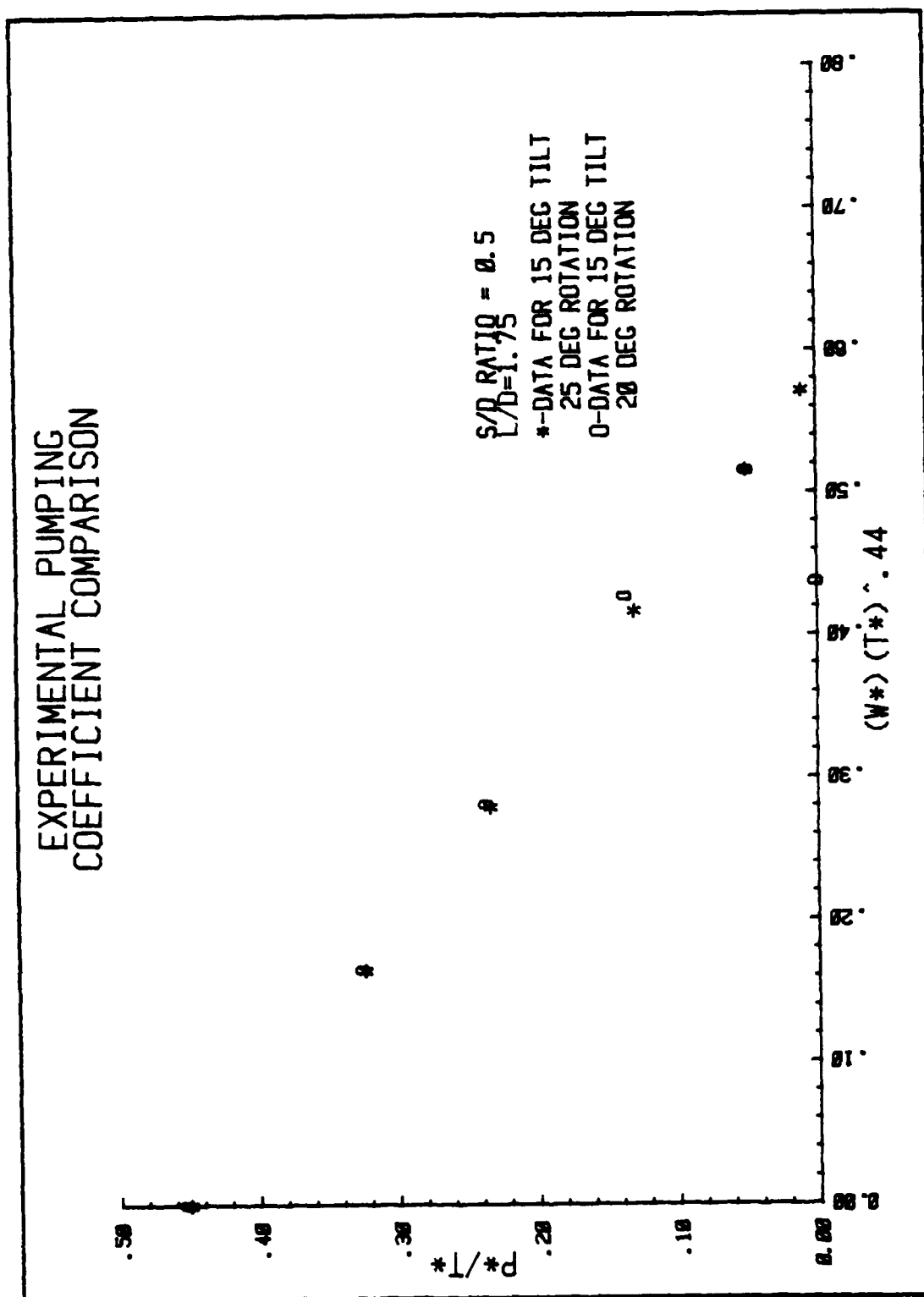


FIGURE 38.1

# AXIAL PRESSURE DISTRIBUTION COMPARISON

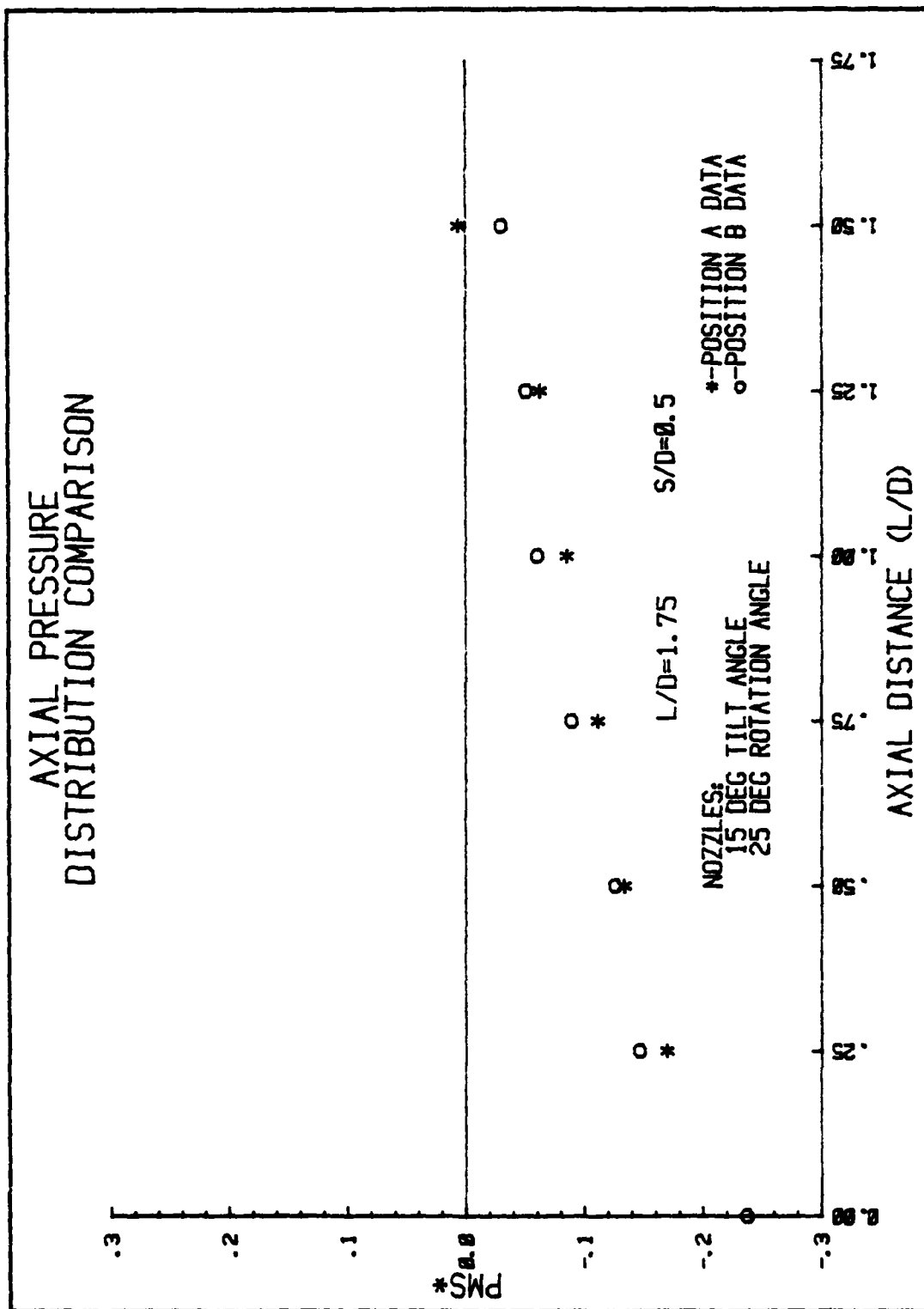


FIGURE 36.2

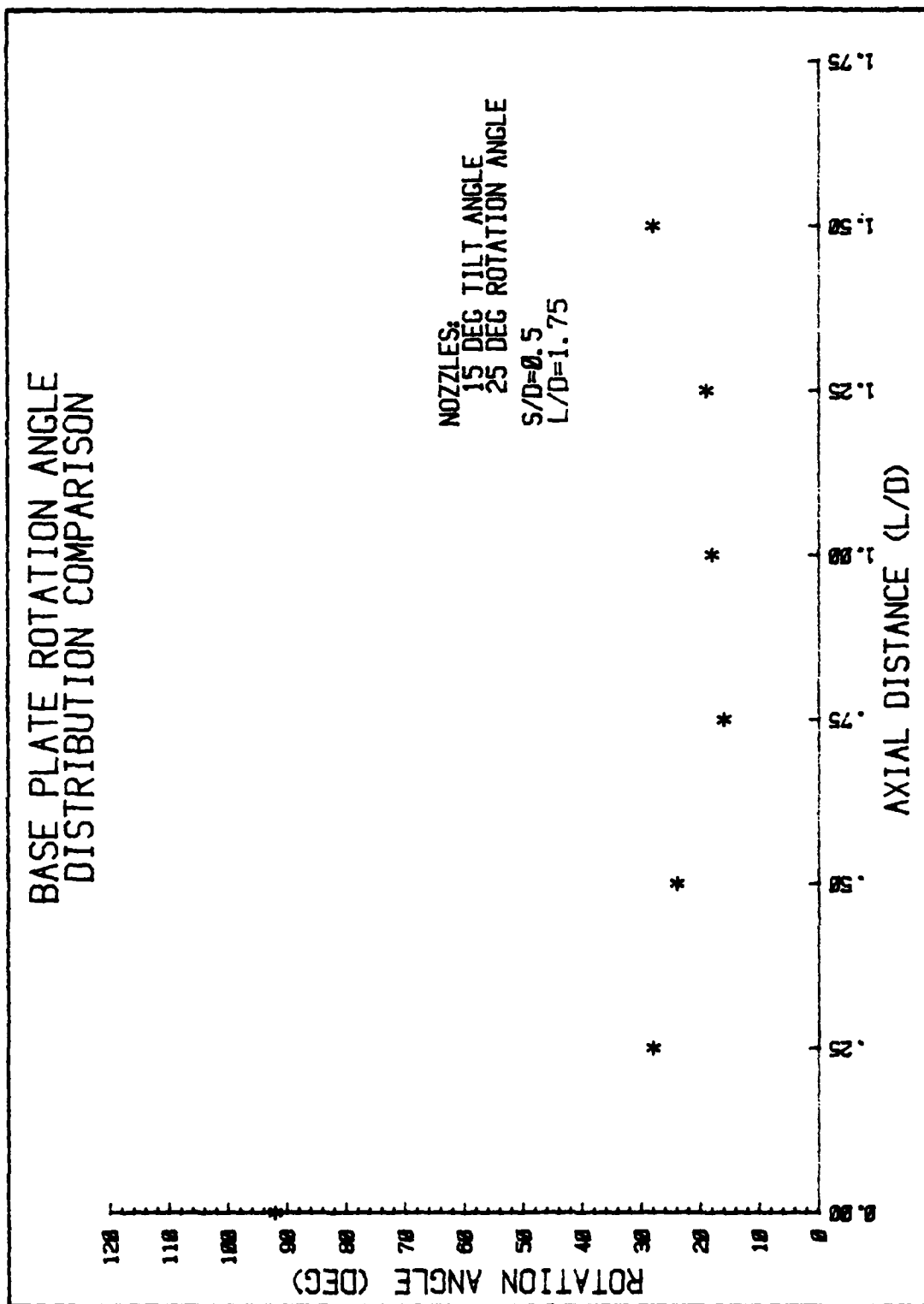


FIGURE 36.3

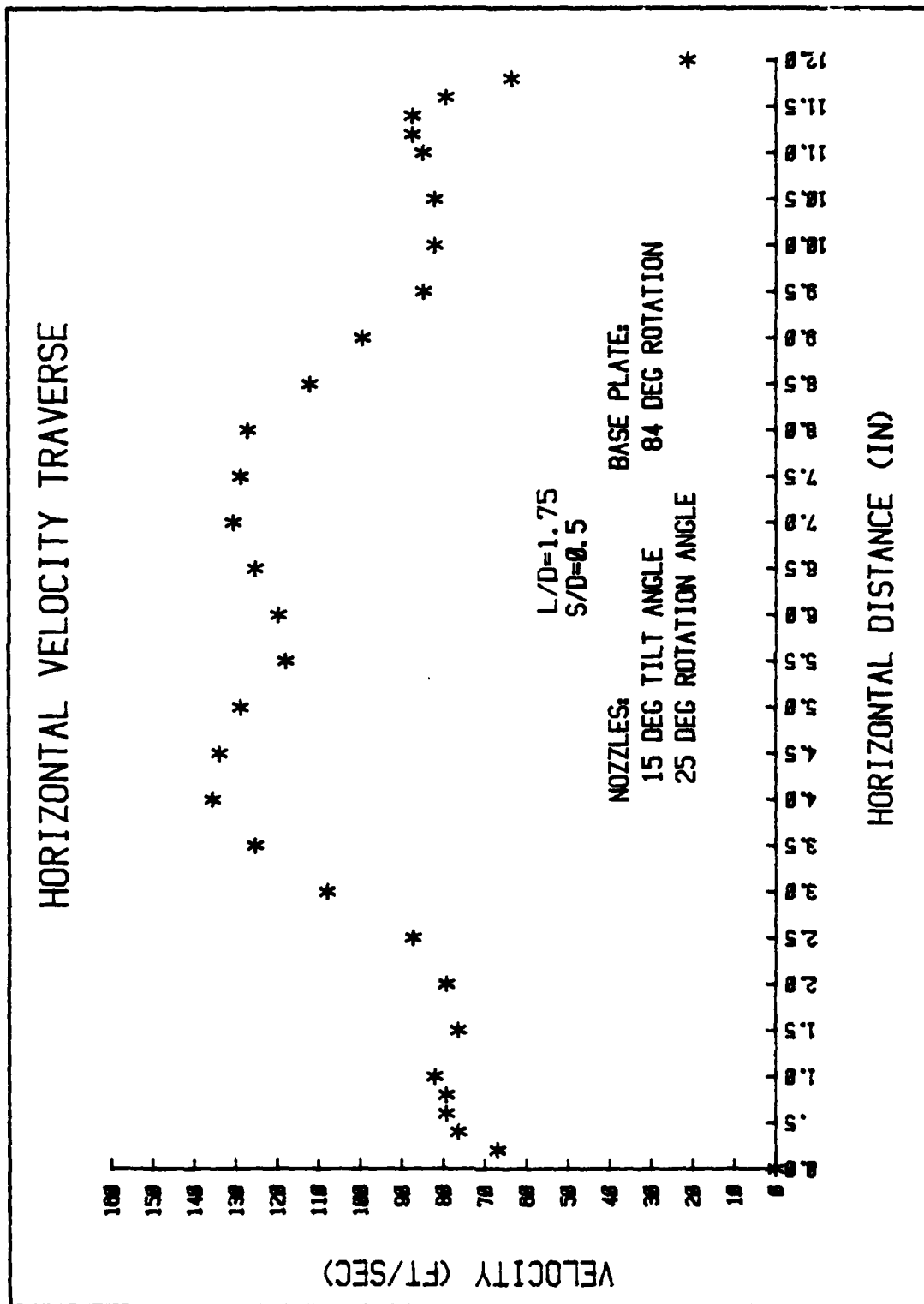


FIGURE 36.4



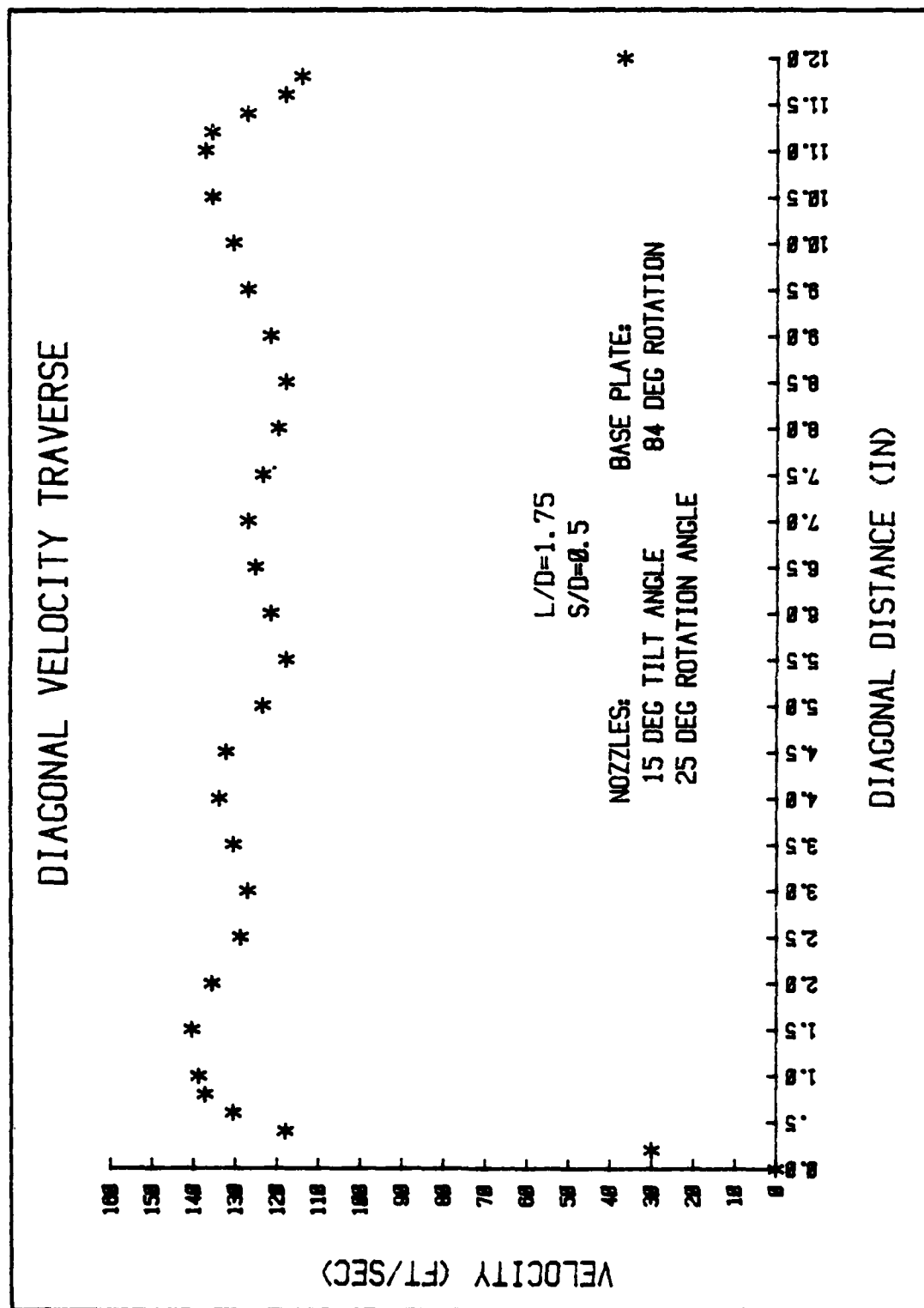


FIGURE 38.5

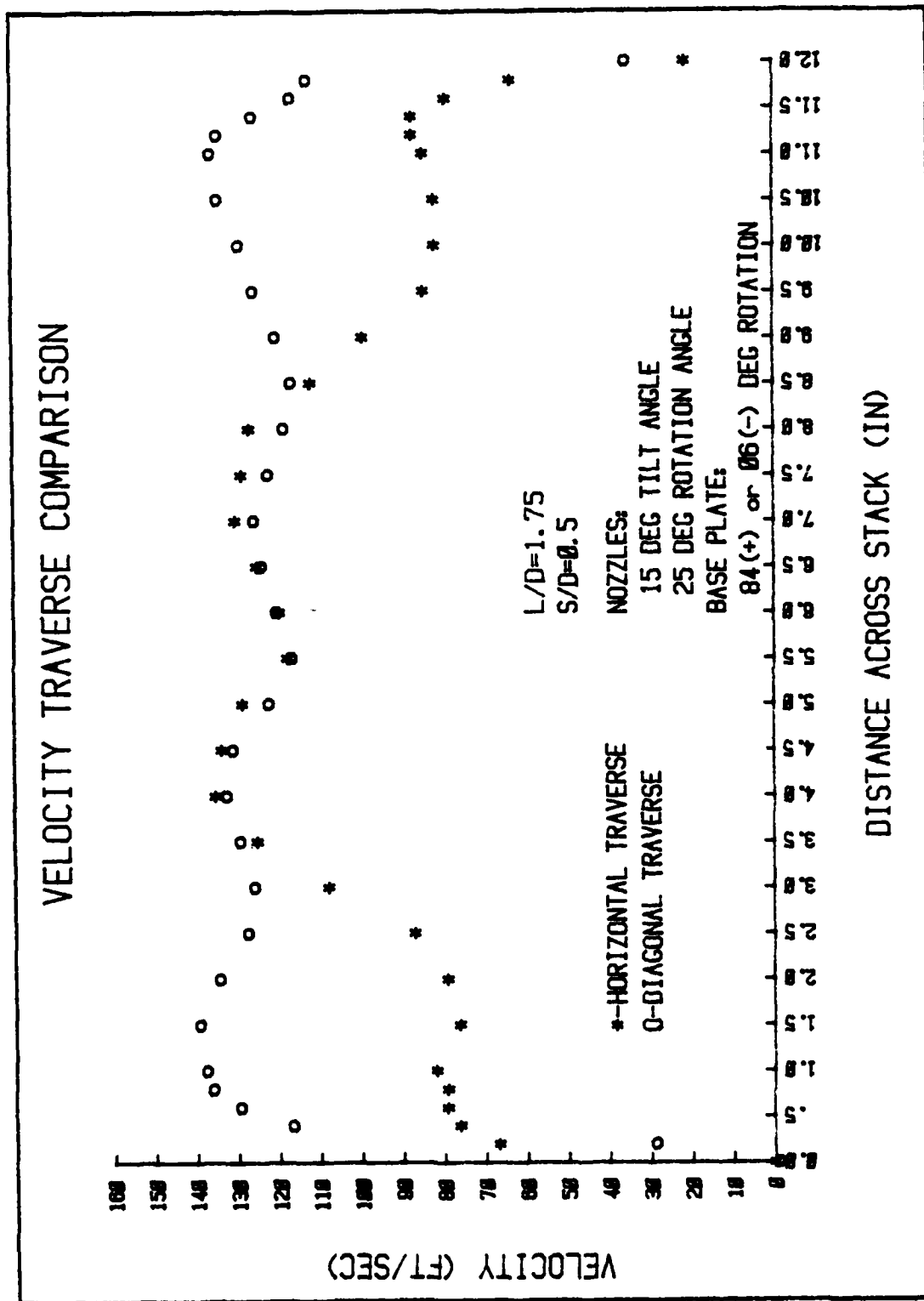


FIGURE 36.6

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

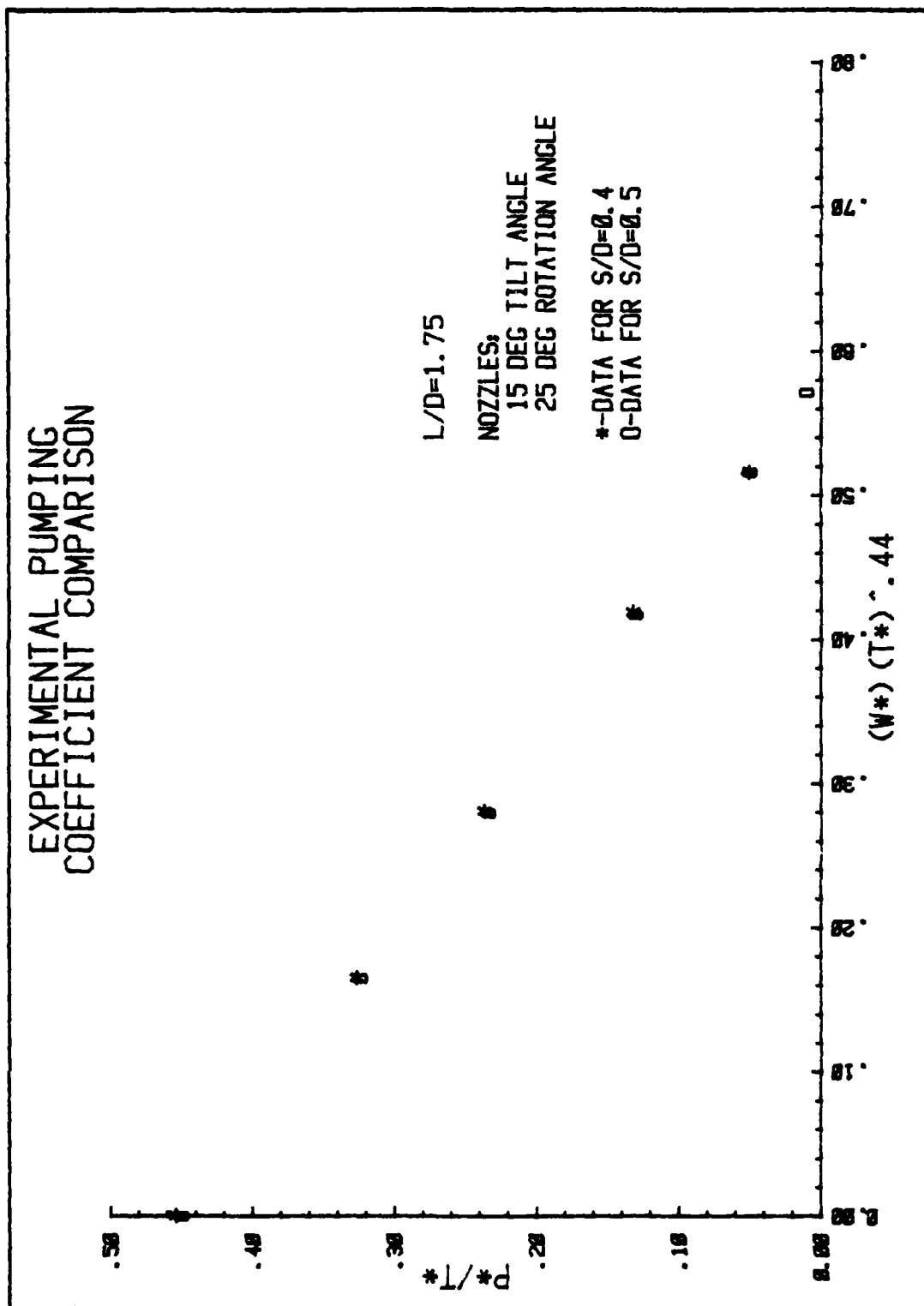


FIGURE 37

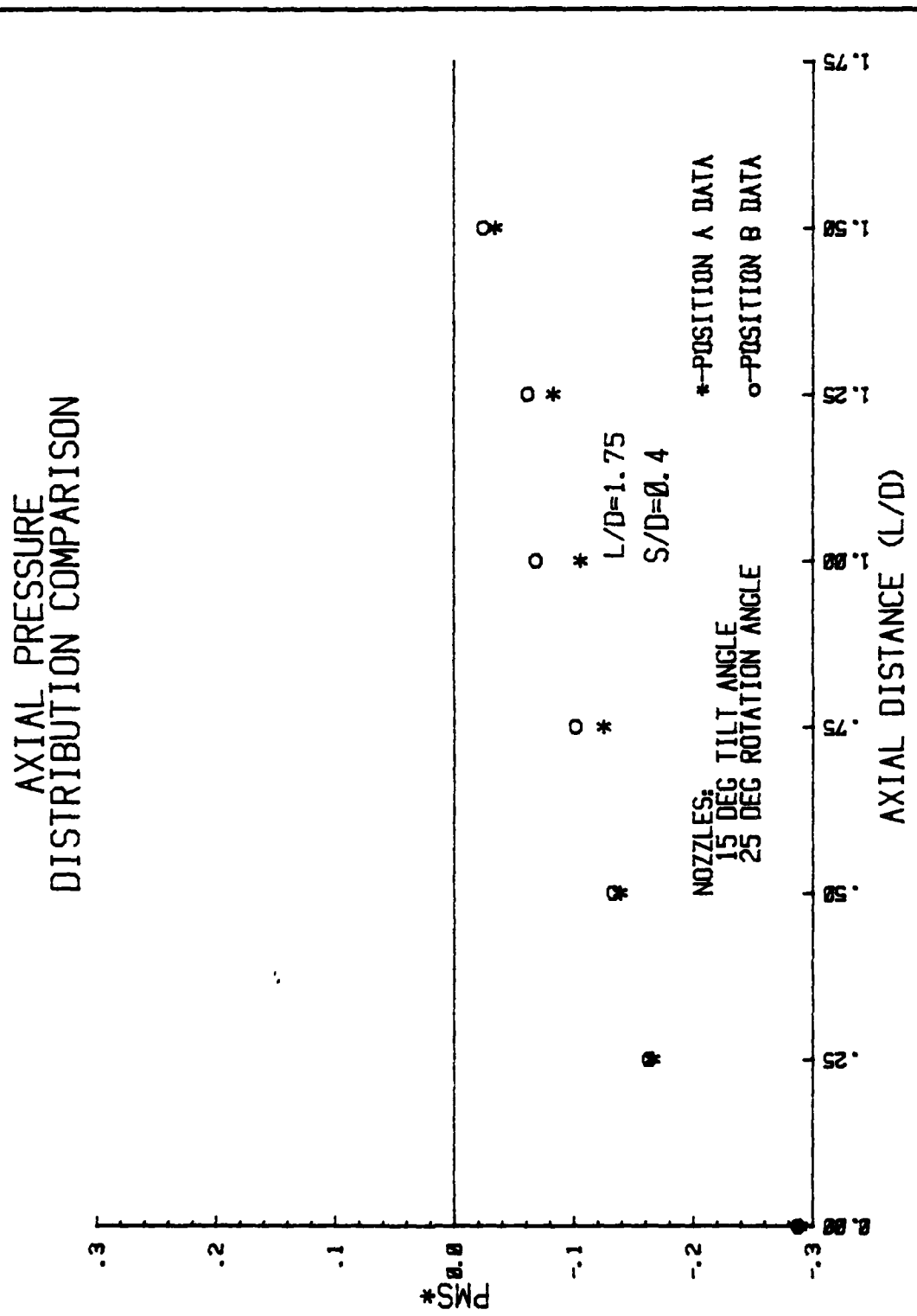


FIGURE 37.1

# BASE PLATE ROTATION ANGLE DISTRIBUTION COMPARISON

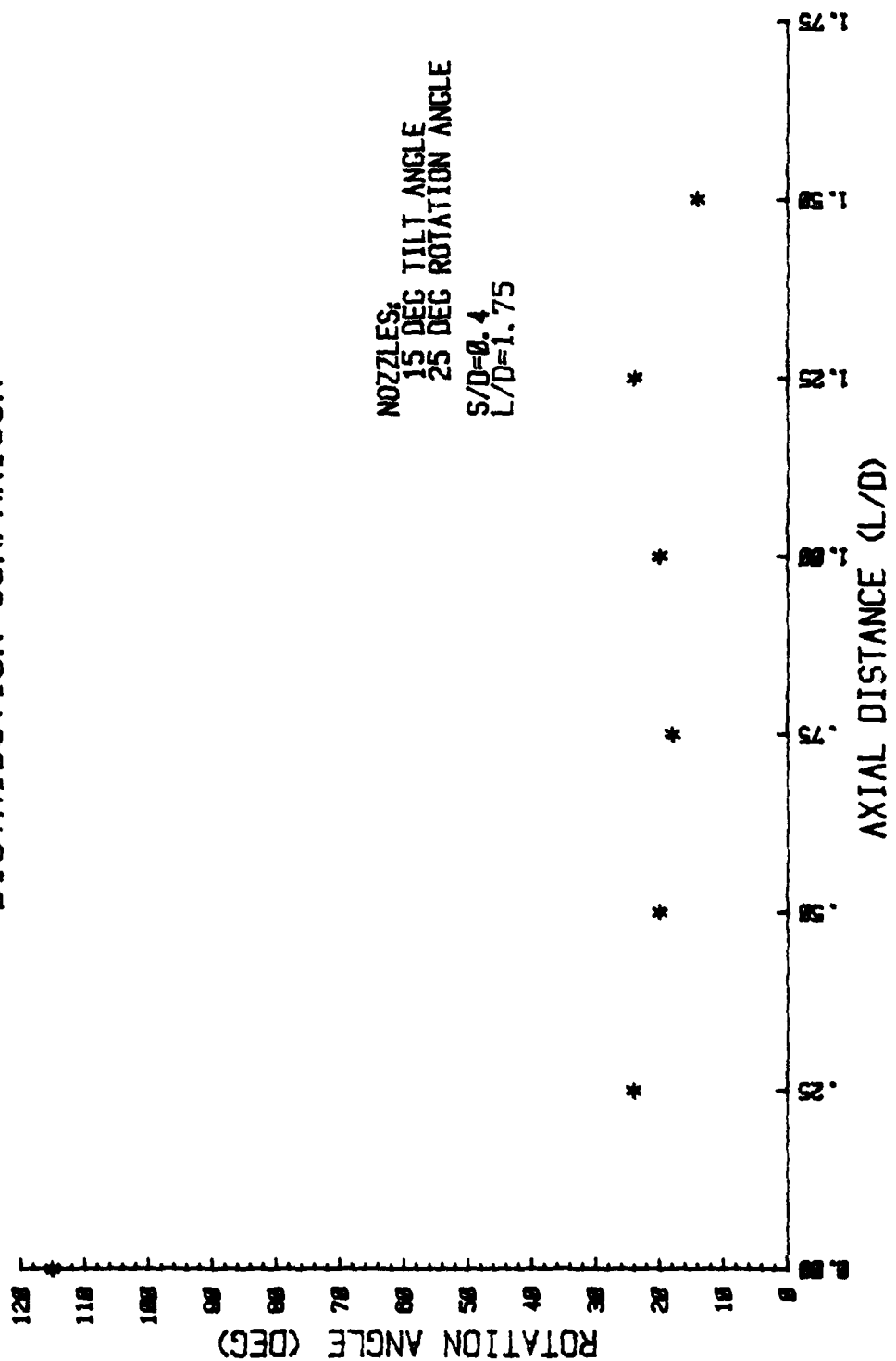


FIGURE 37.2

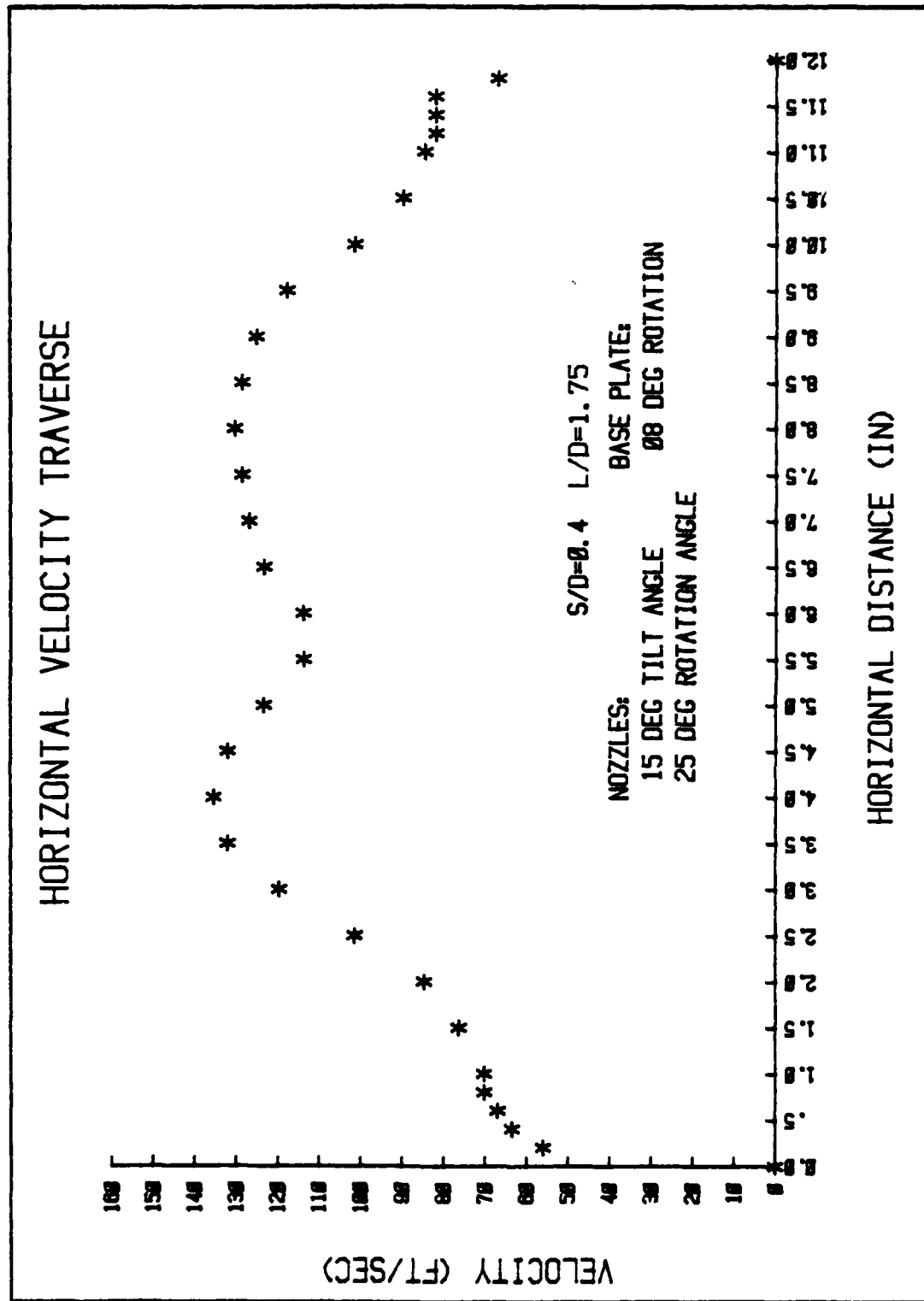


FIGURE 37.3

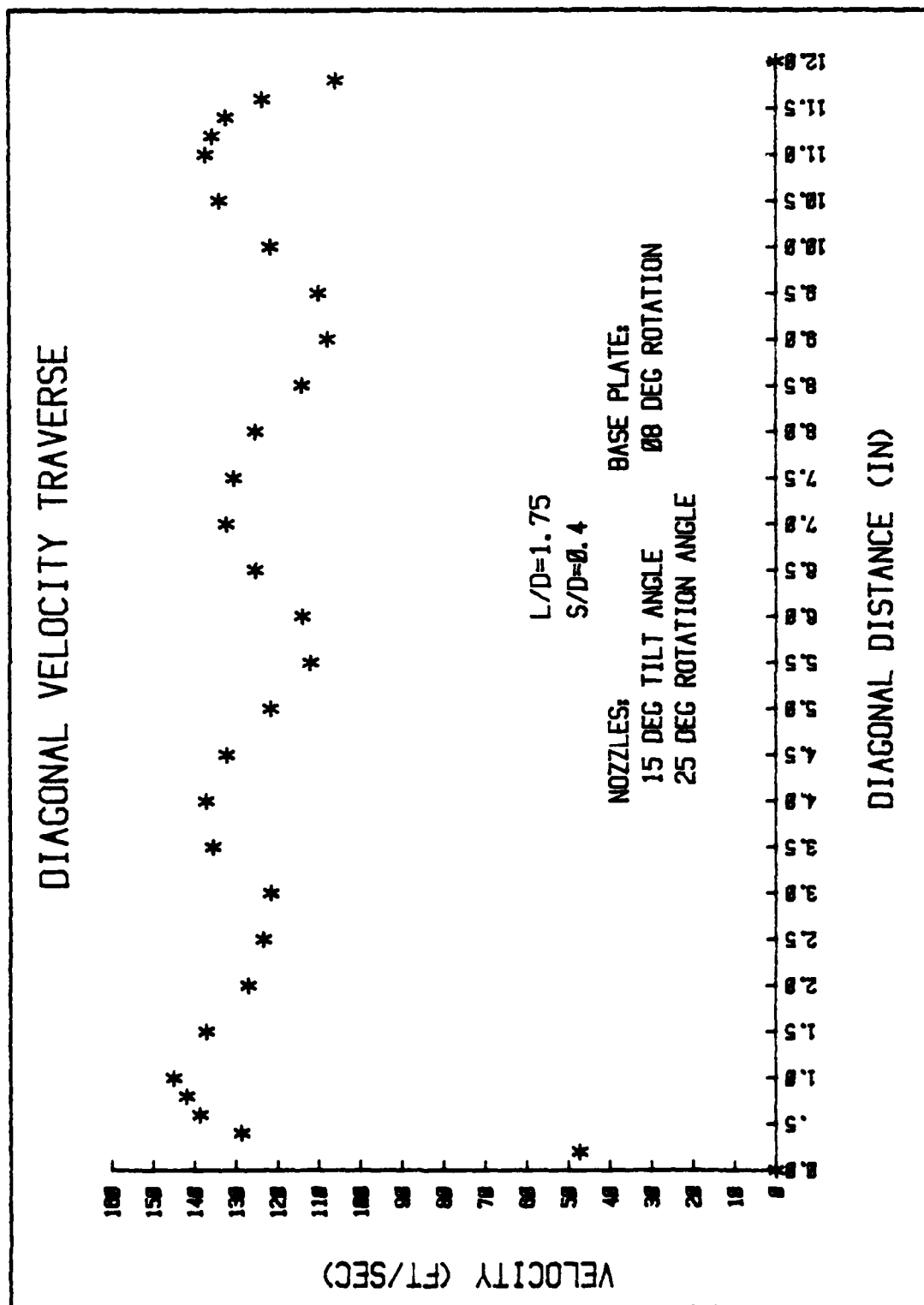


FIGURE 37.4

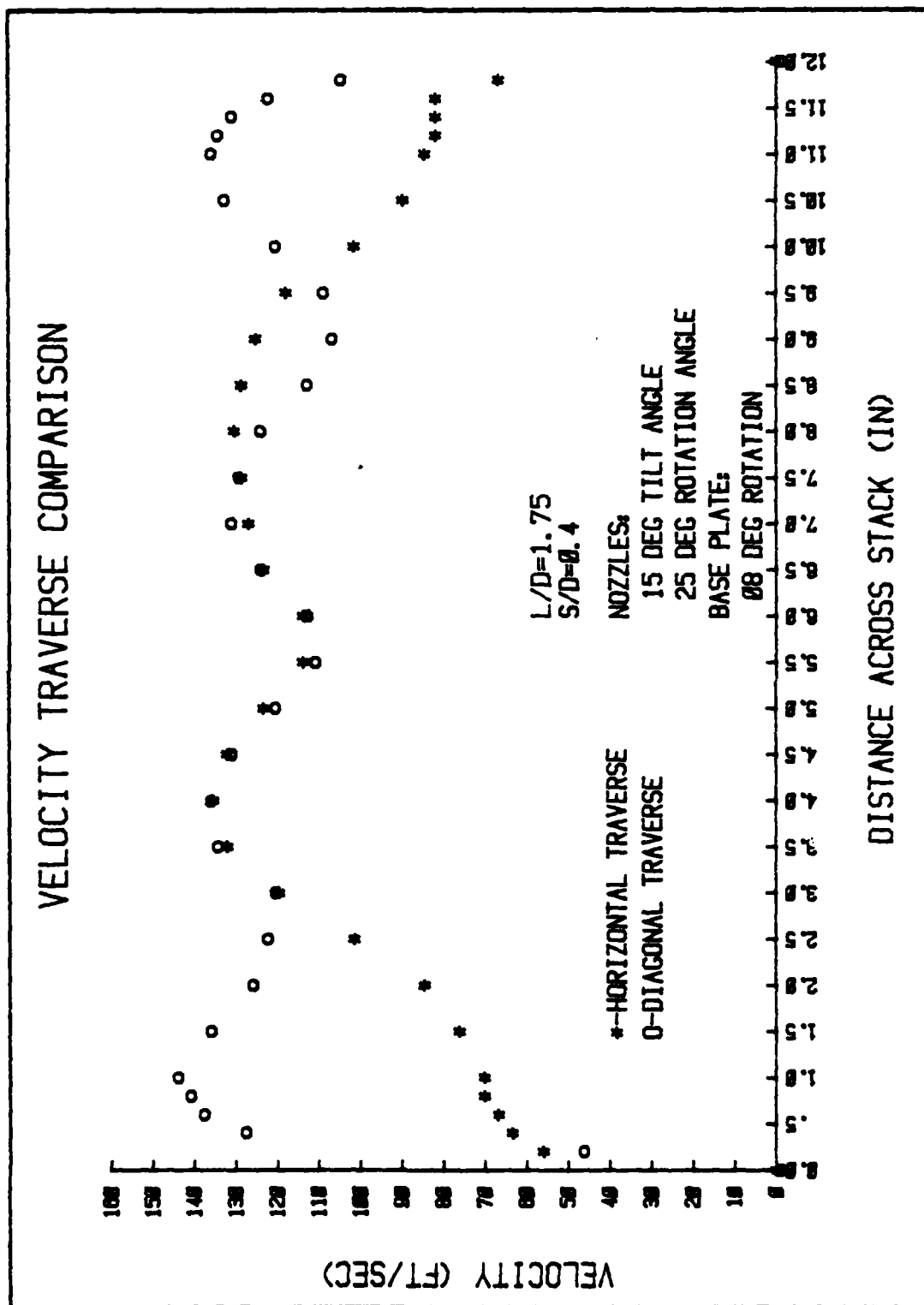


FIGURE 37.5



# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

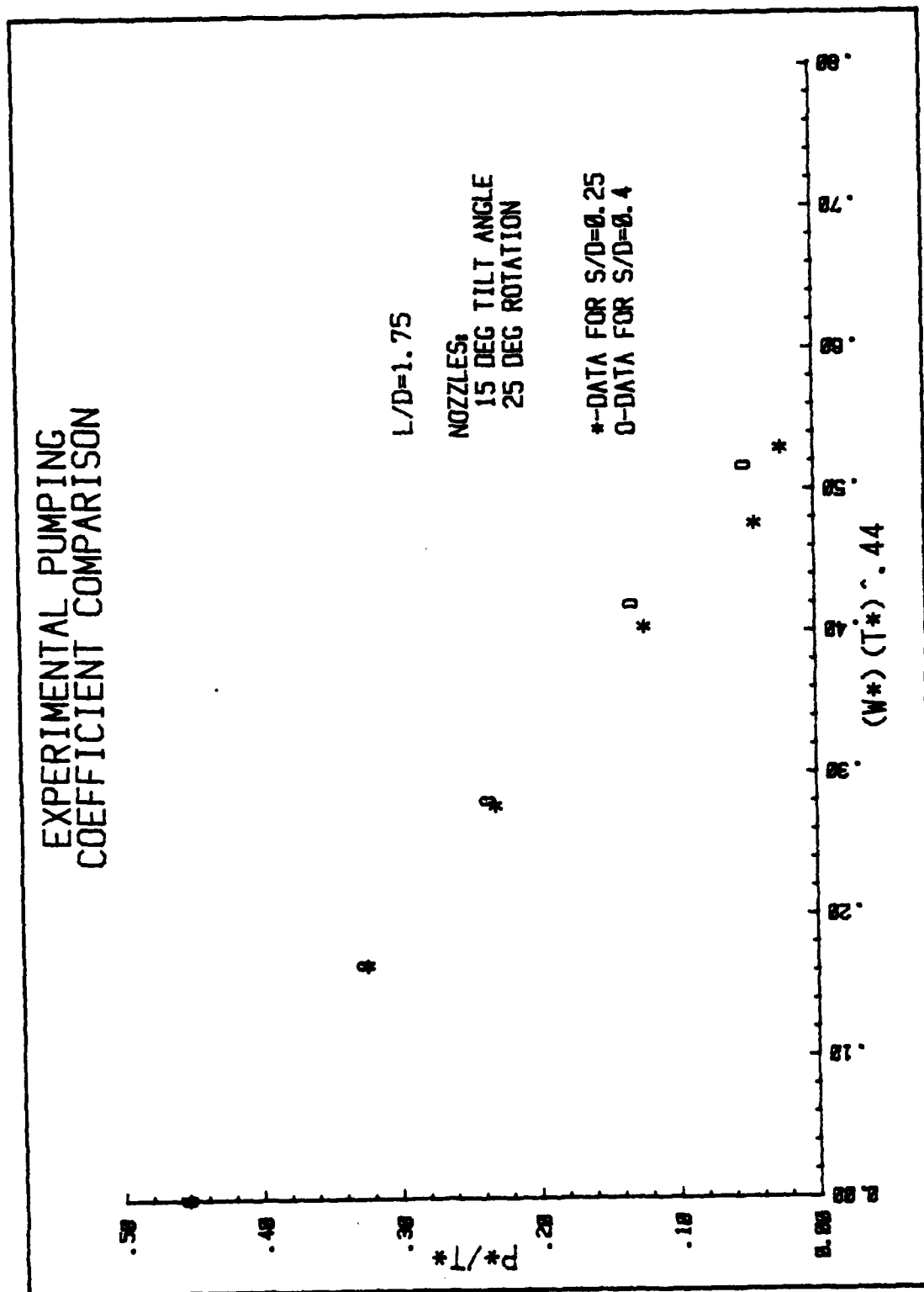


FIGURE 38

# AXIAL PRESSURE DISTRIBUTION COMPARISON

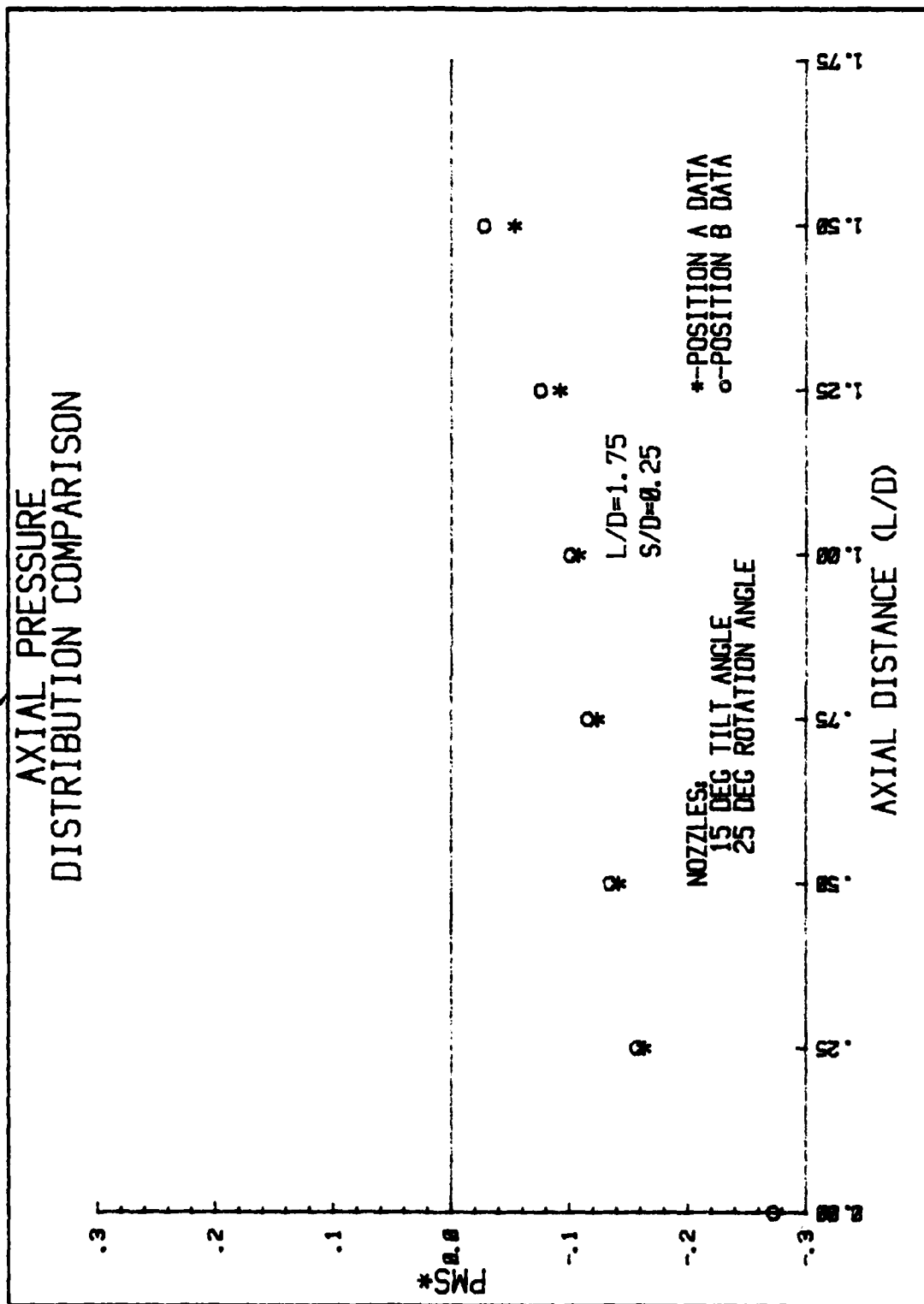


FIGURE 38.1

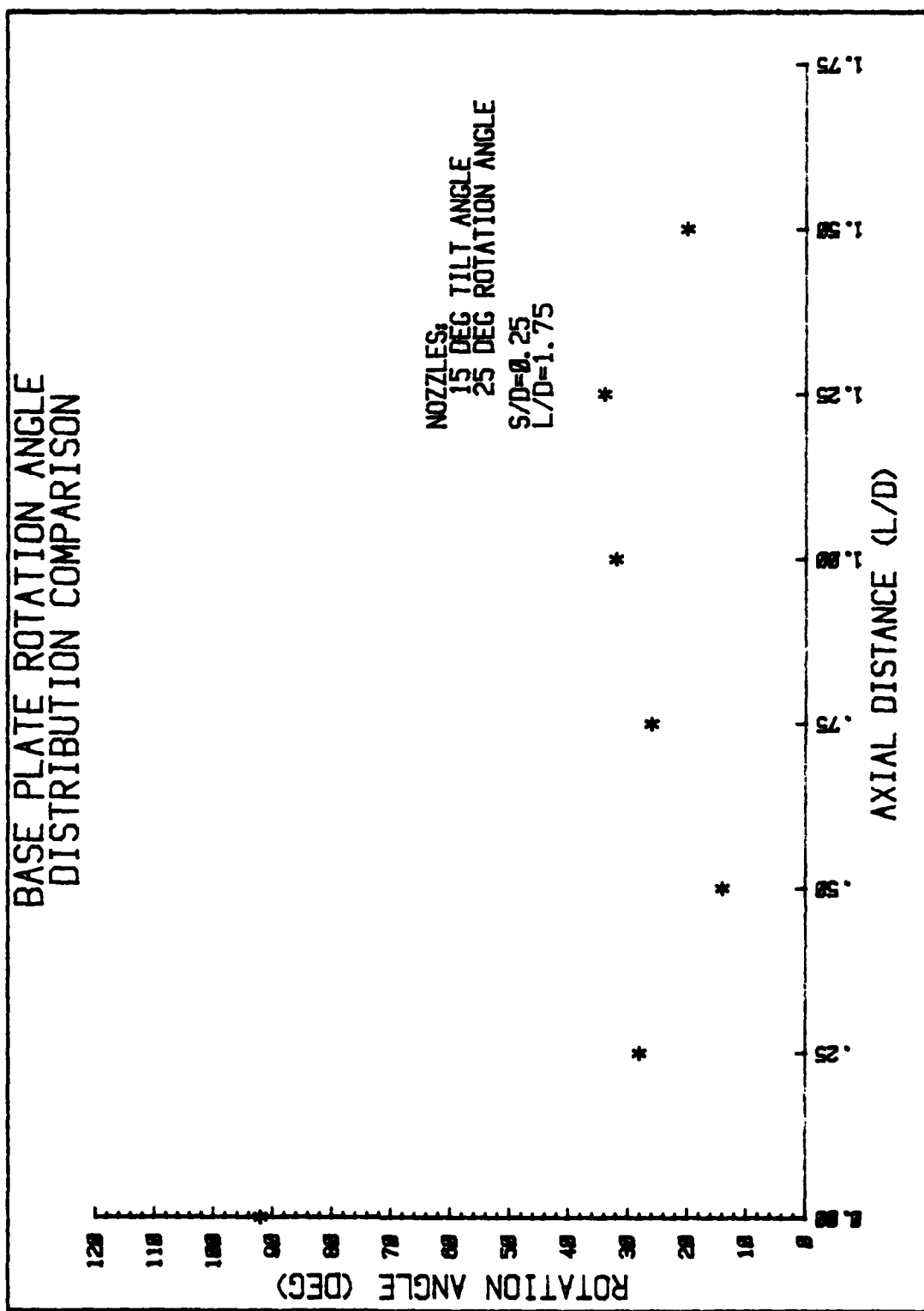


FIGURE 38.2

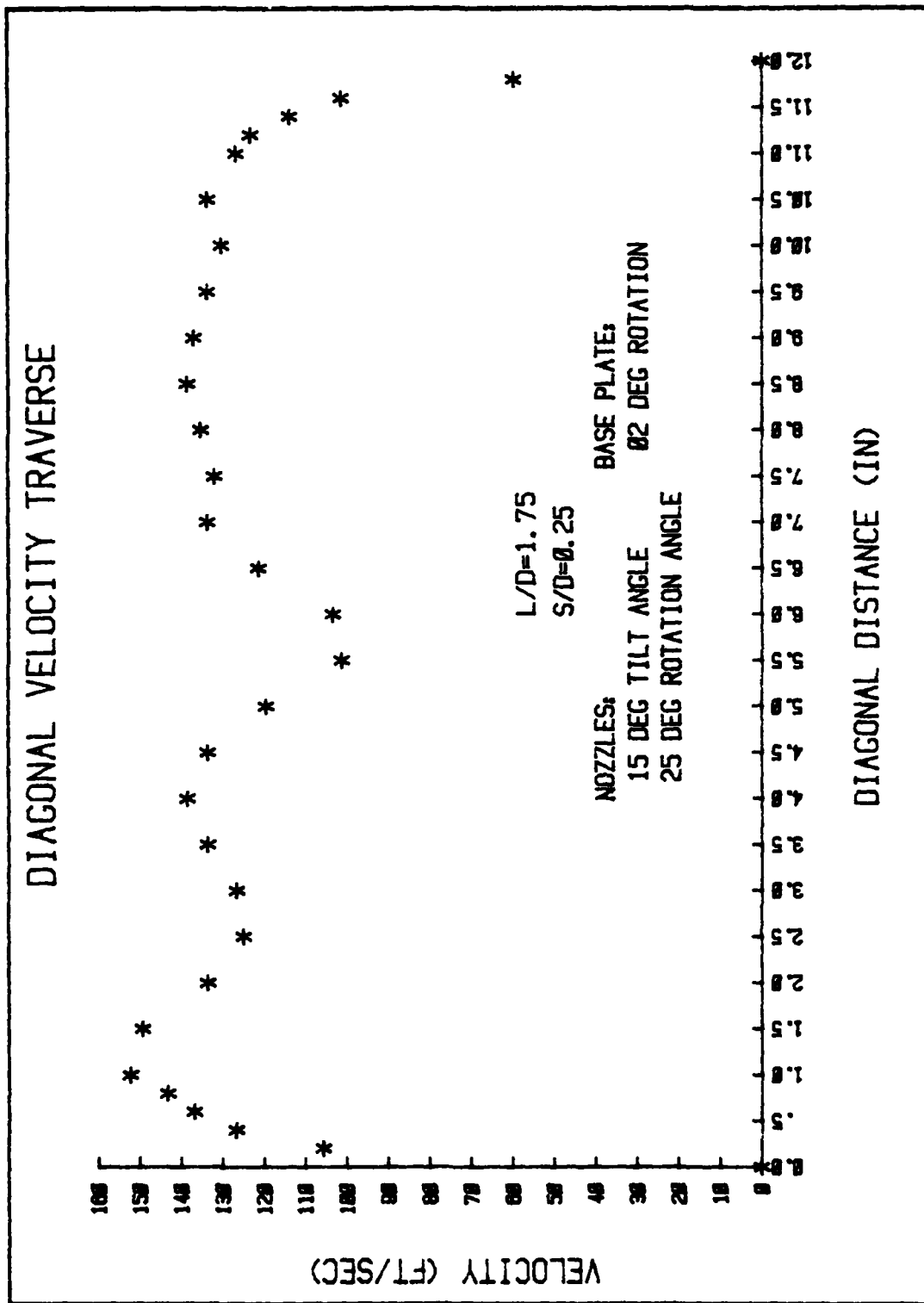


FIGURE 38.3

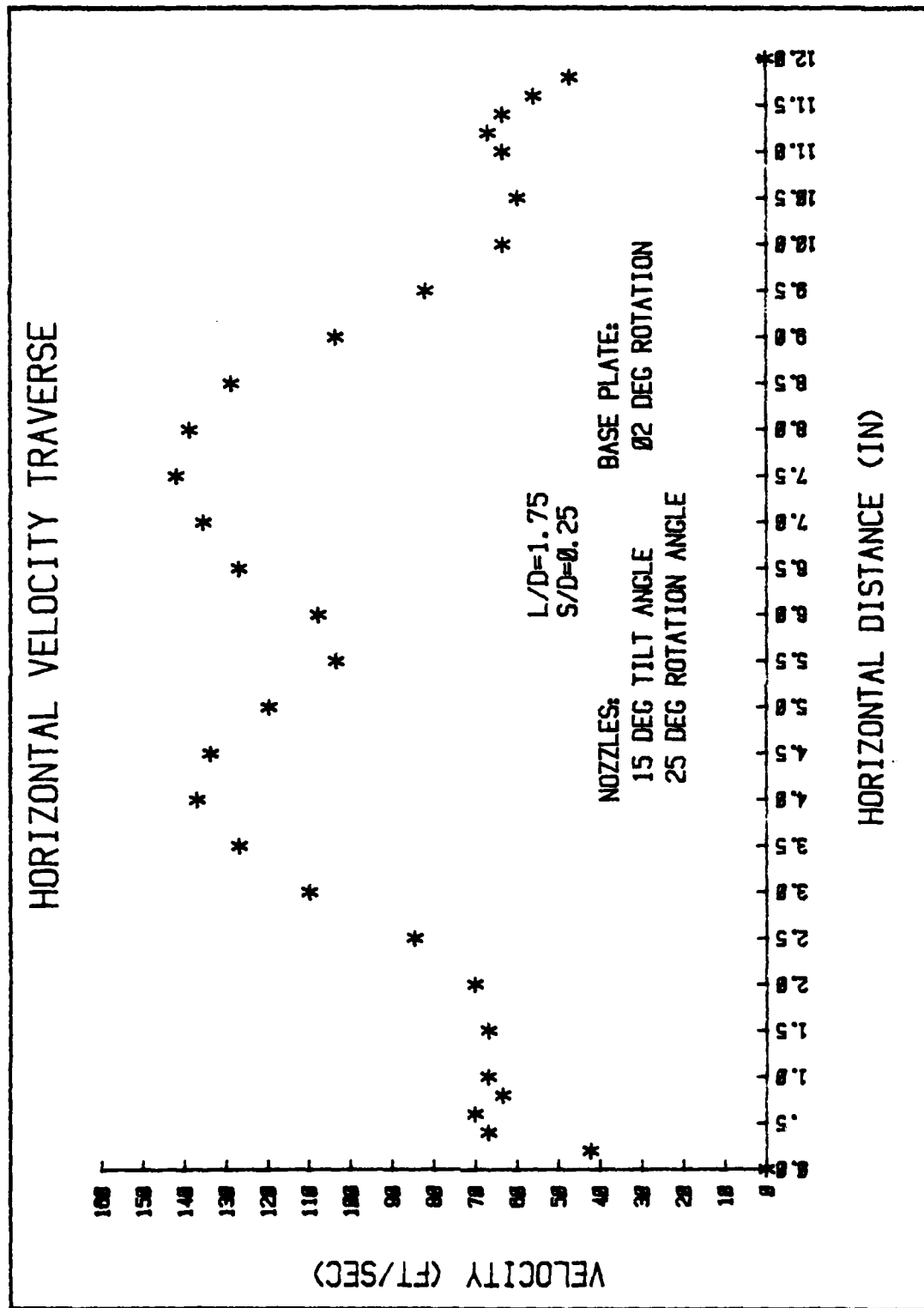


FIGURE 38.4

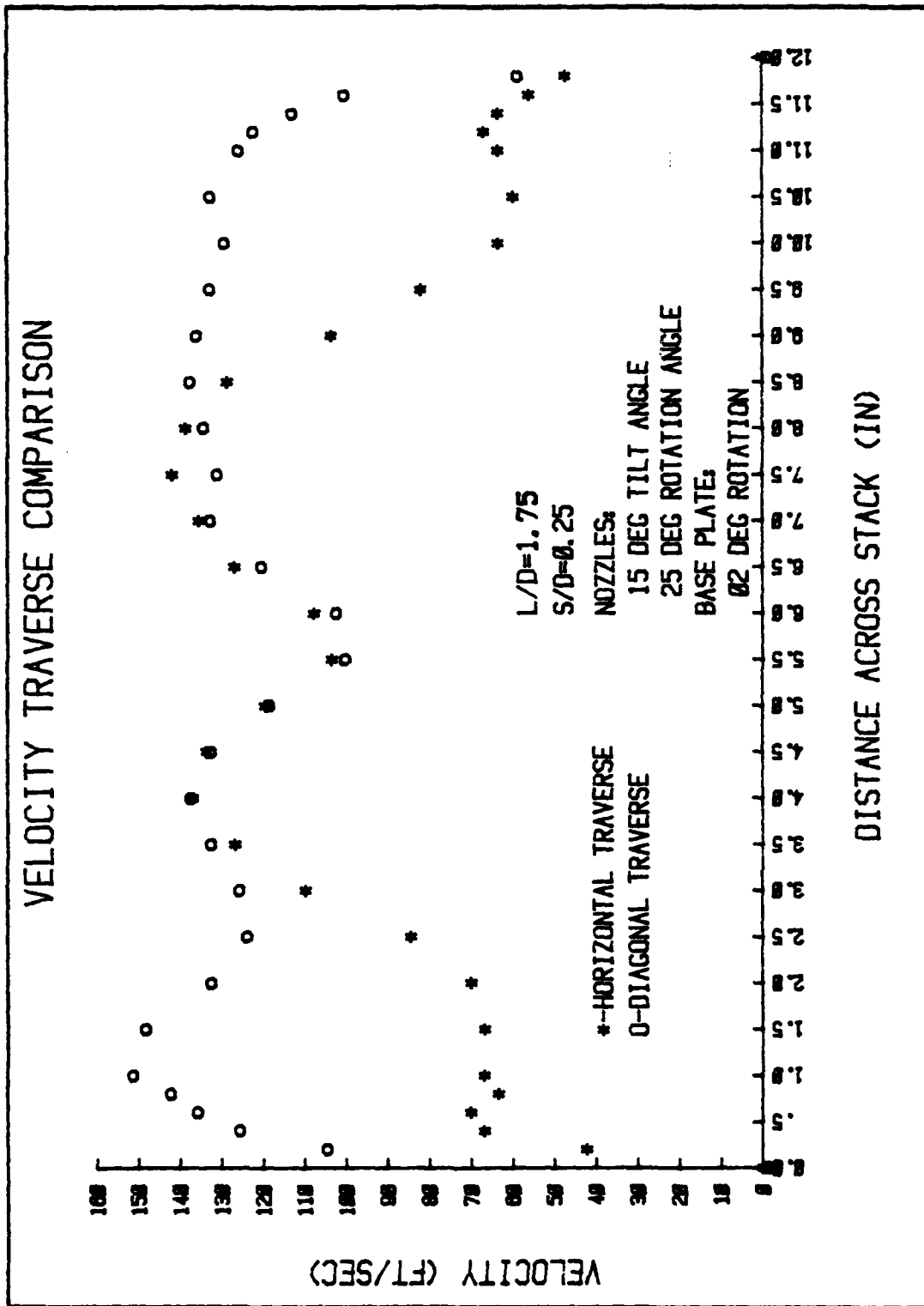


FIGURE 38.5

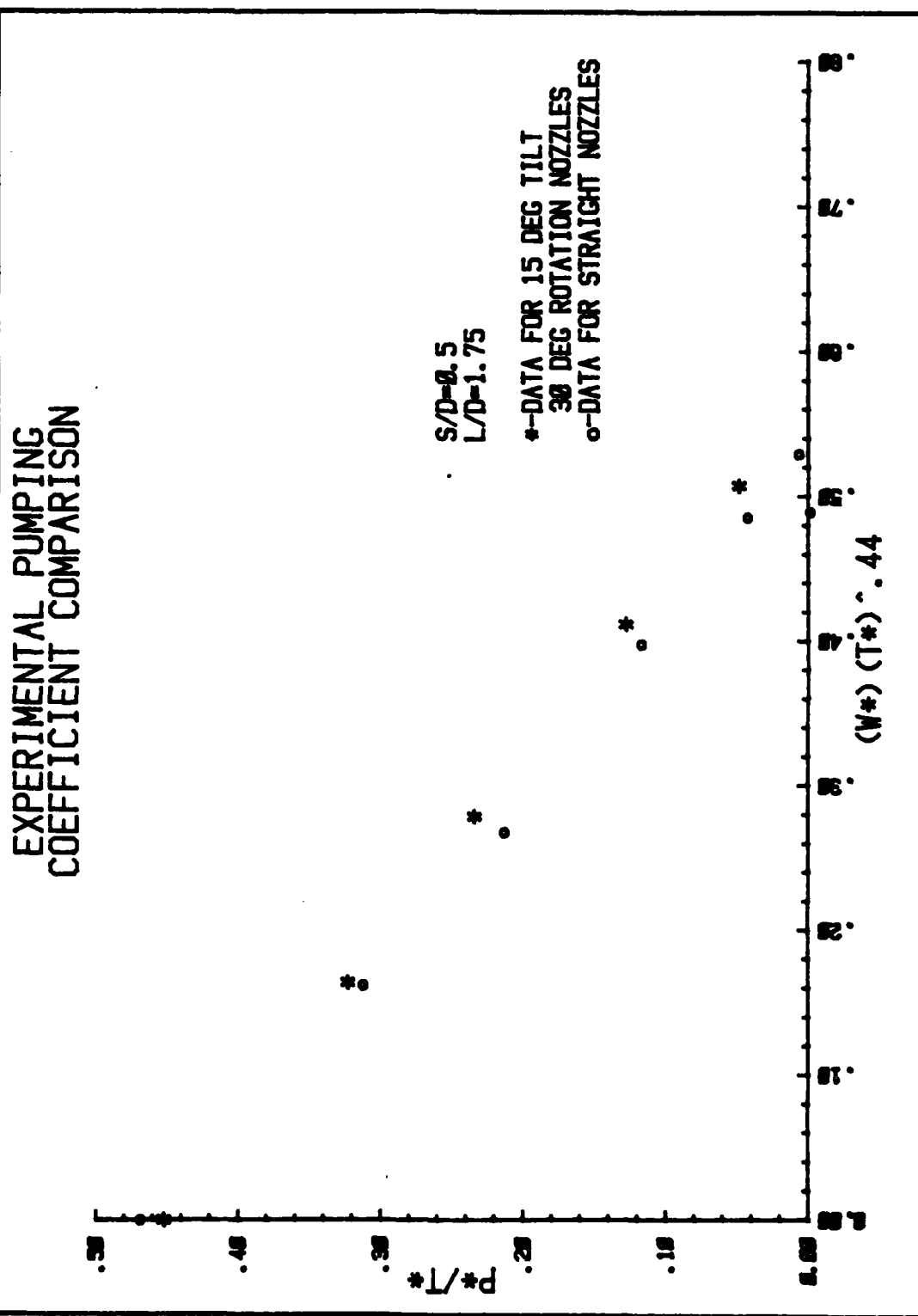


FIGURE 38

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

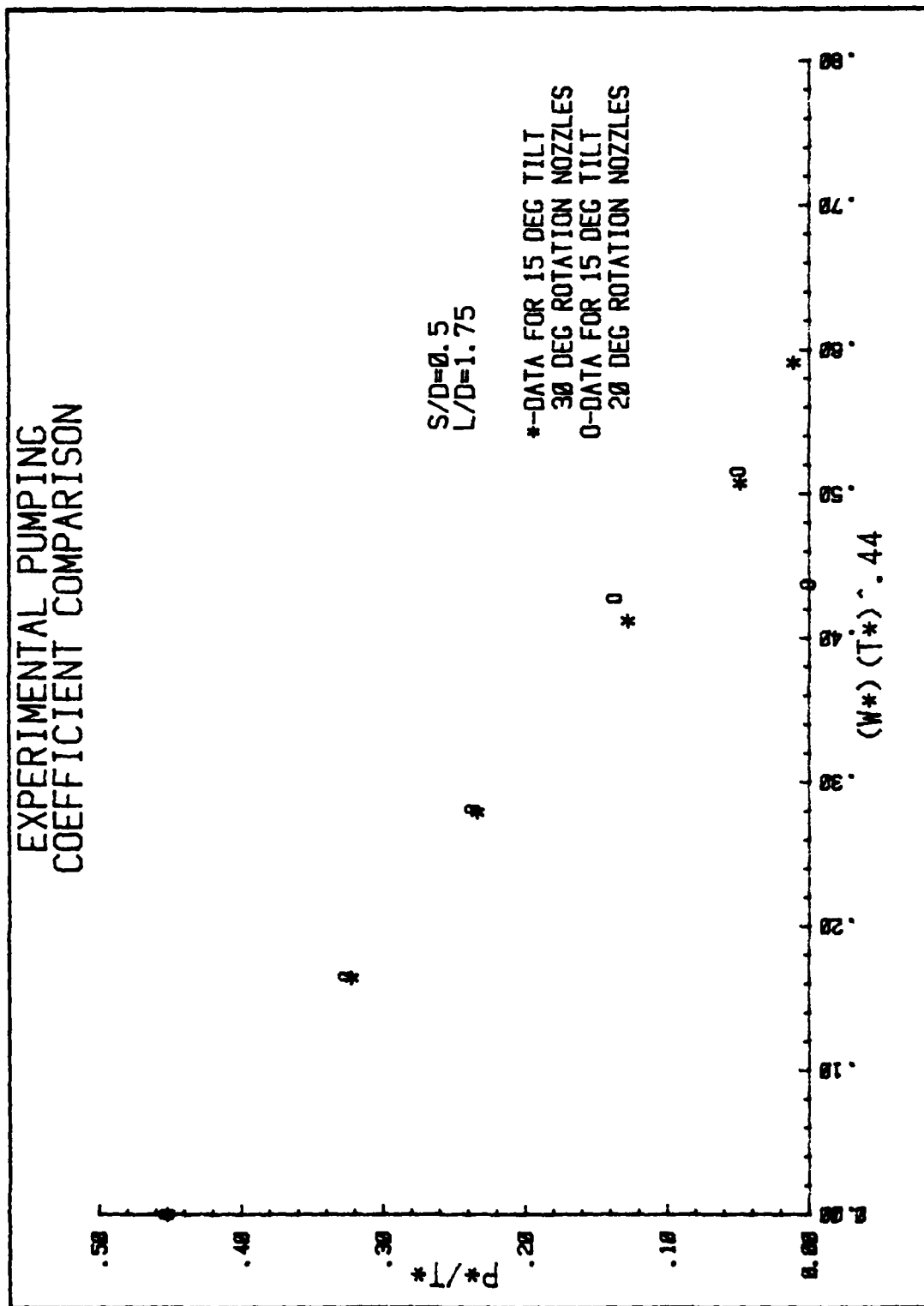


FIGURE 39.1



# AXIAL PRESSURE DISTRIBUTION COMPARISON

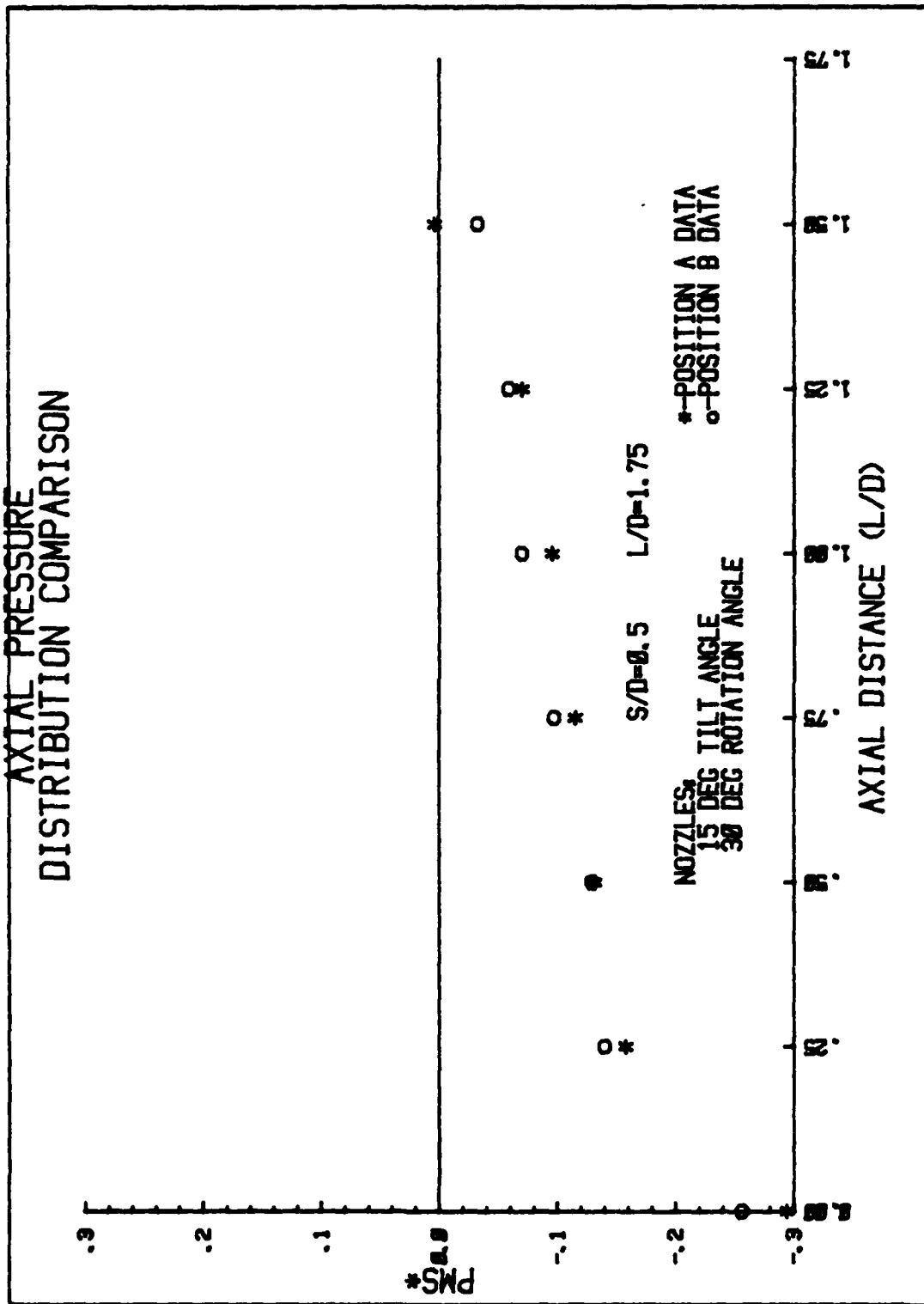


FIGURE 30.2

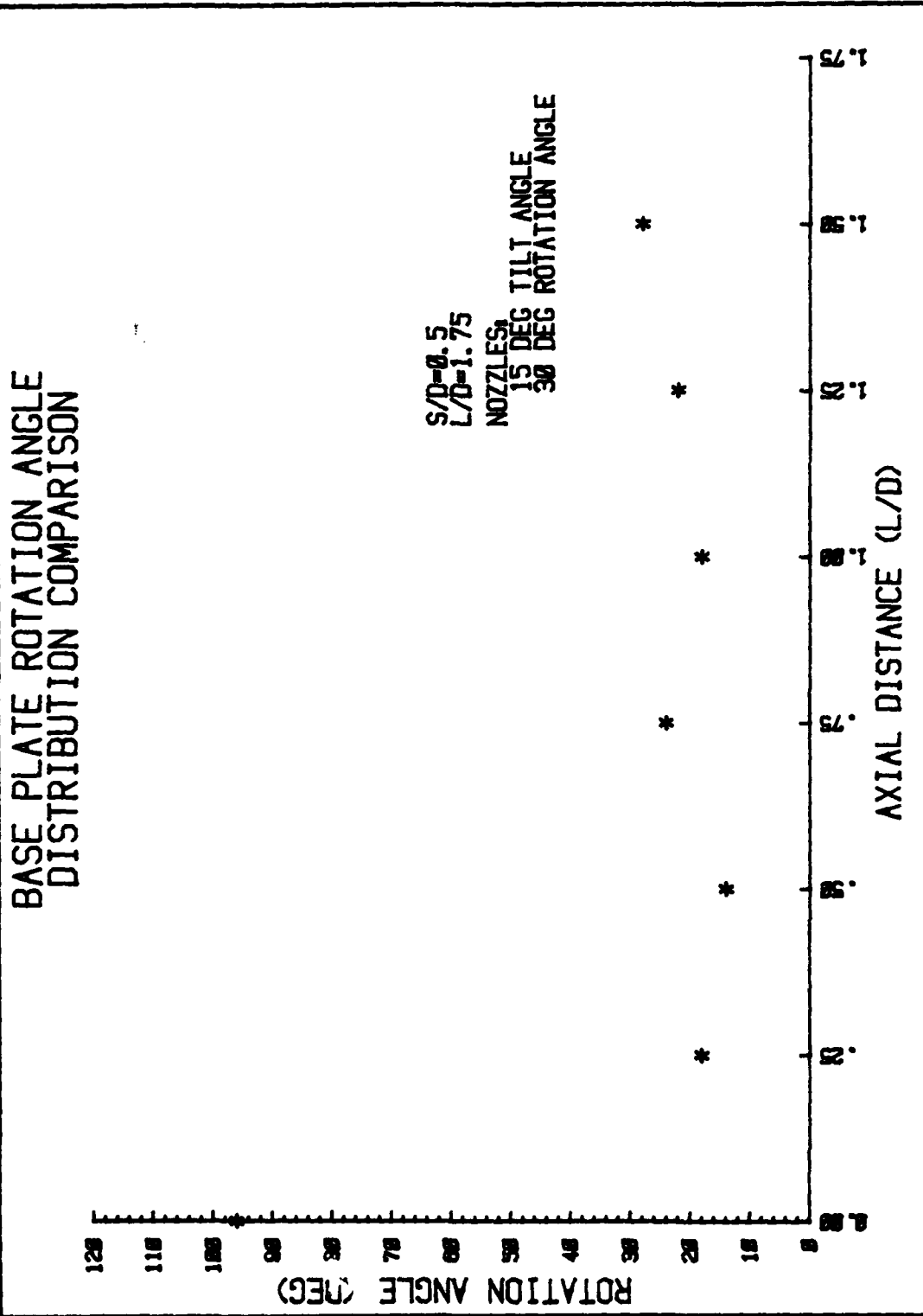
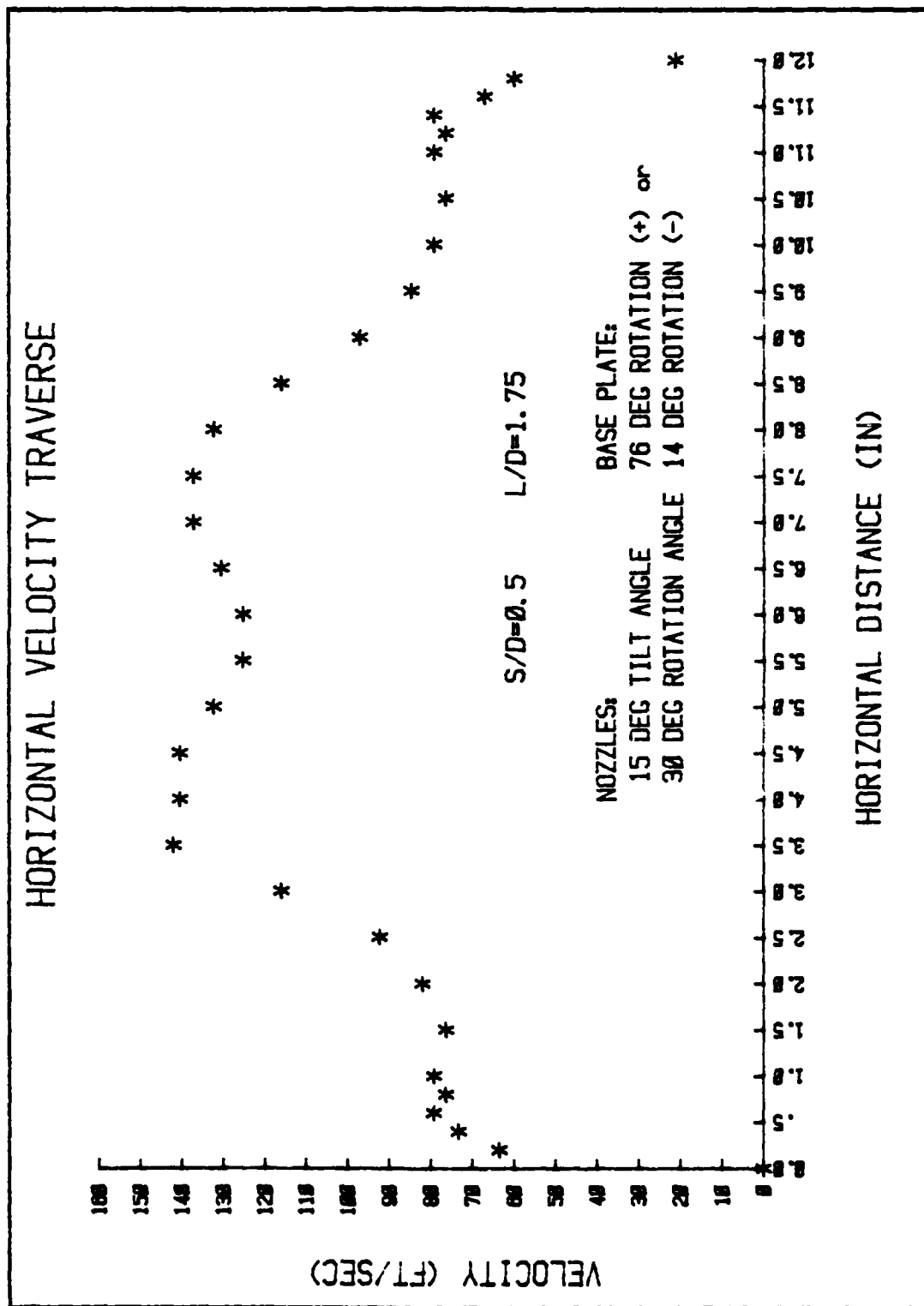


FIGURE 39.3



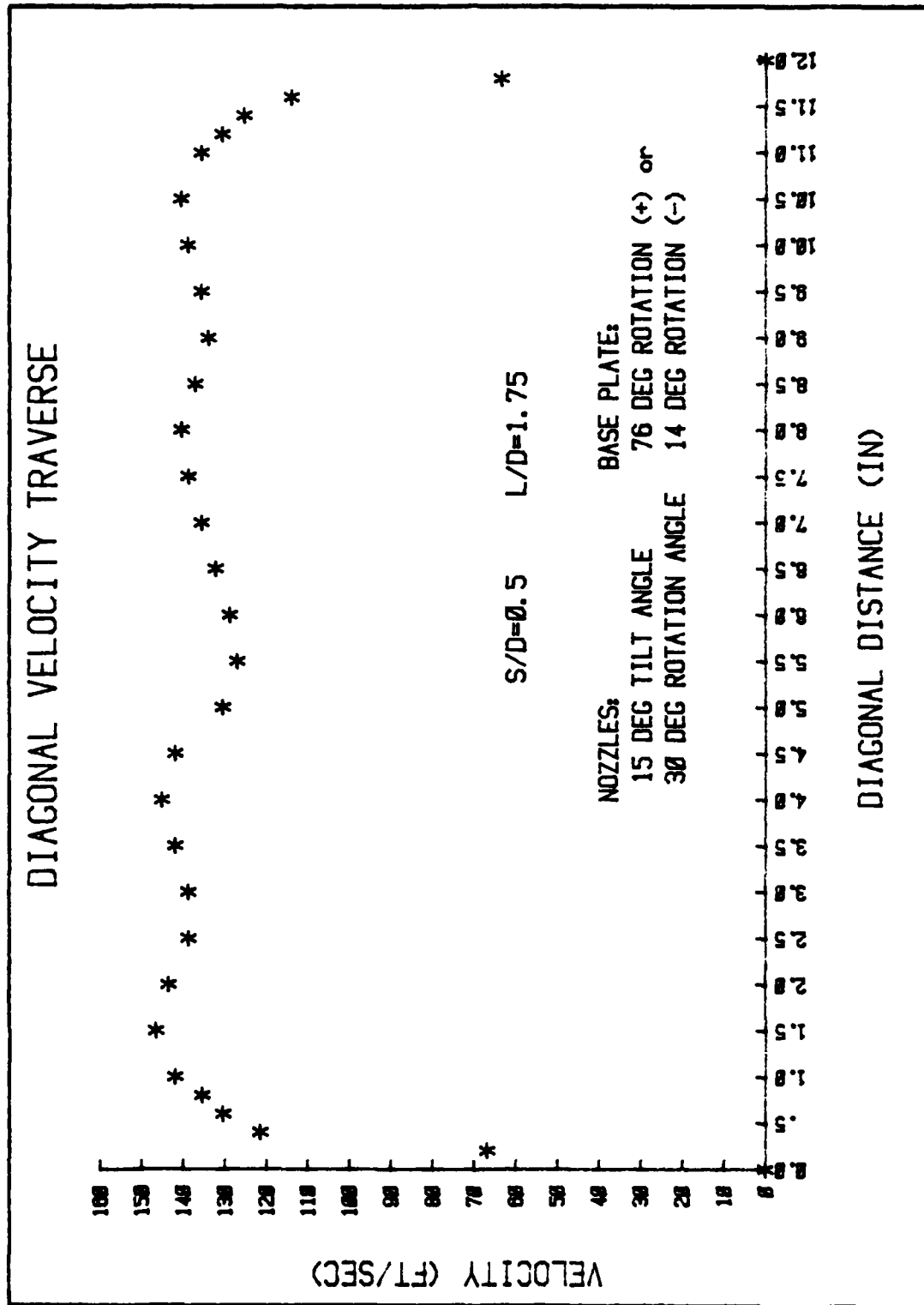


FIGURE 39.5

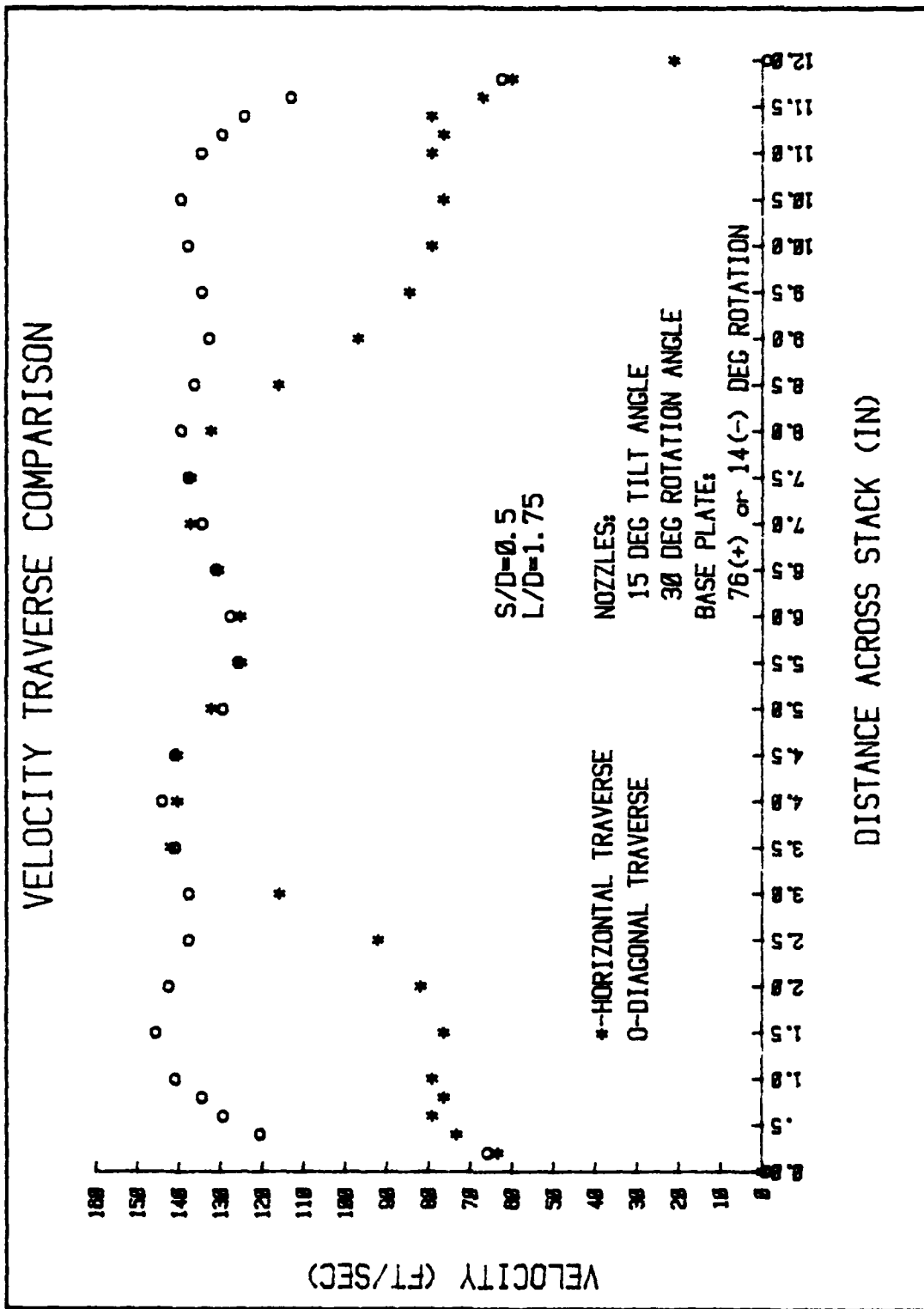


FIGURE 39.6

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

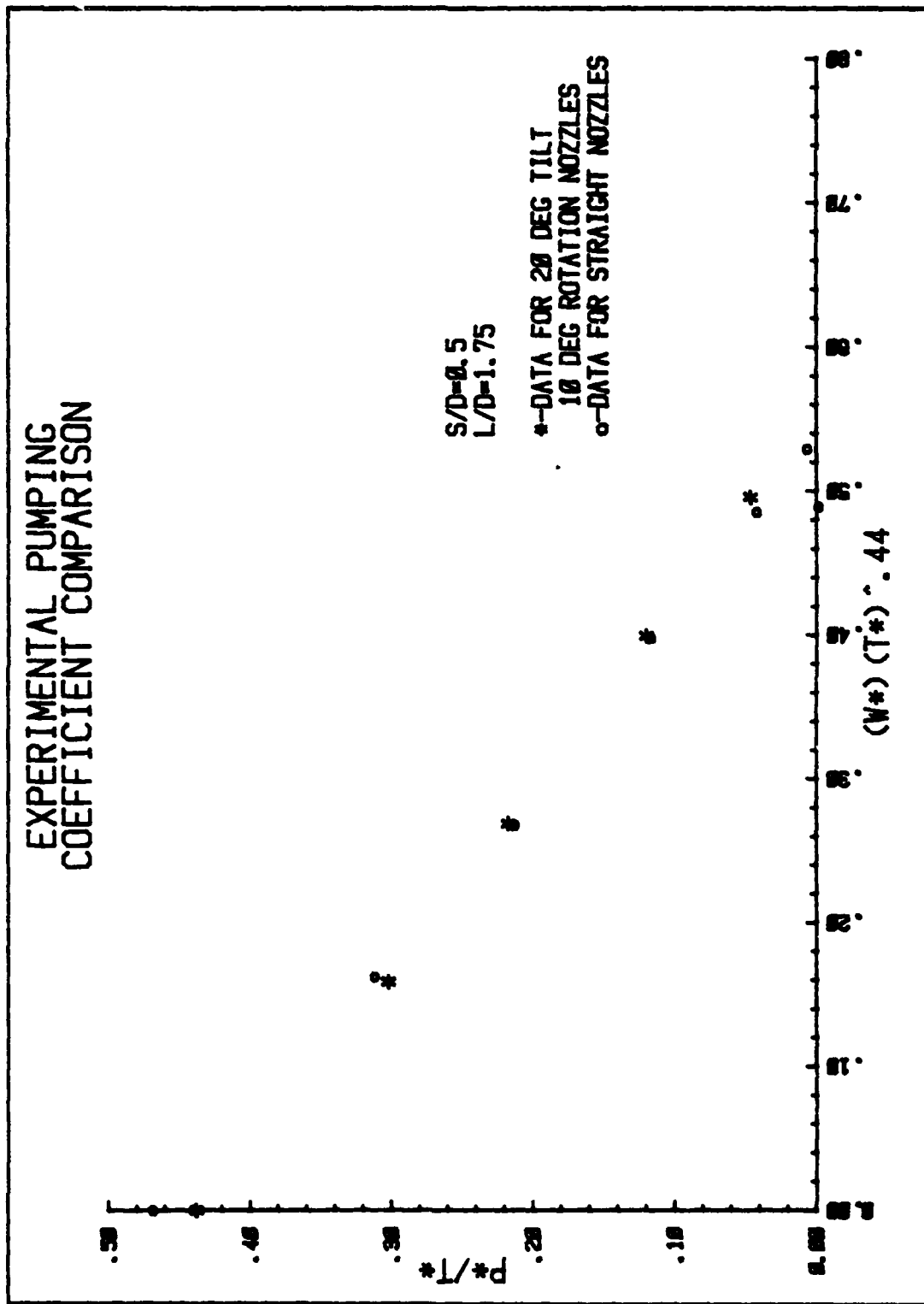


FIGURE 40

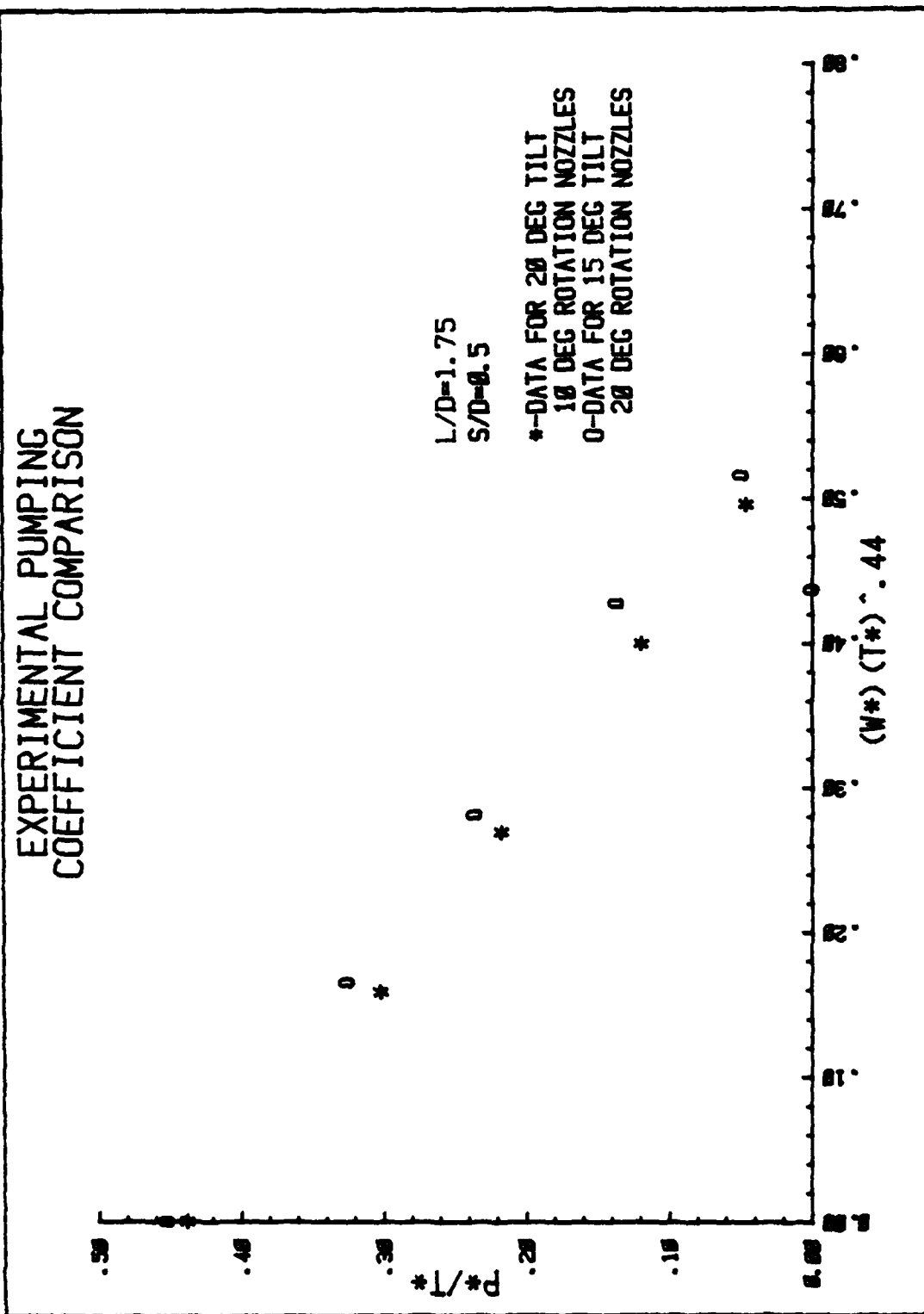


FIGURE 40.1

# AXIAL PRESSURE DISTRIBUTION COMPARISON

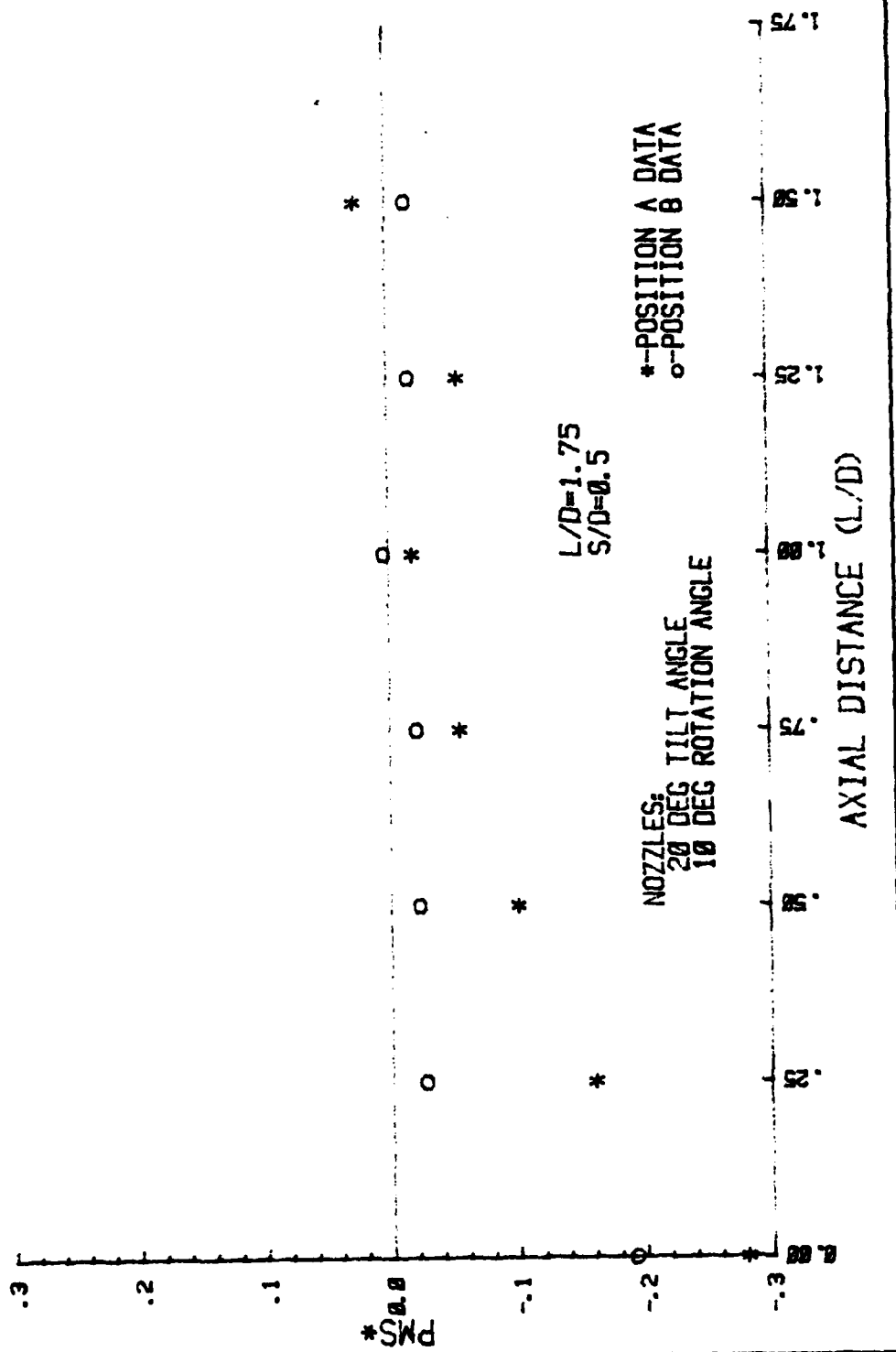


FIGURE 40.2



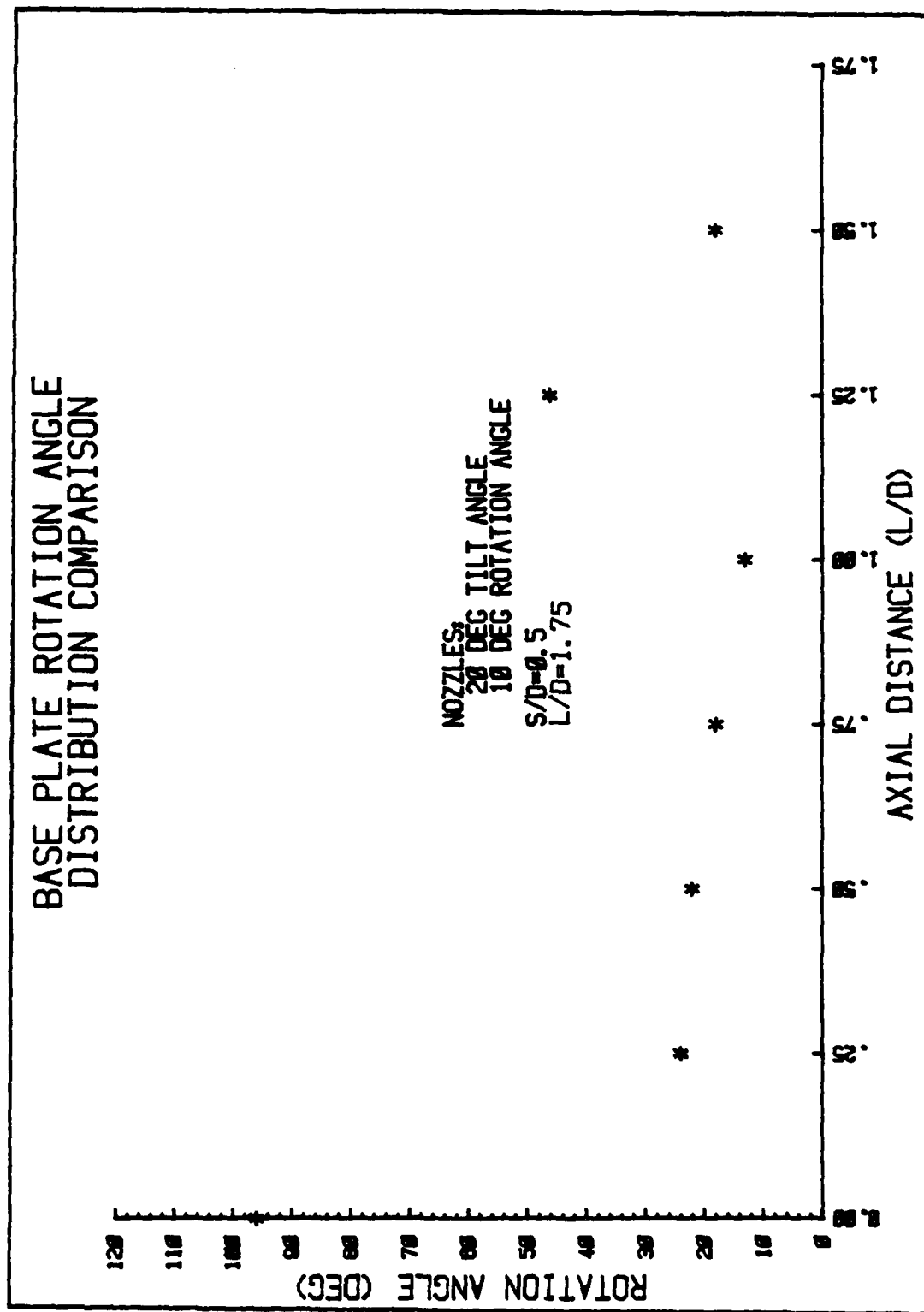


FIGURE 40.3

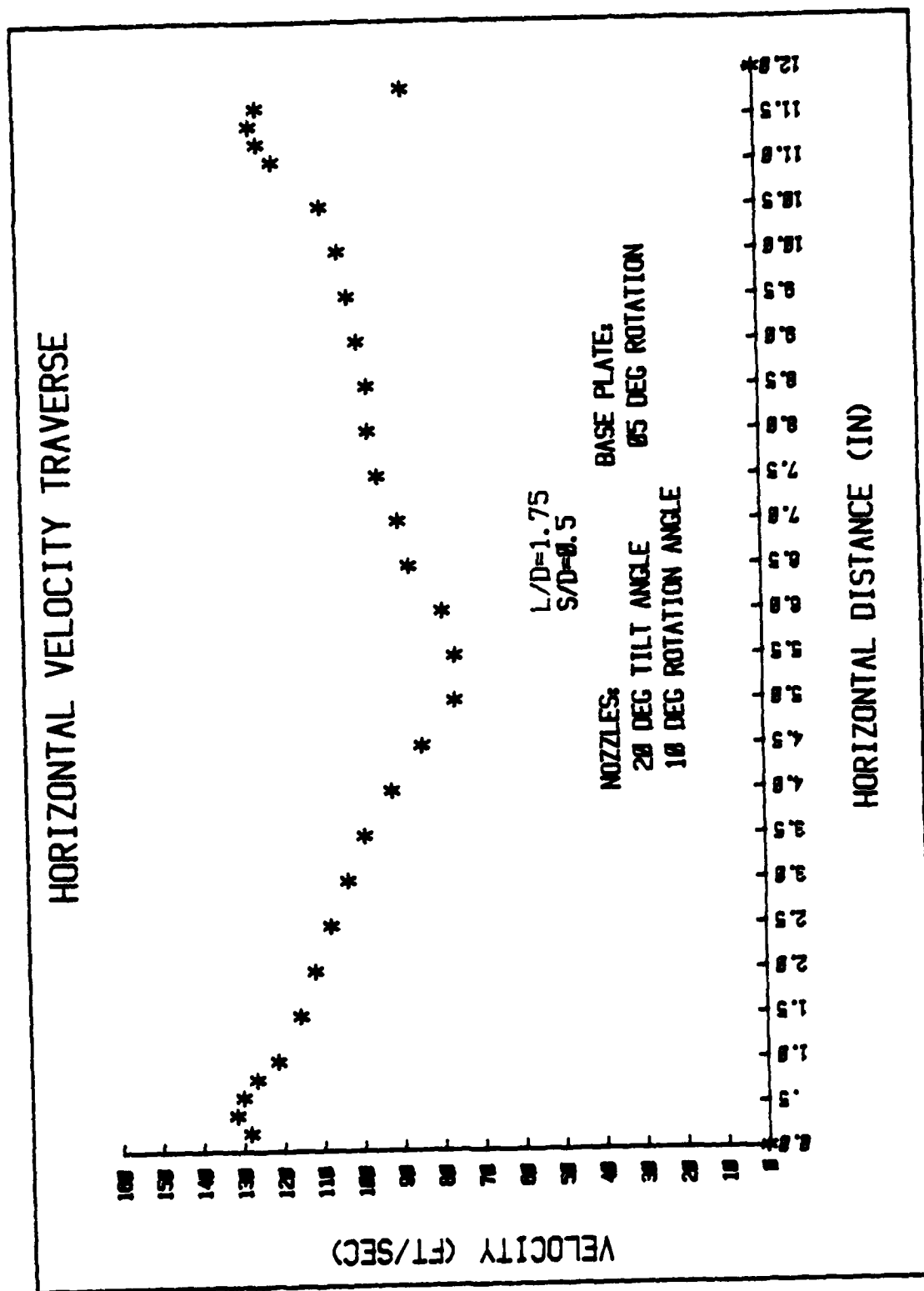


FIGURE 40.4

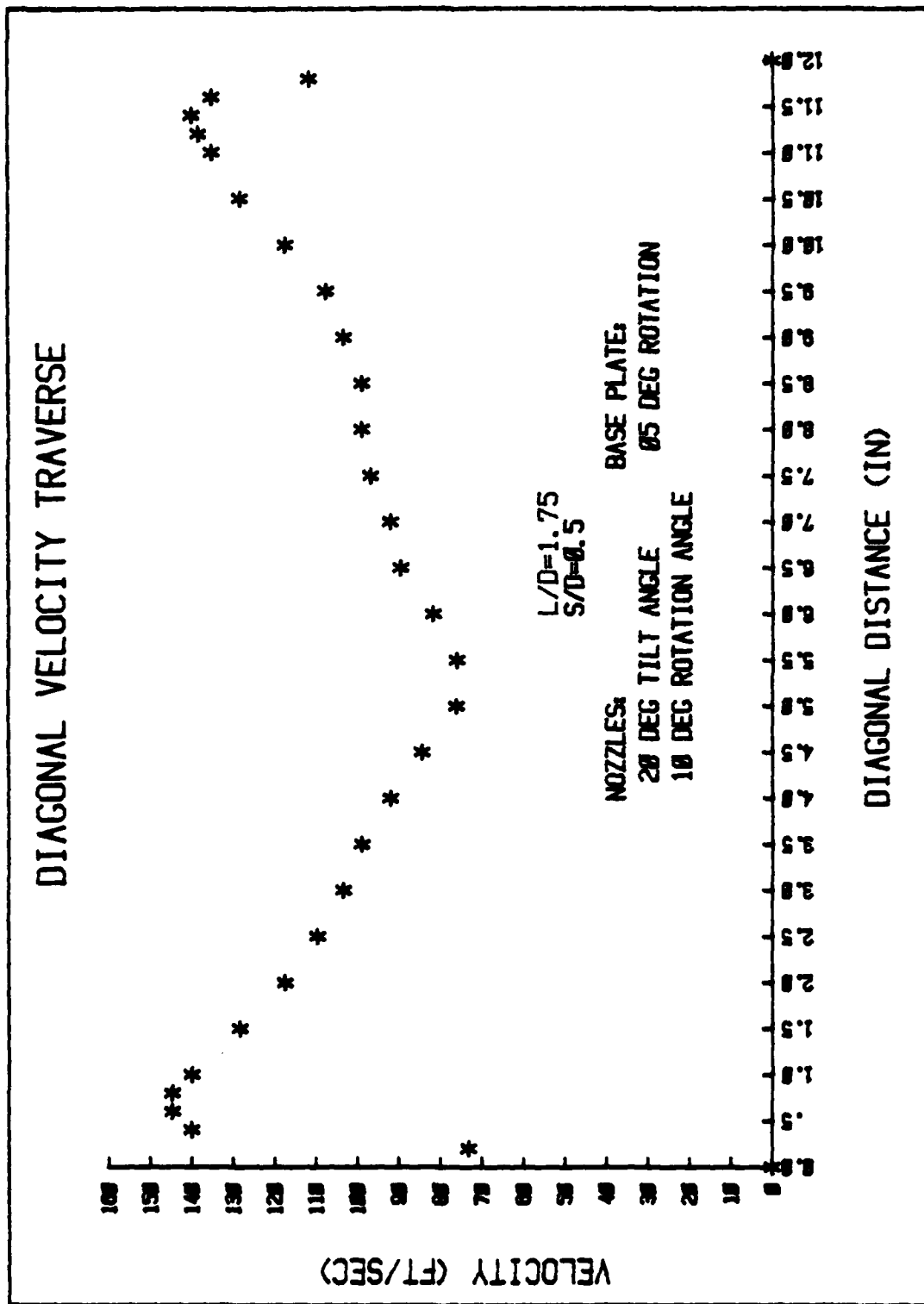
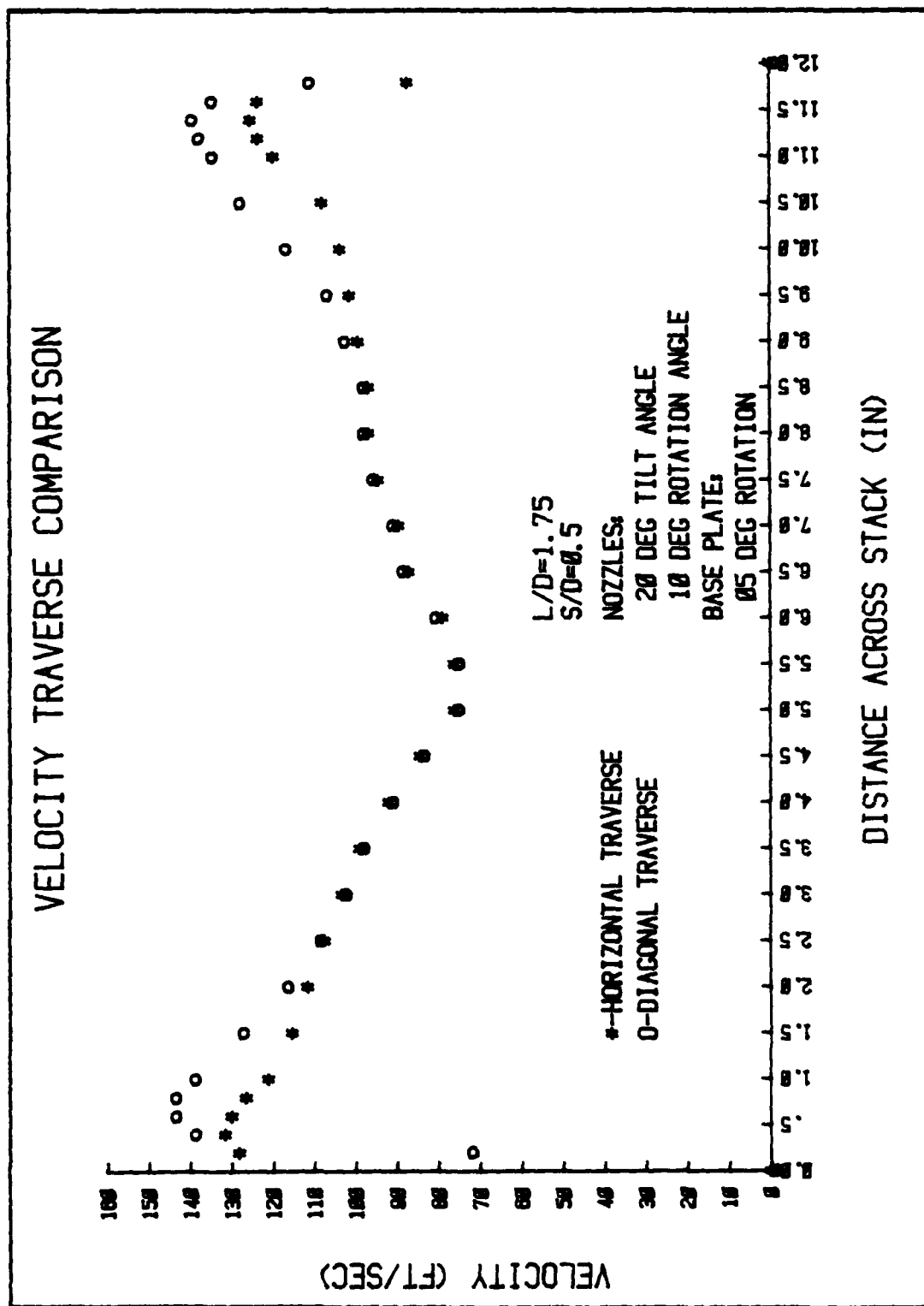


FIGURE 40.5



**FIGURE 40.6**

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

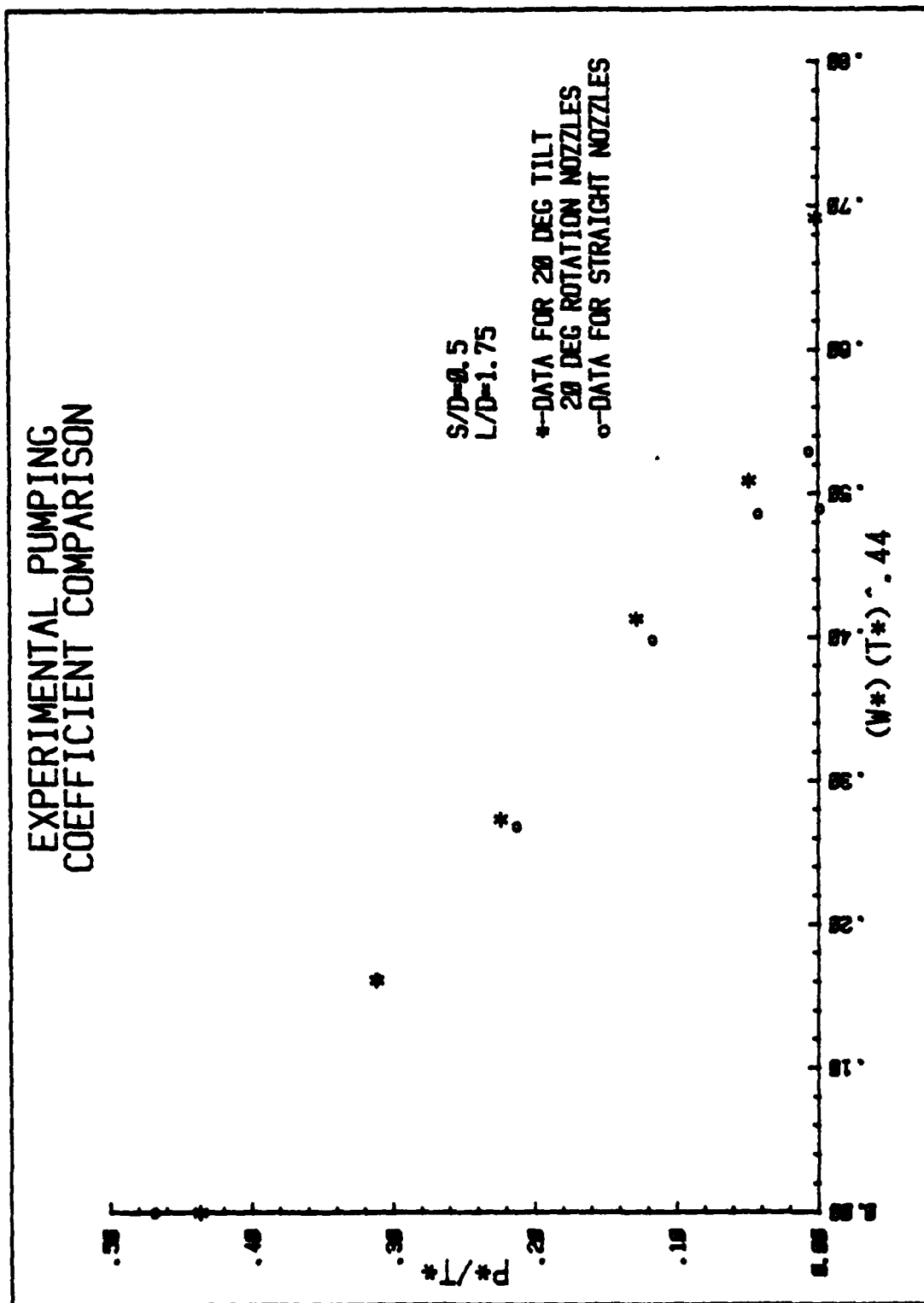


FIGURE 41

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

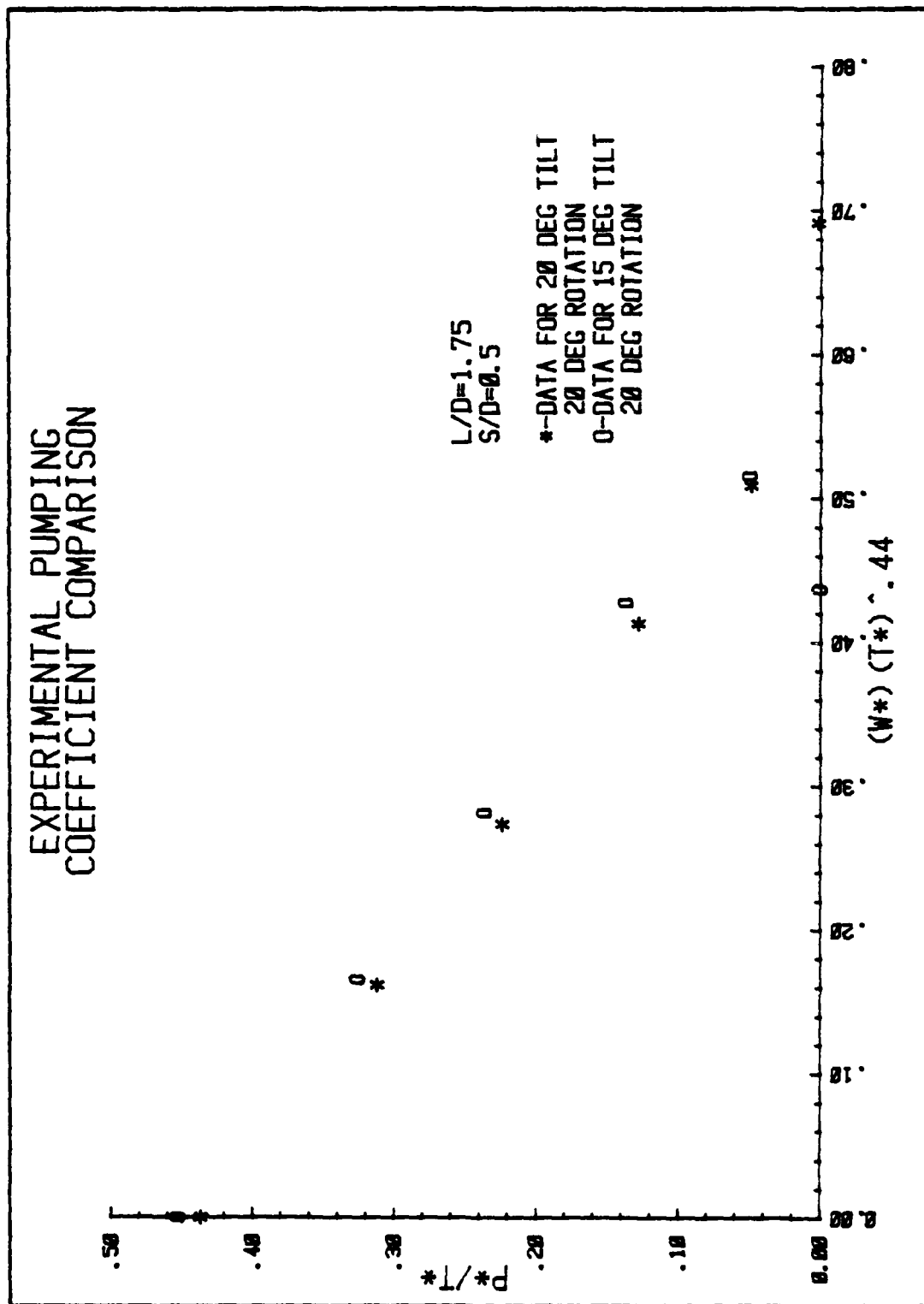


FIGURE 41.1

# AXIAL PRESSURE DISTRIBUTION COMPARISON

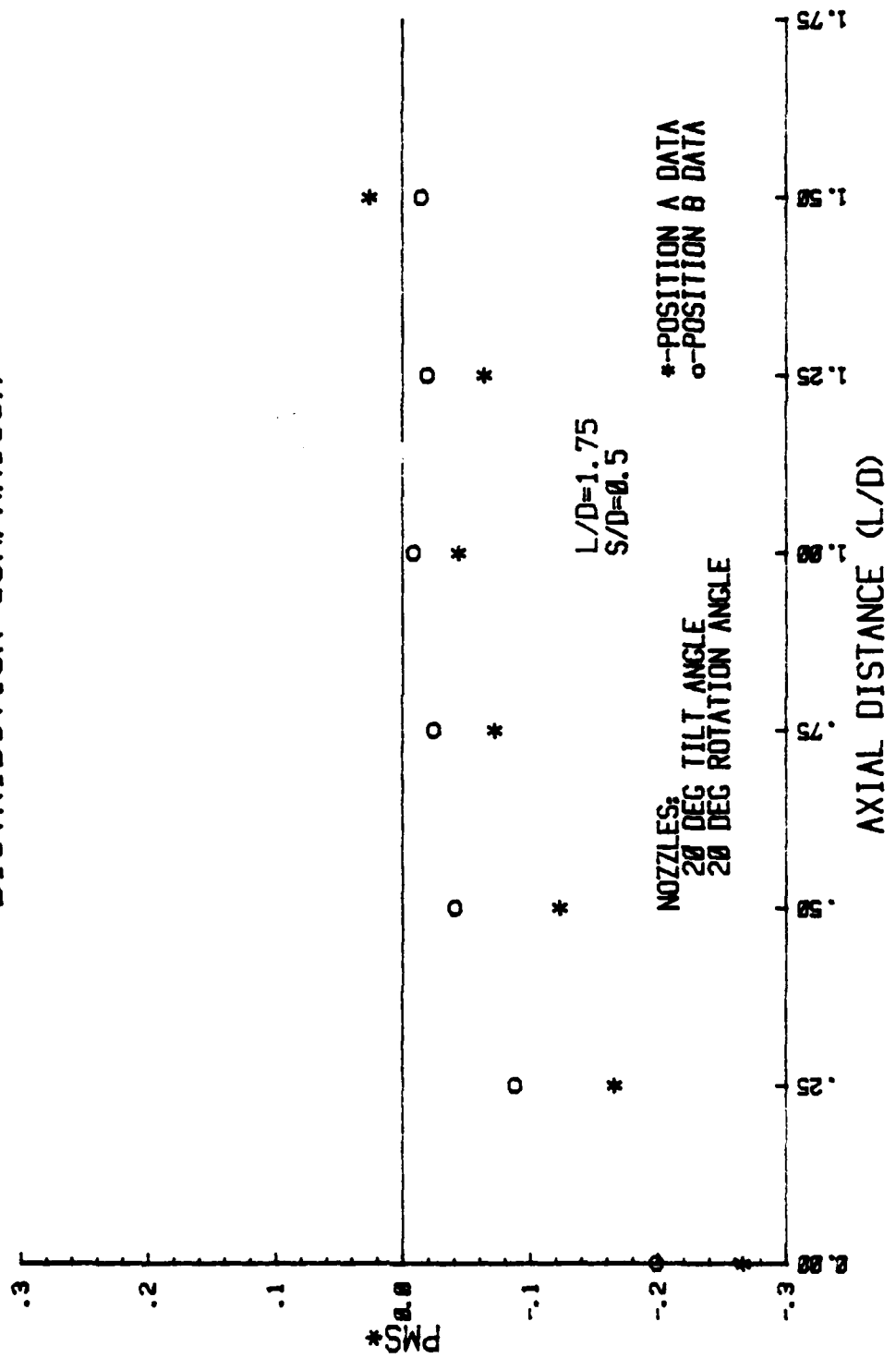


FIGURE 41.2

# BASE PLATE ROTATION ANGLE DISTRIBUTION COMPARISON

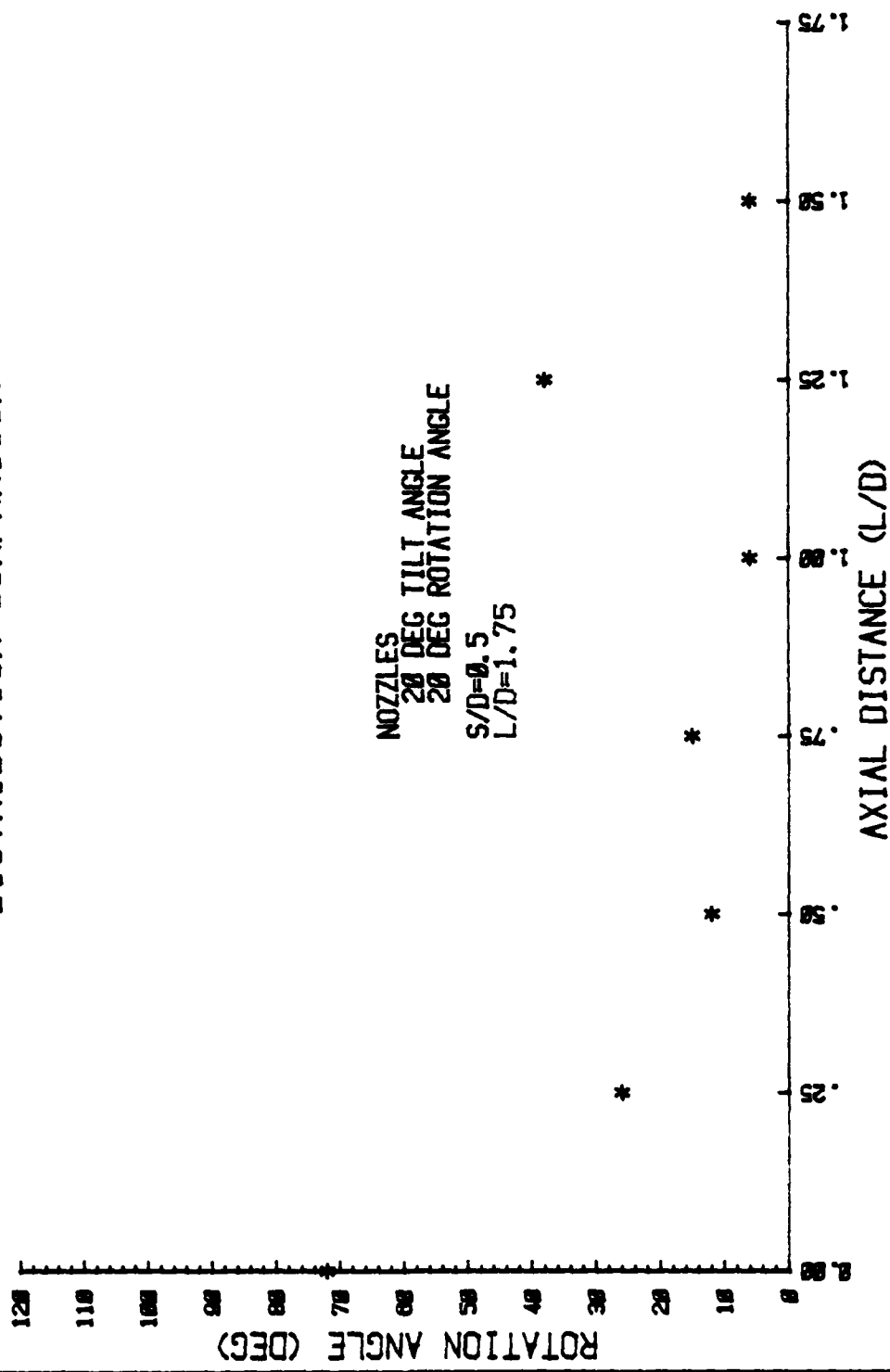


FIGURE 41.3



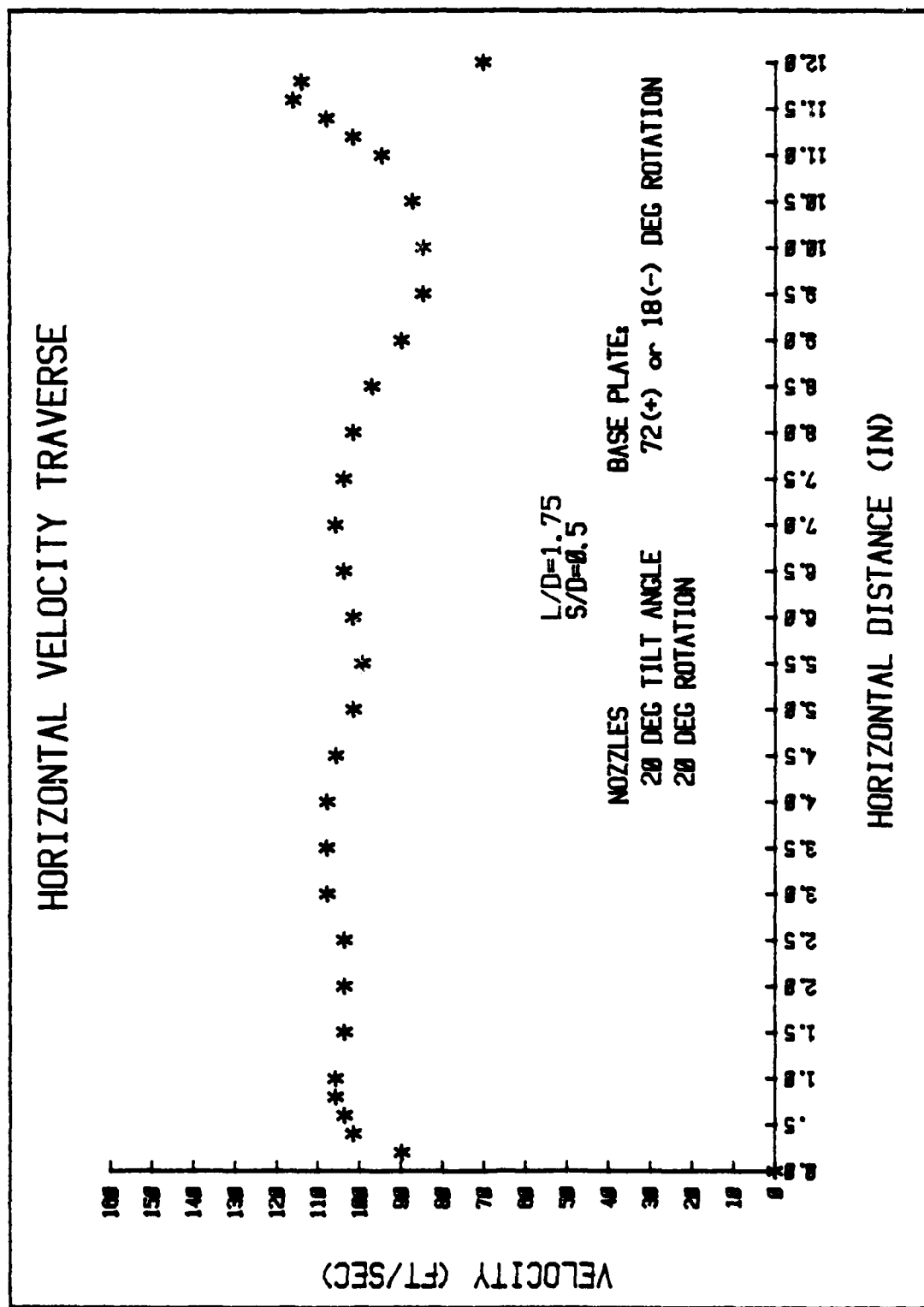


FIGURE 41.4

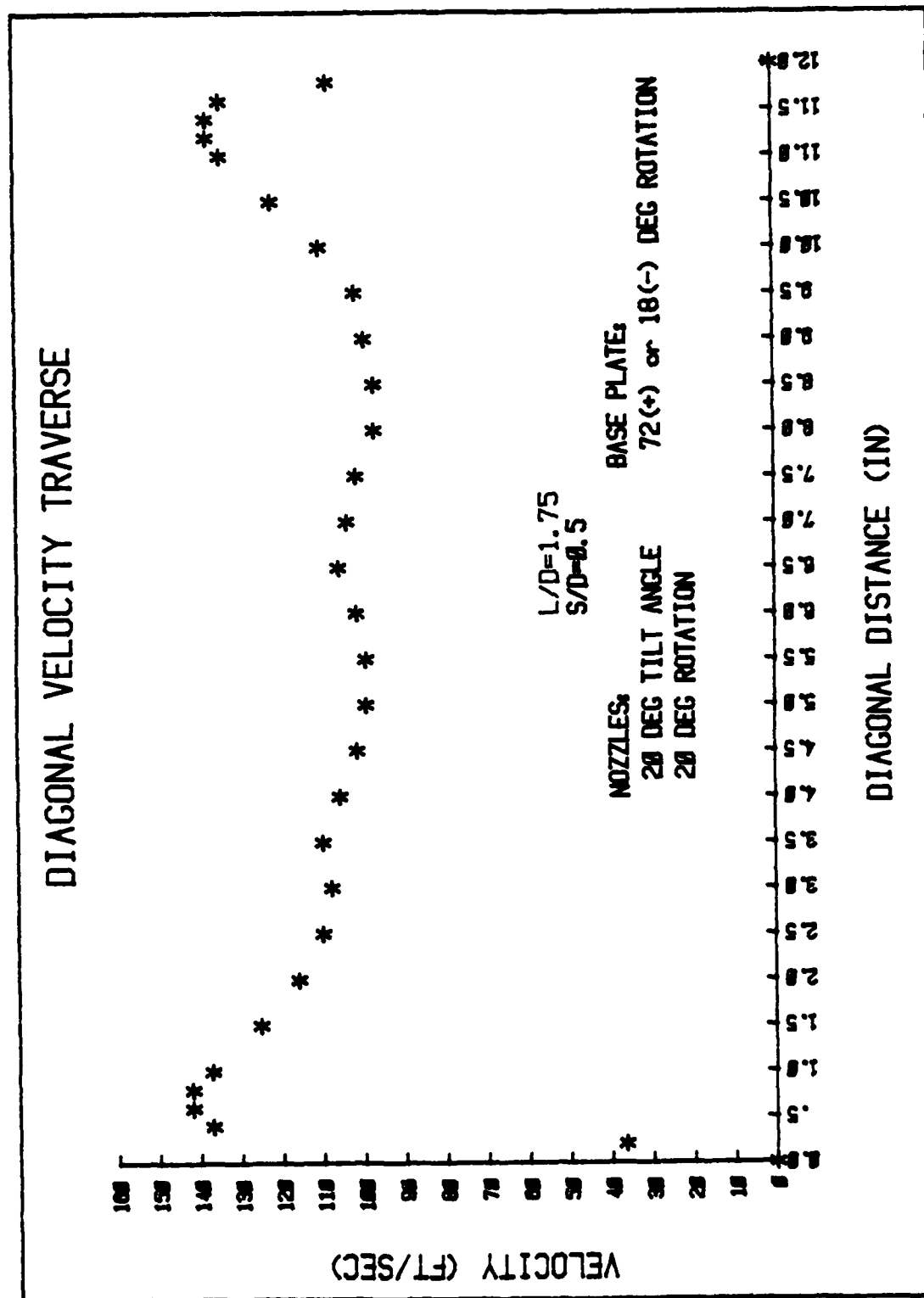


FIGURE 41.5

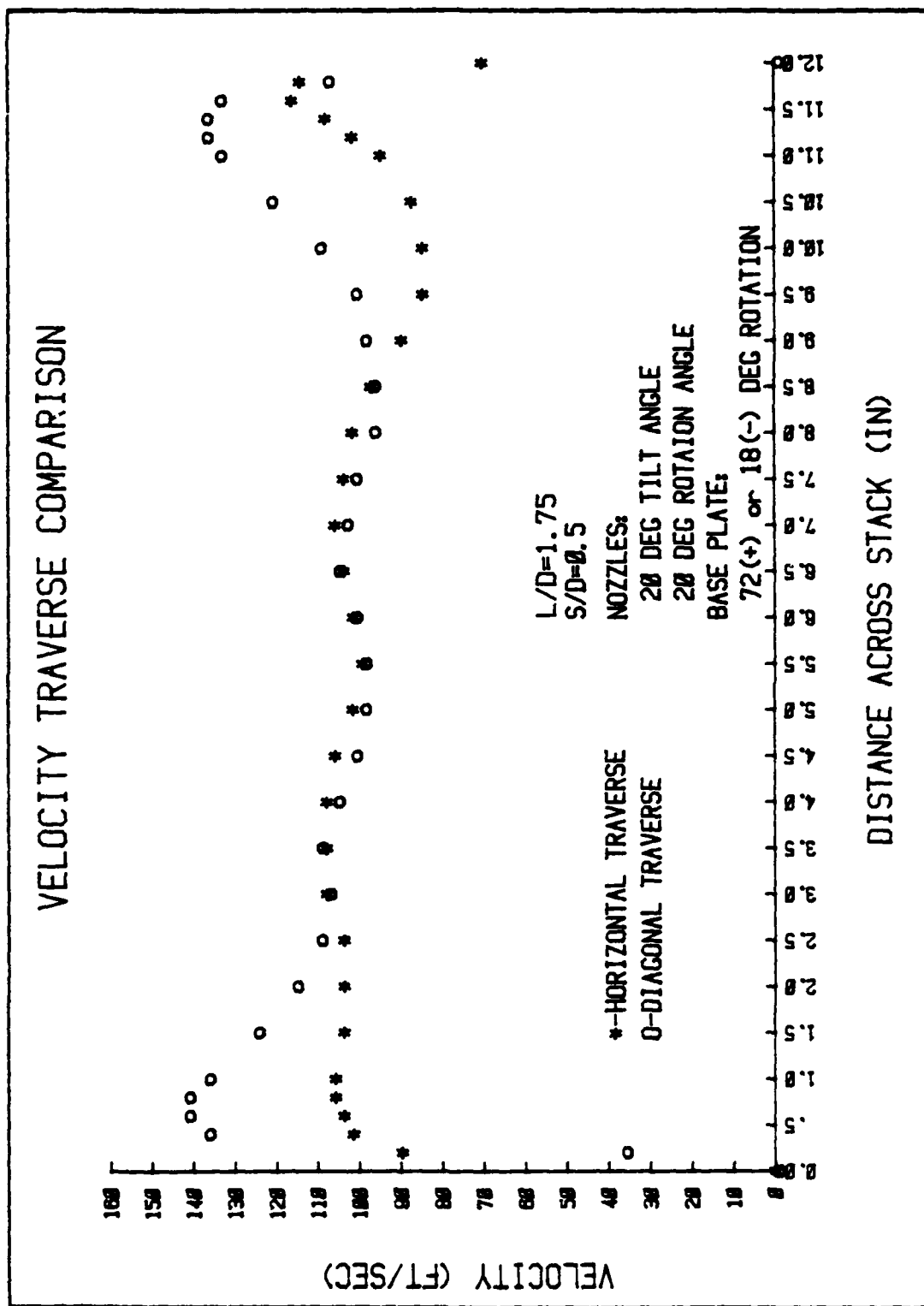


FIGURE 41.6

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

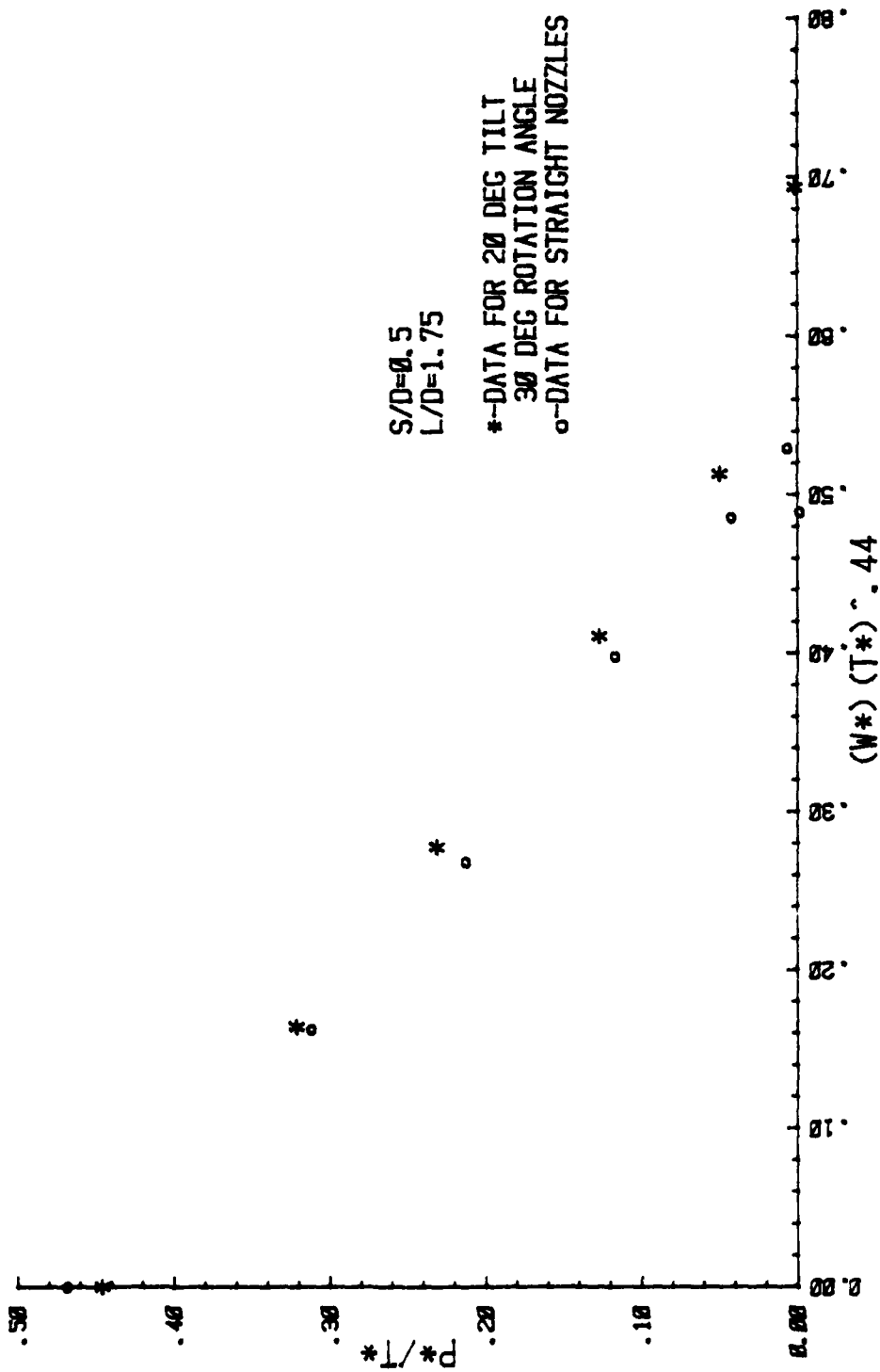


FIGURE 42

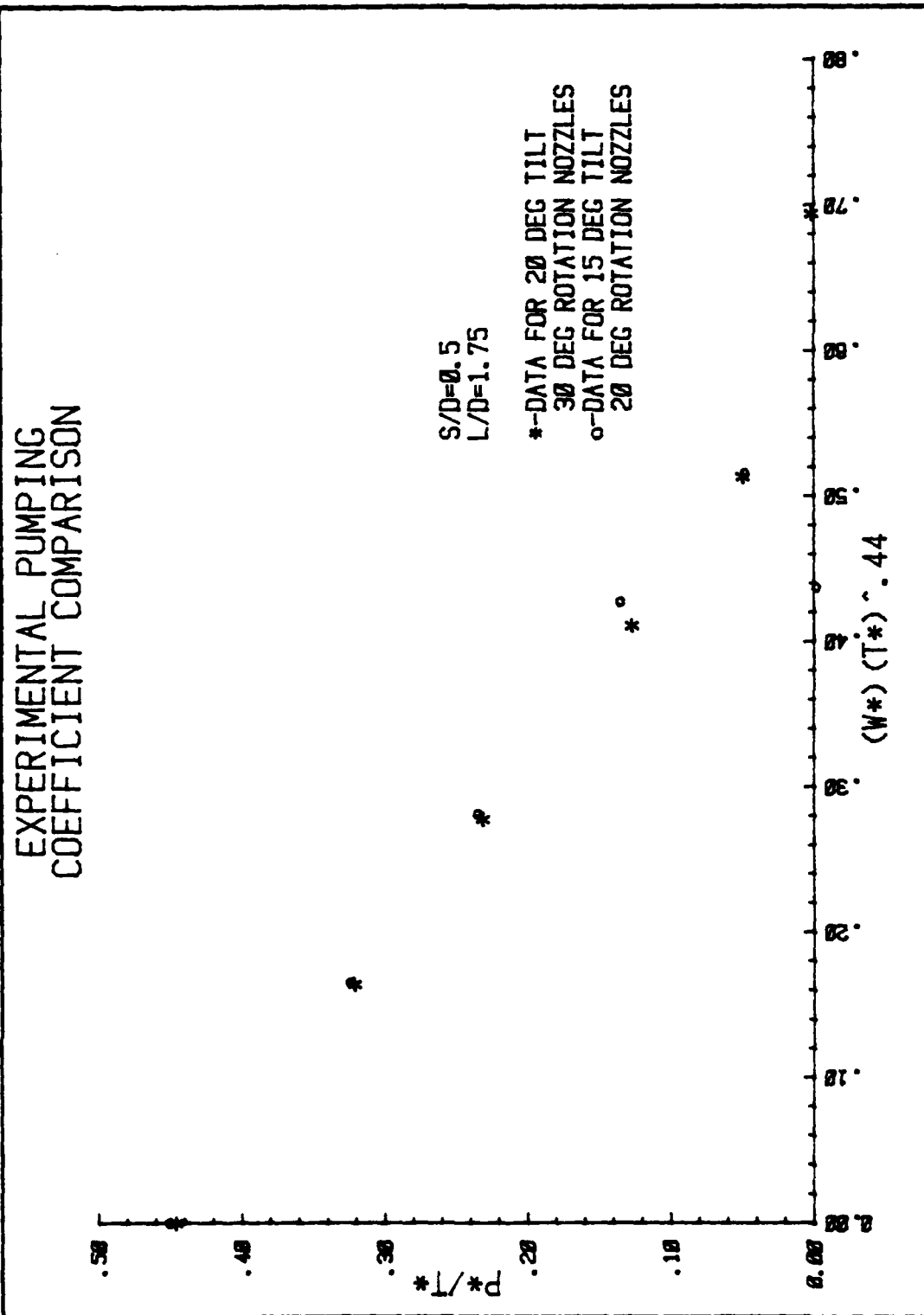


FIGURE 42.1

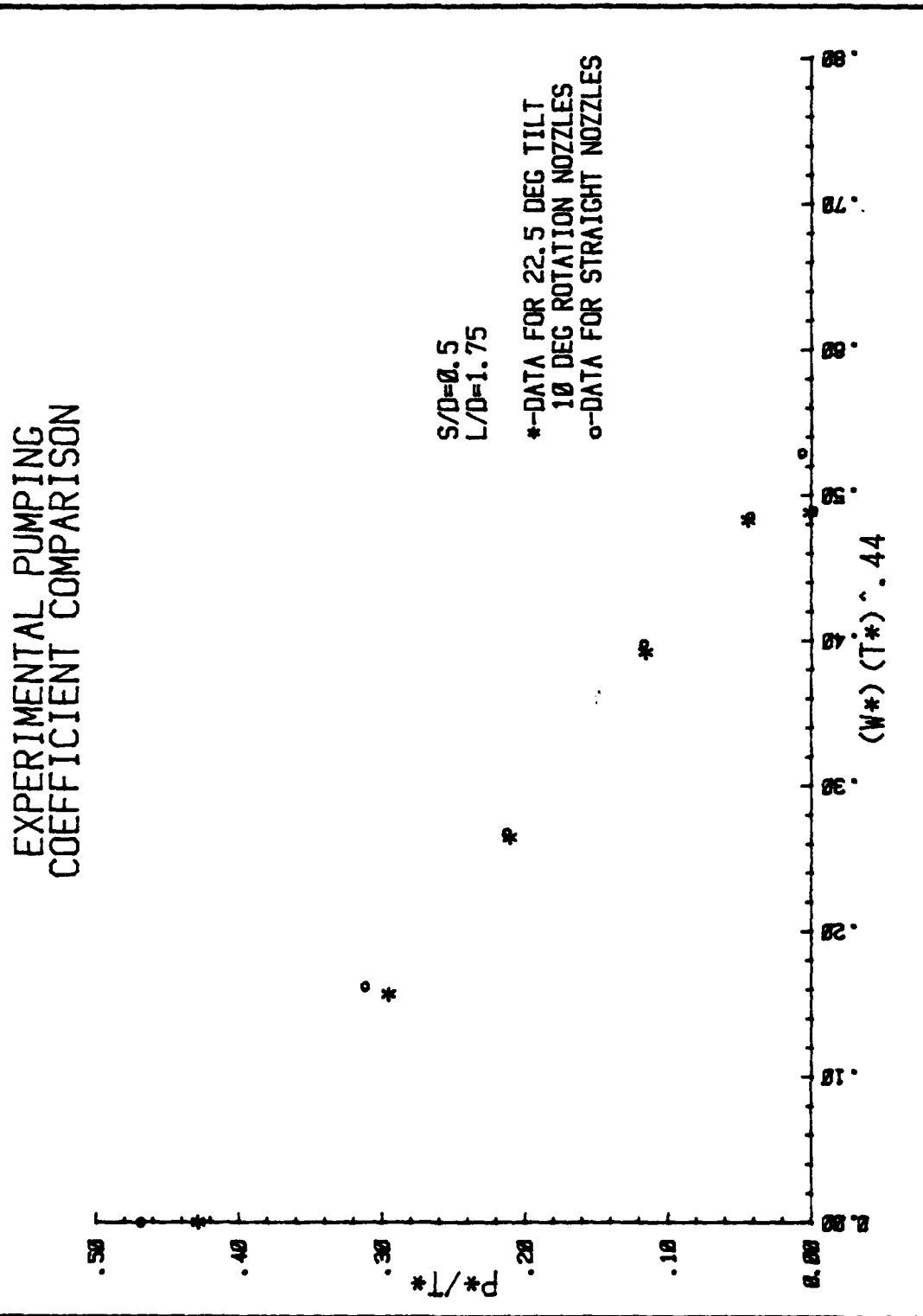


FIGURE 43

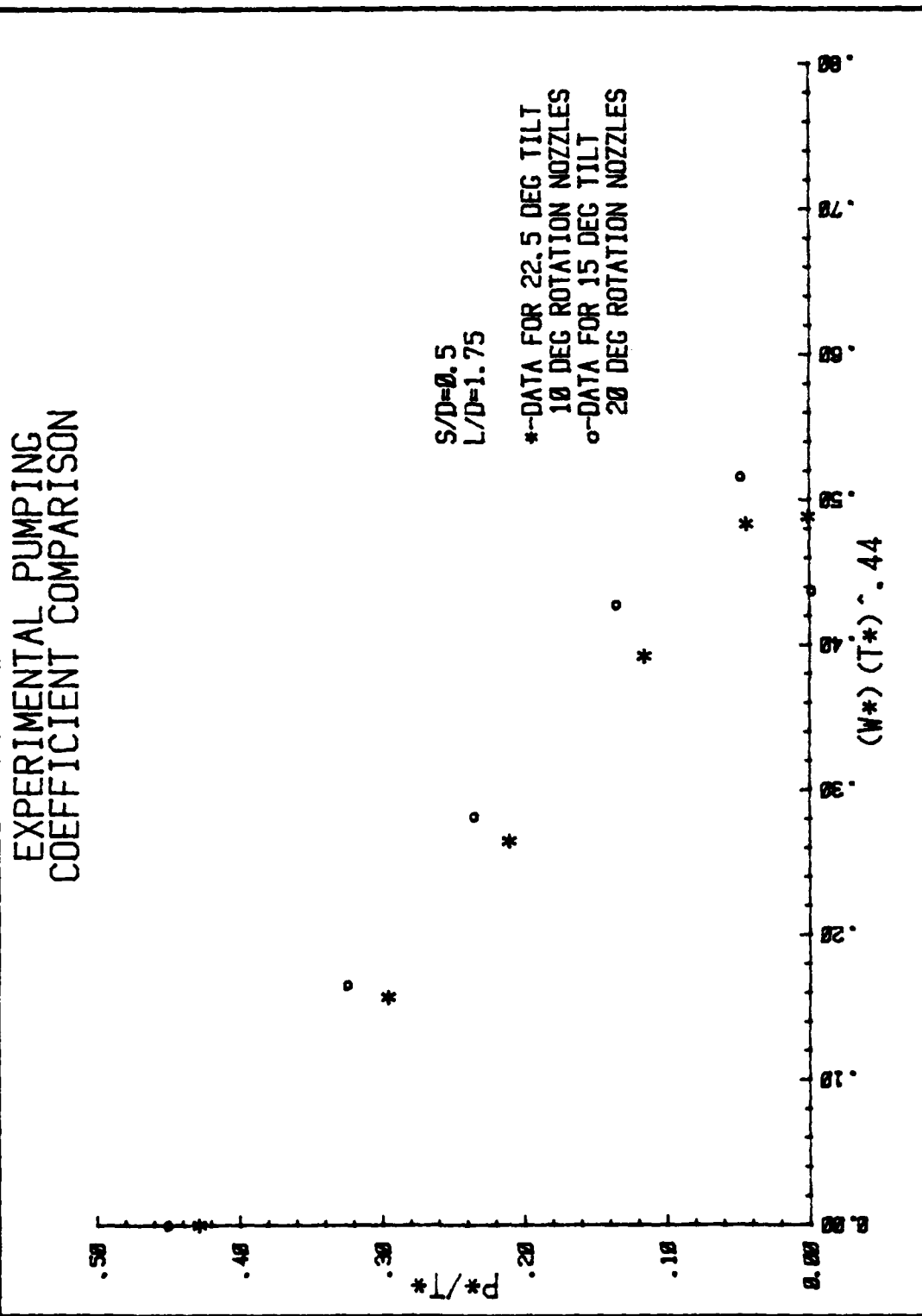


FIGURE 43.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

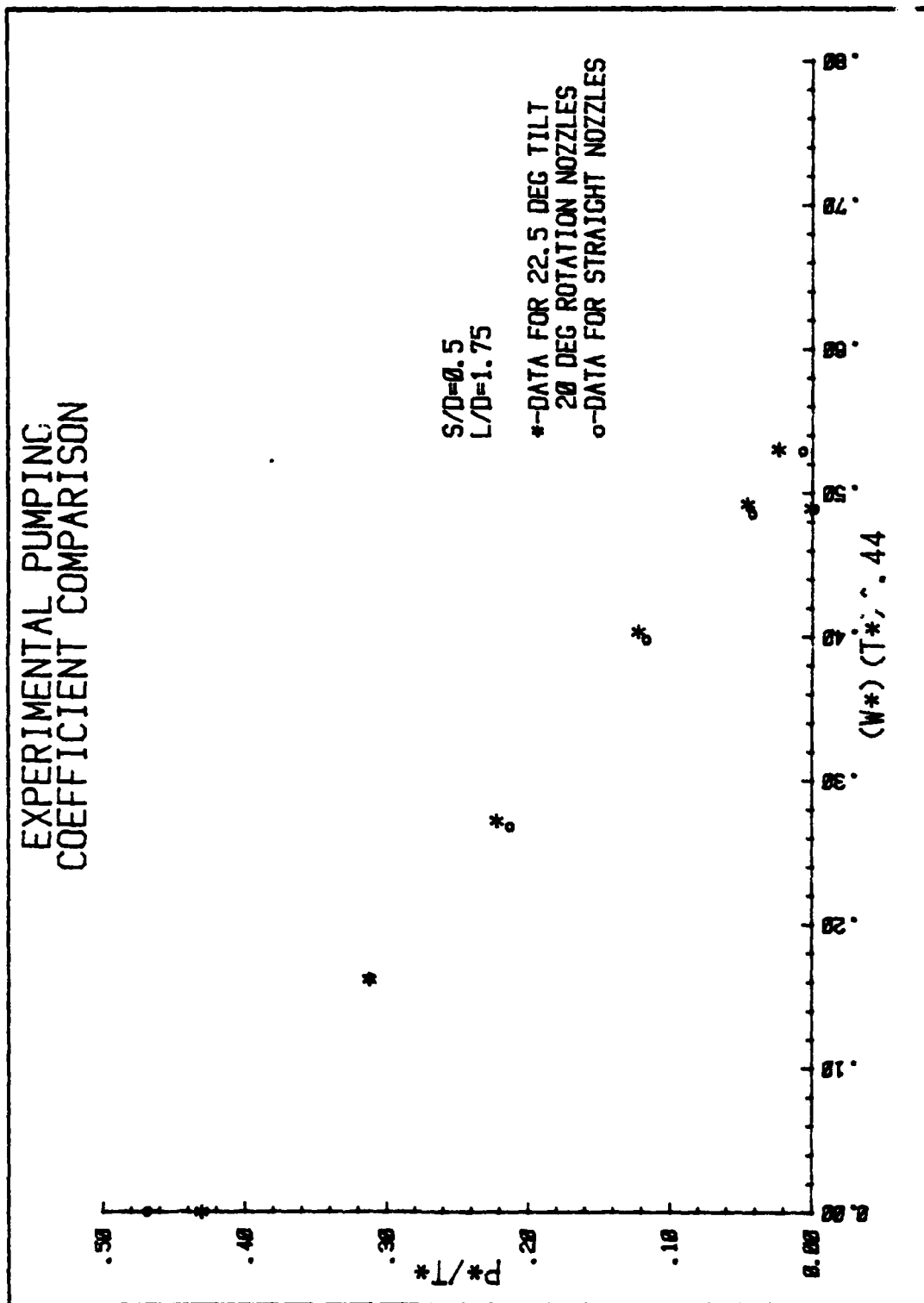


FIGURE 44



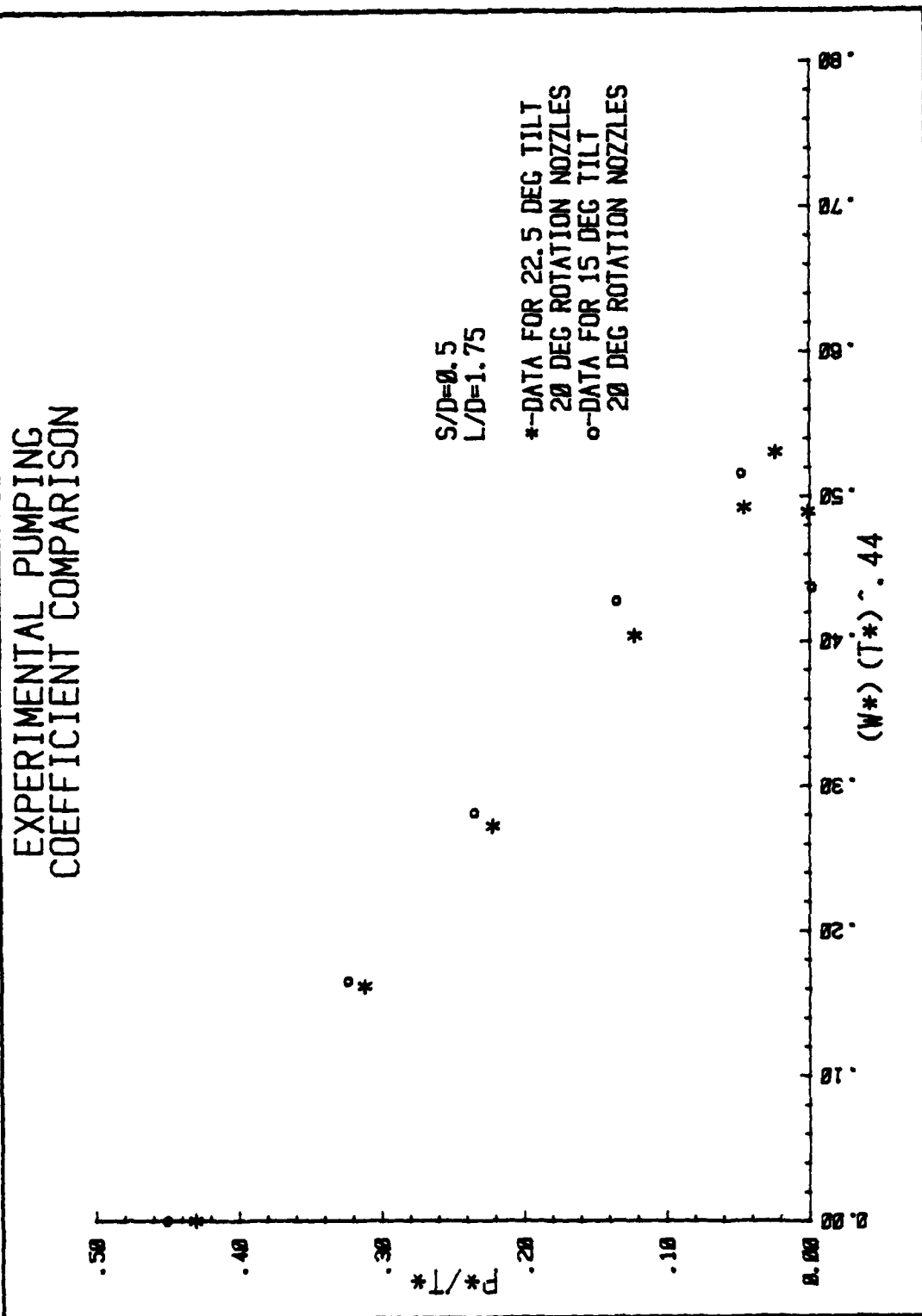


FIGURE 44.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

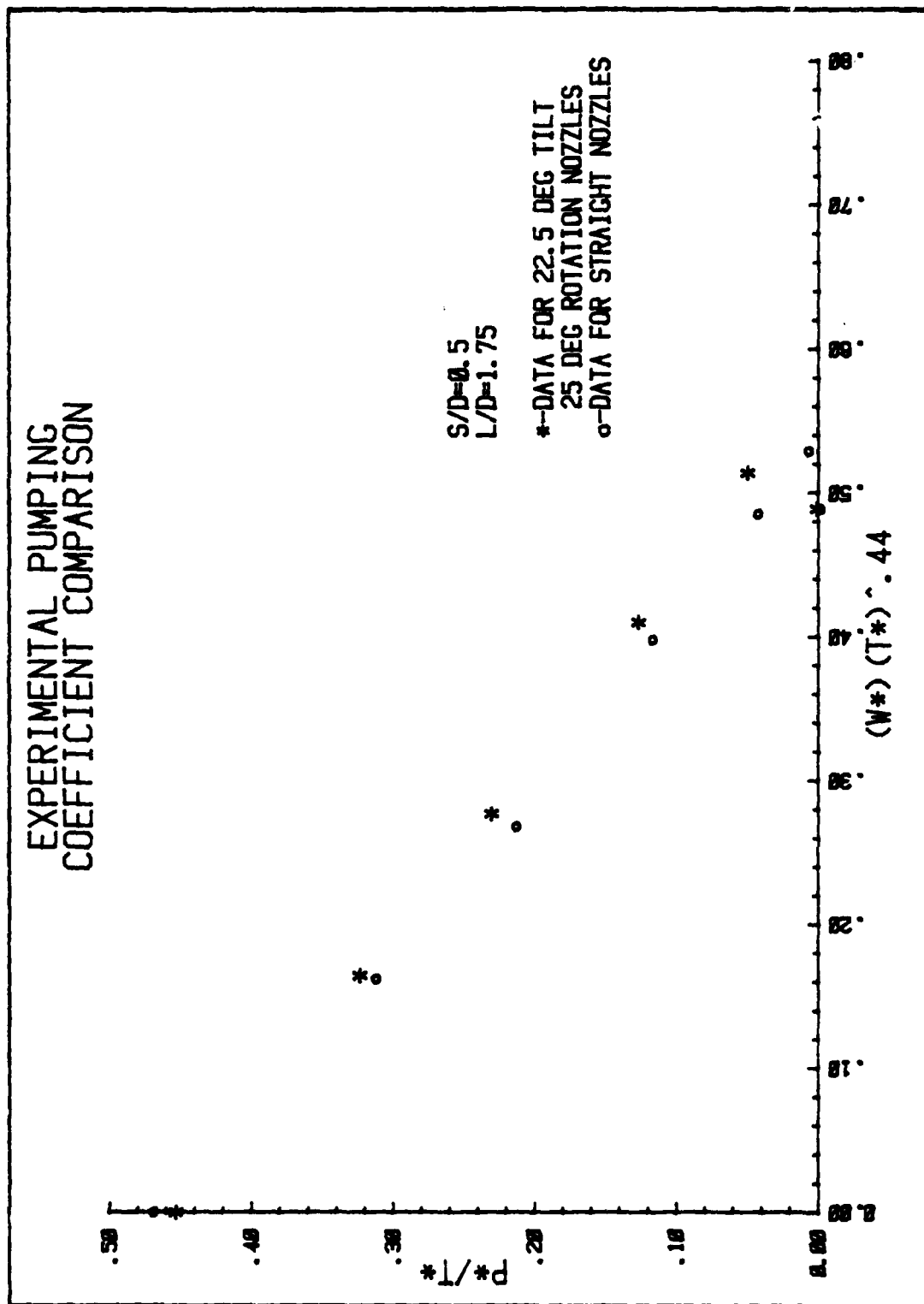


FIGURE 45

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

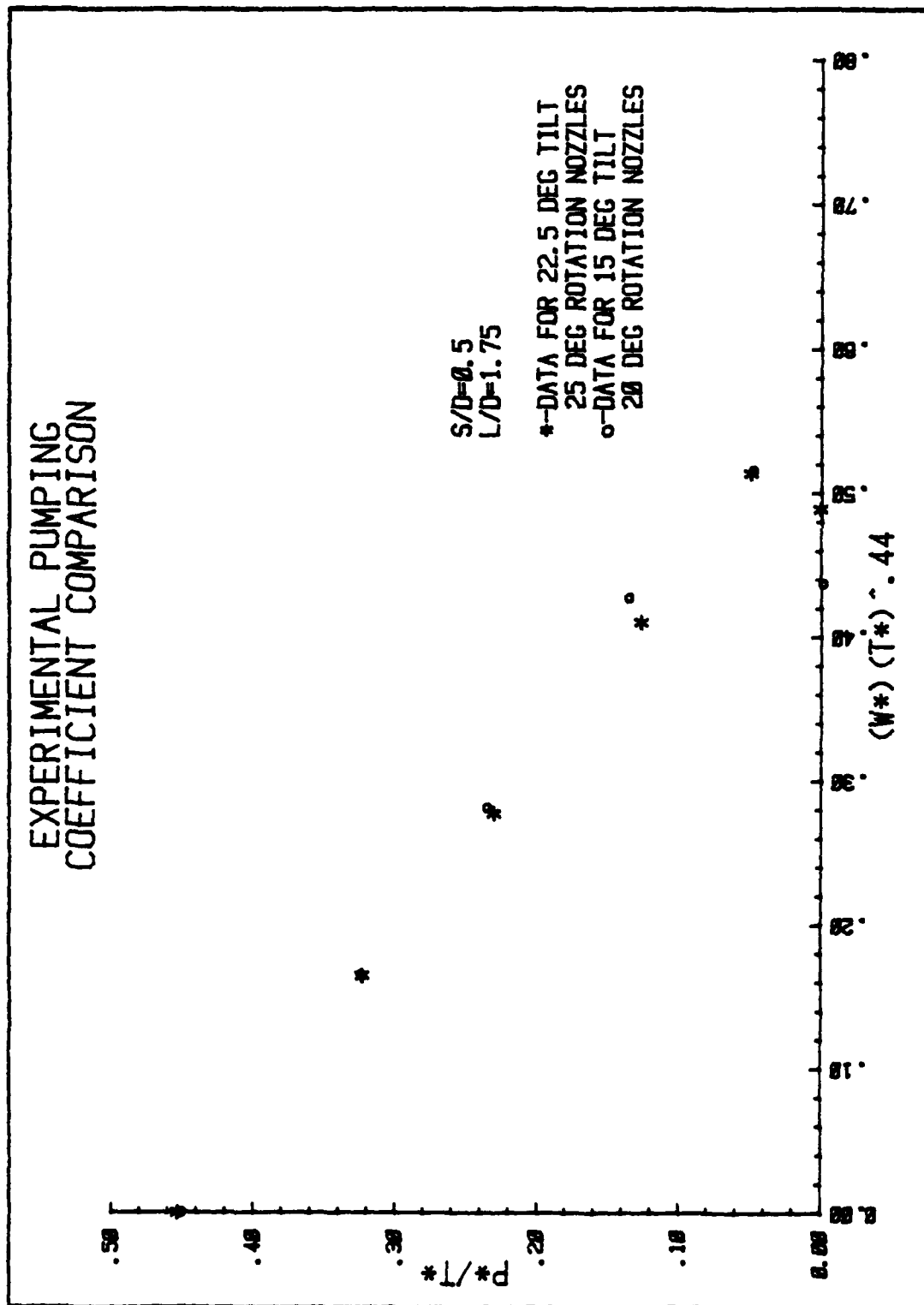


FIGURE 45.1

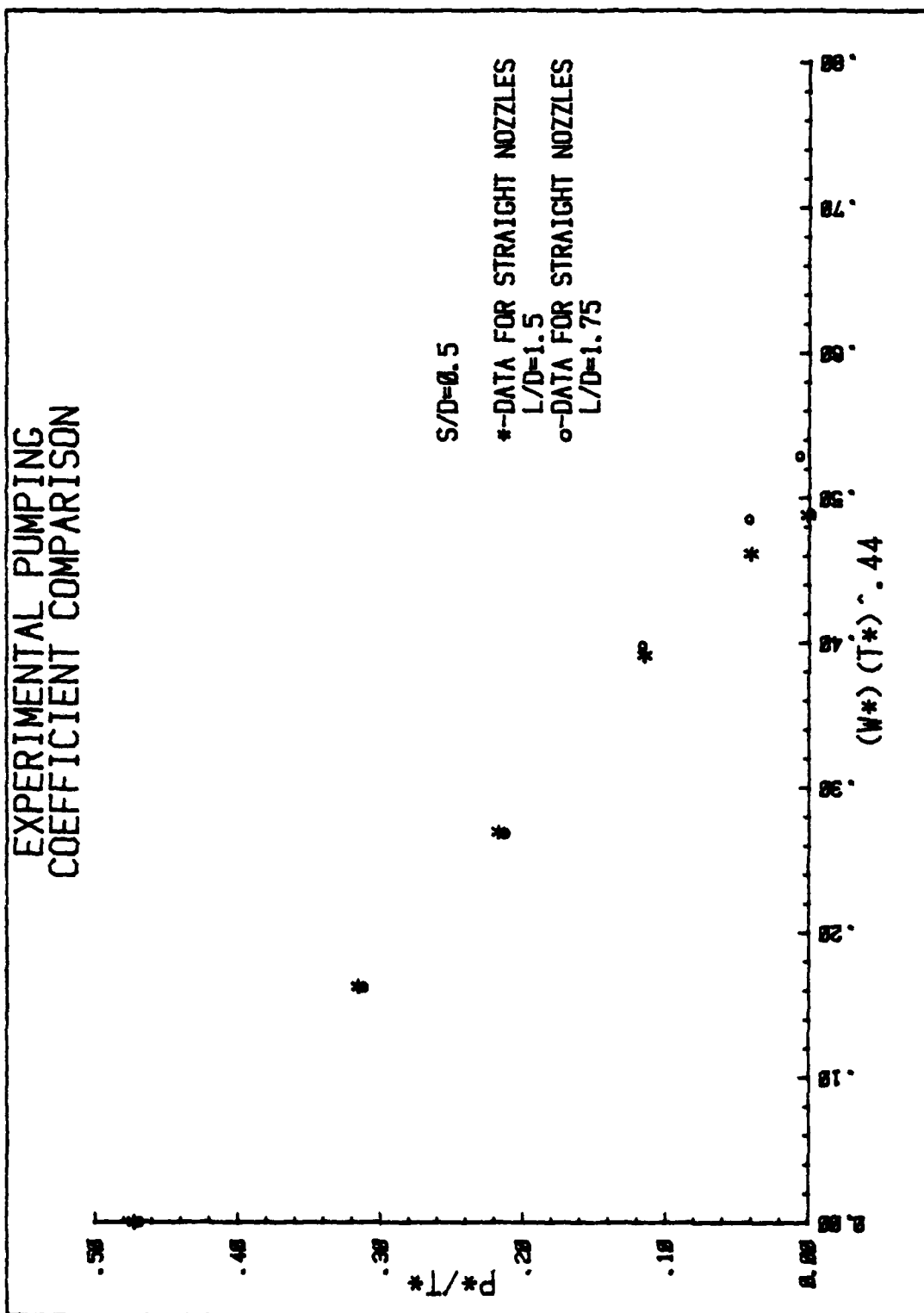


FIGURE 46

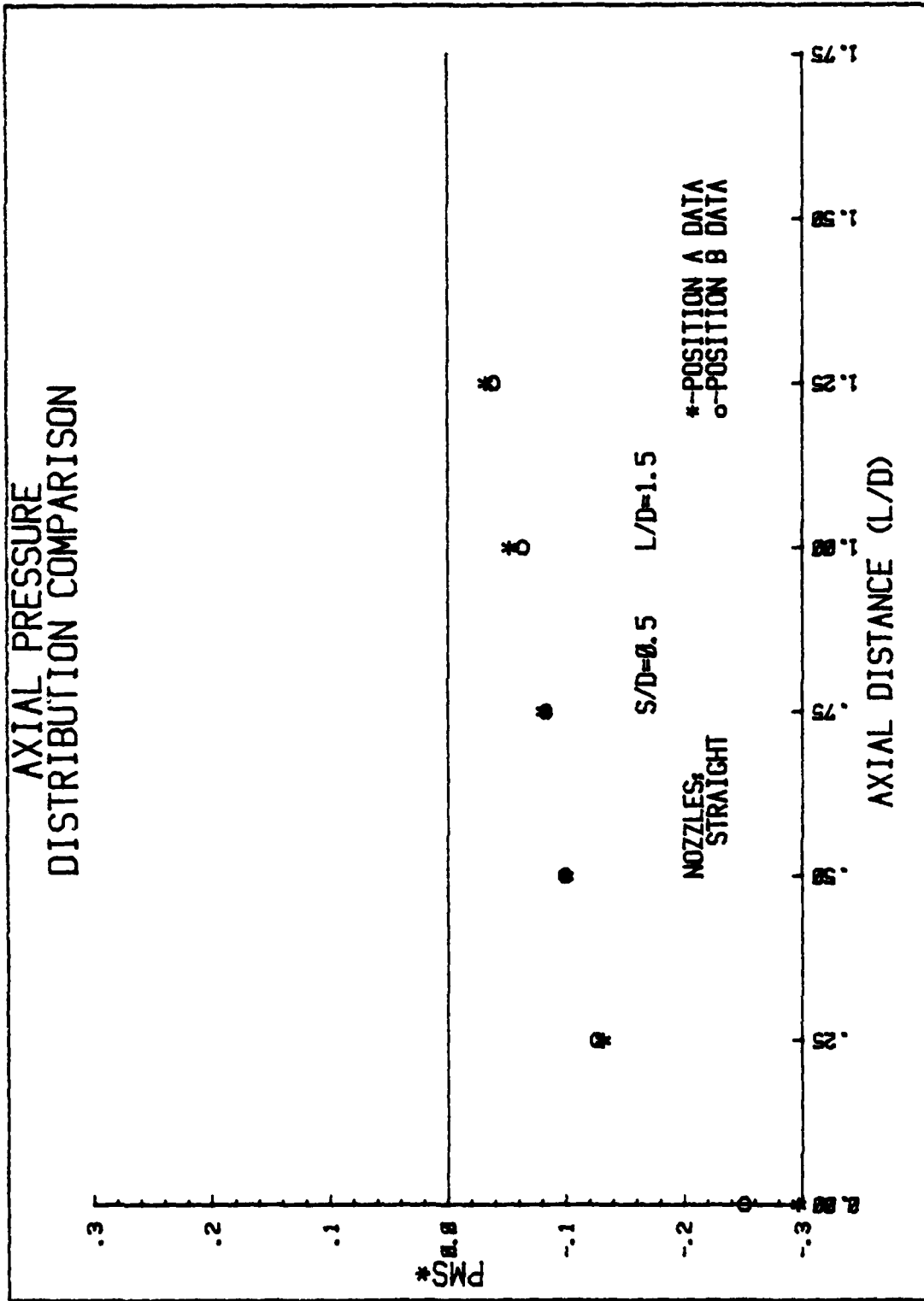


FIGURE 46.1

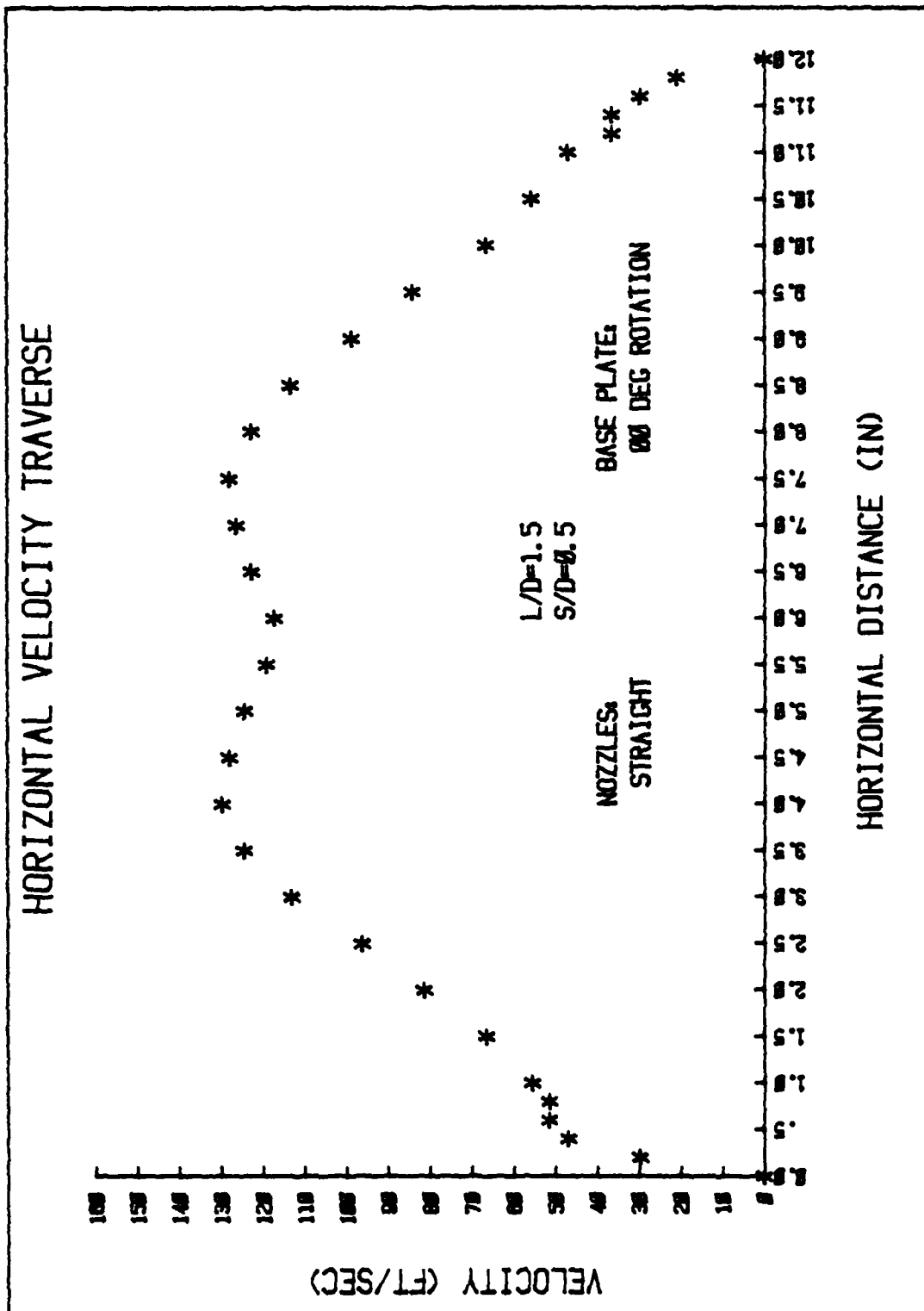


FIGURE 48.2

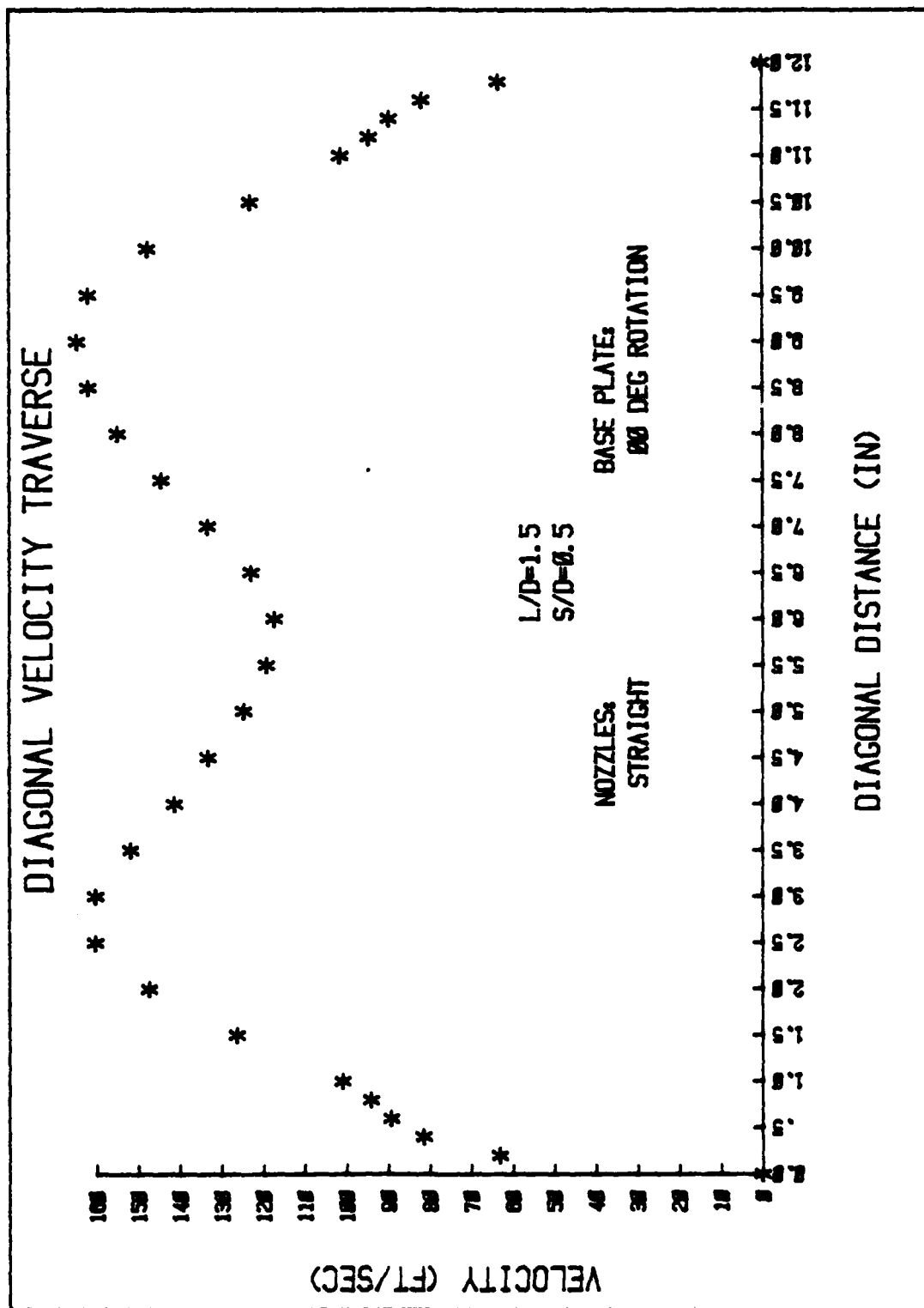


FIGURE 4B.3

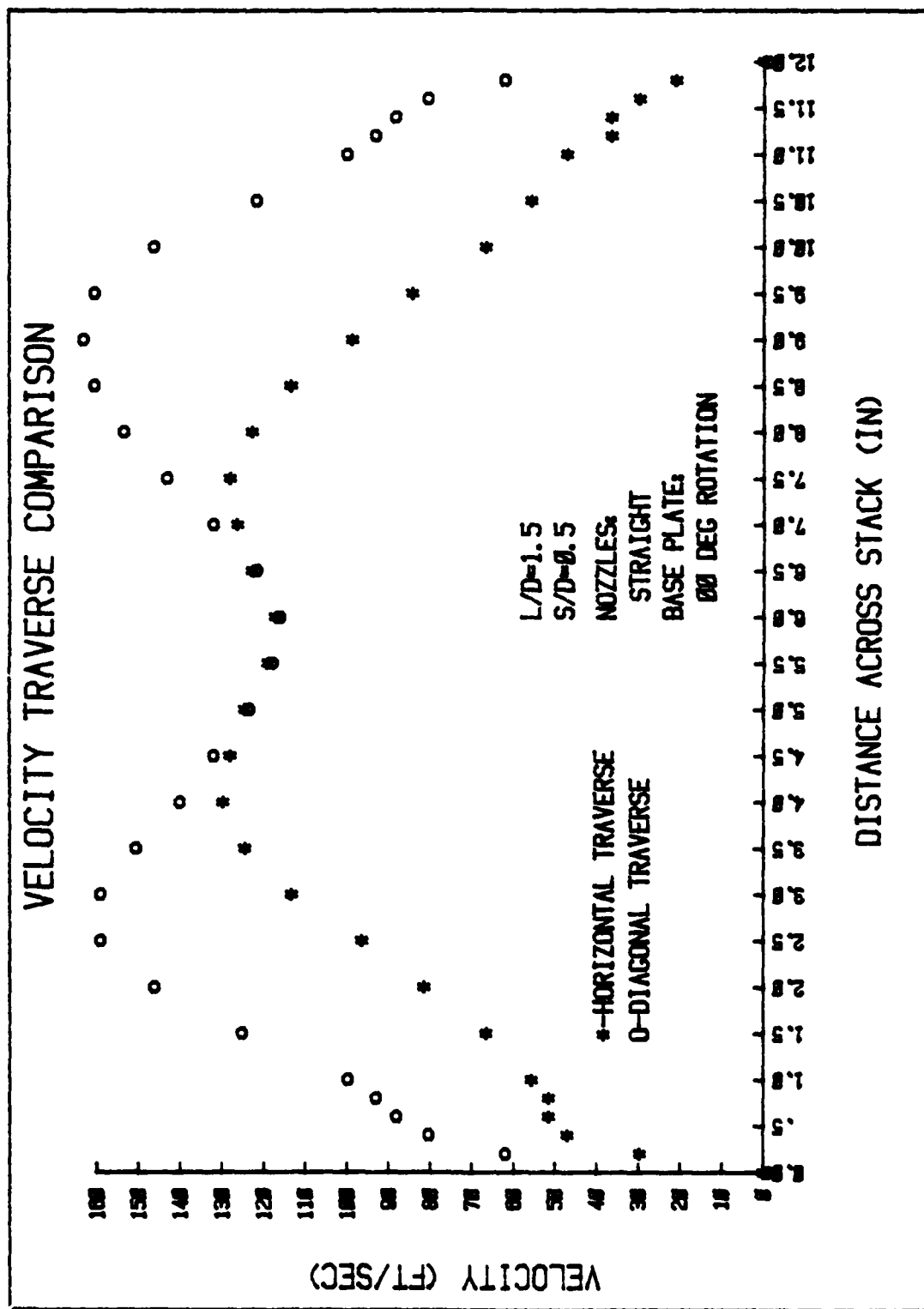
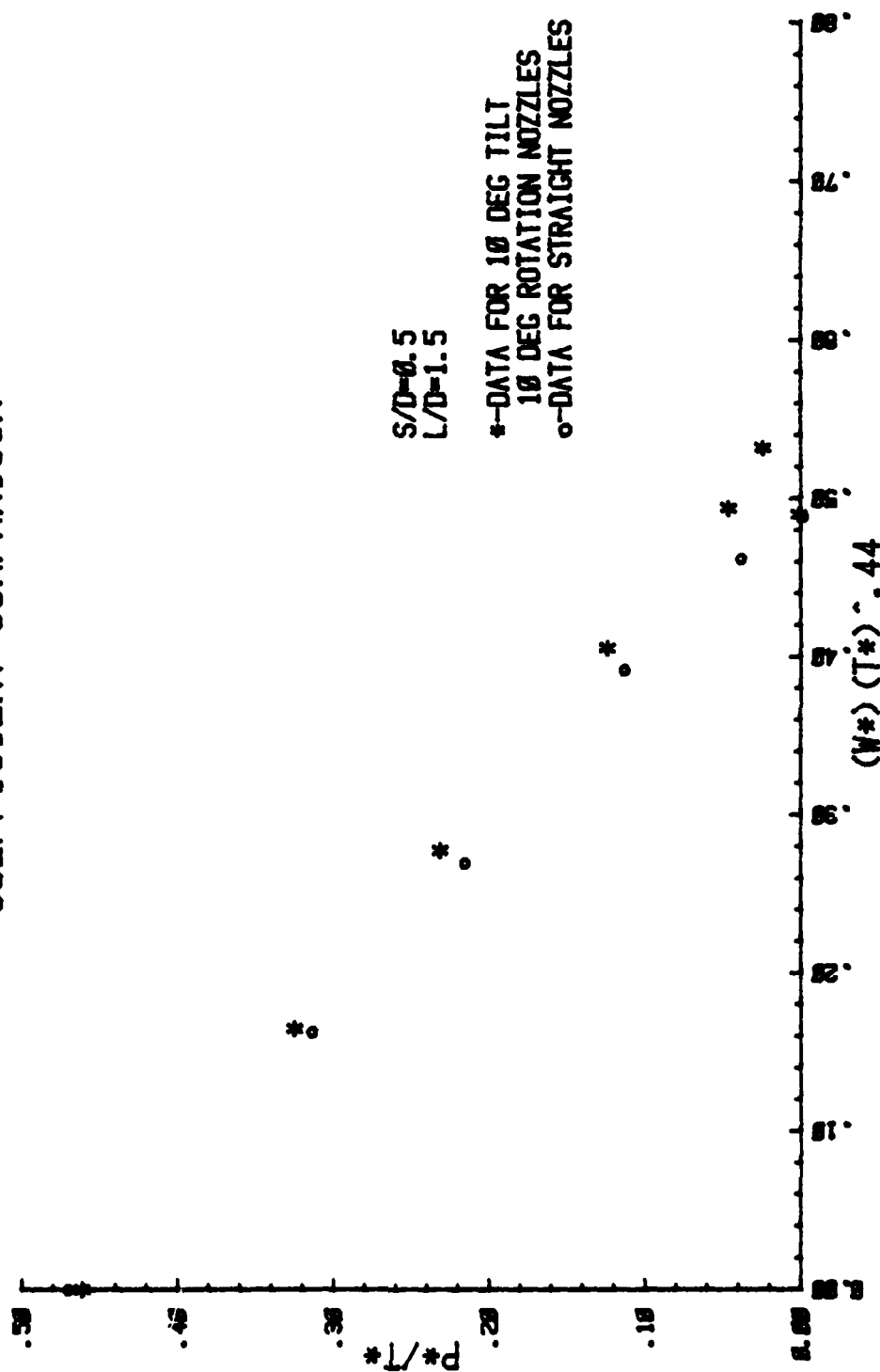


FIGURE 46.4



S/D=0.5  
L/D=1.5  
\*-DATA FOR 10 DEG TILT  
10 DEG ROTATION NOZZLES  
o-DATA FOR STRAIGHT NOZZLES



**FIGURE 47**

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

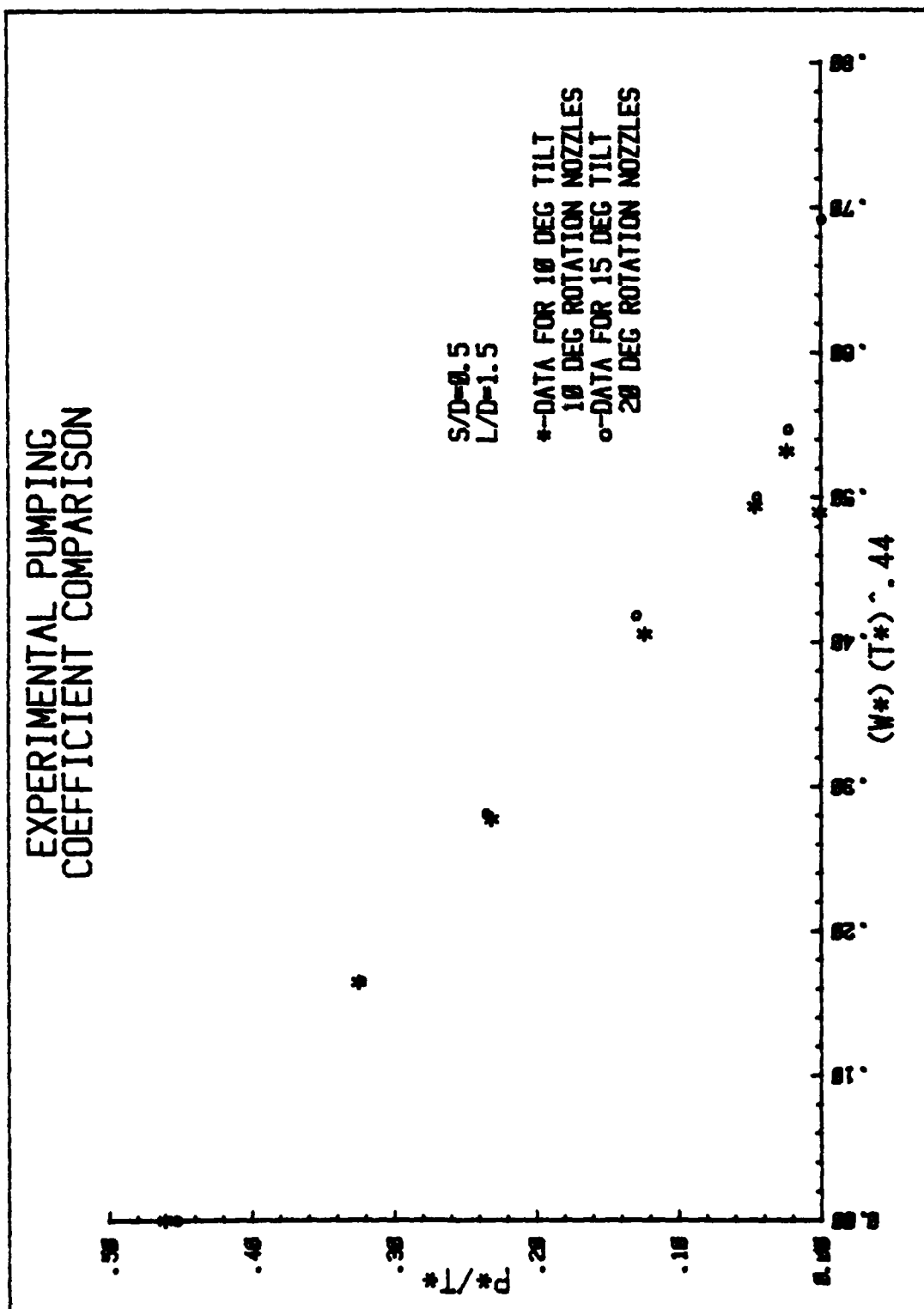


FIGURE 47.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

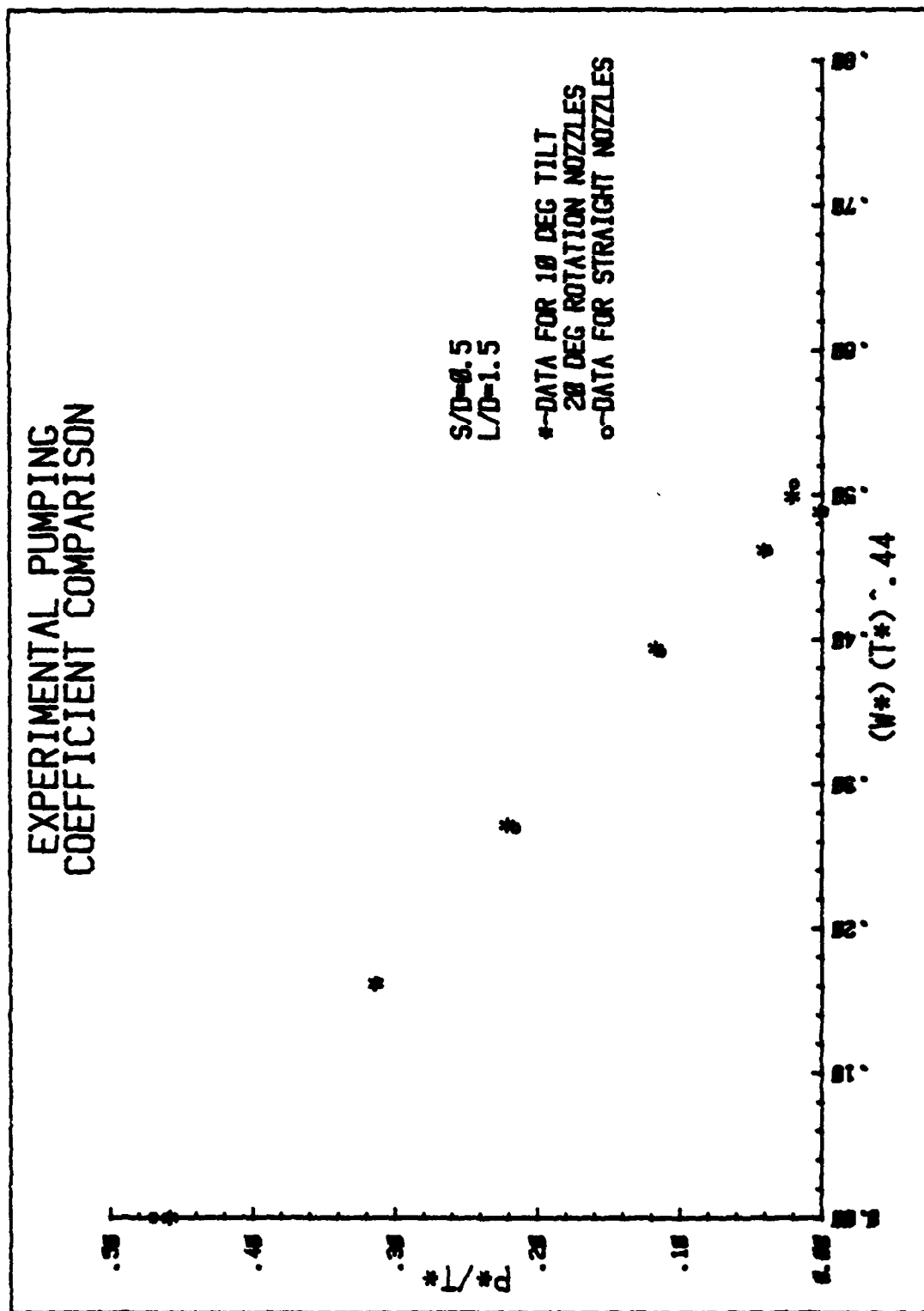


FIGURE 48

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

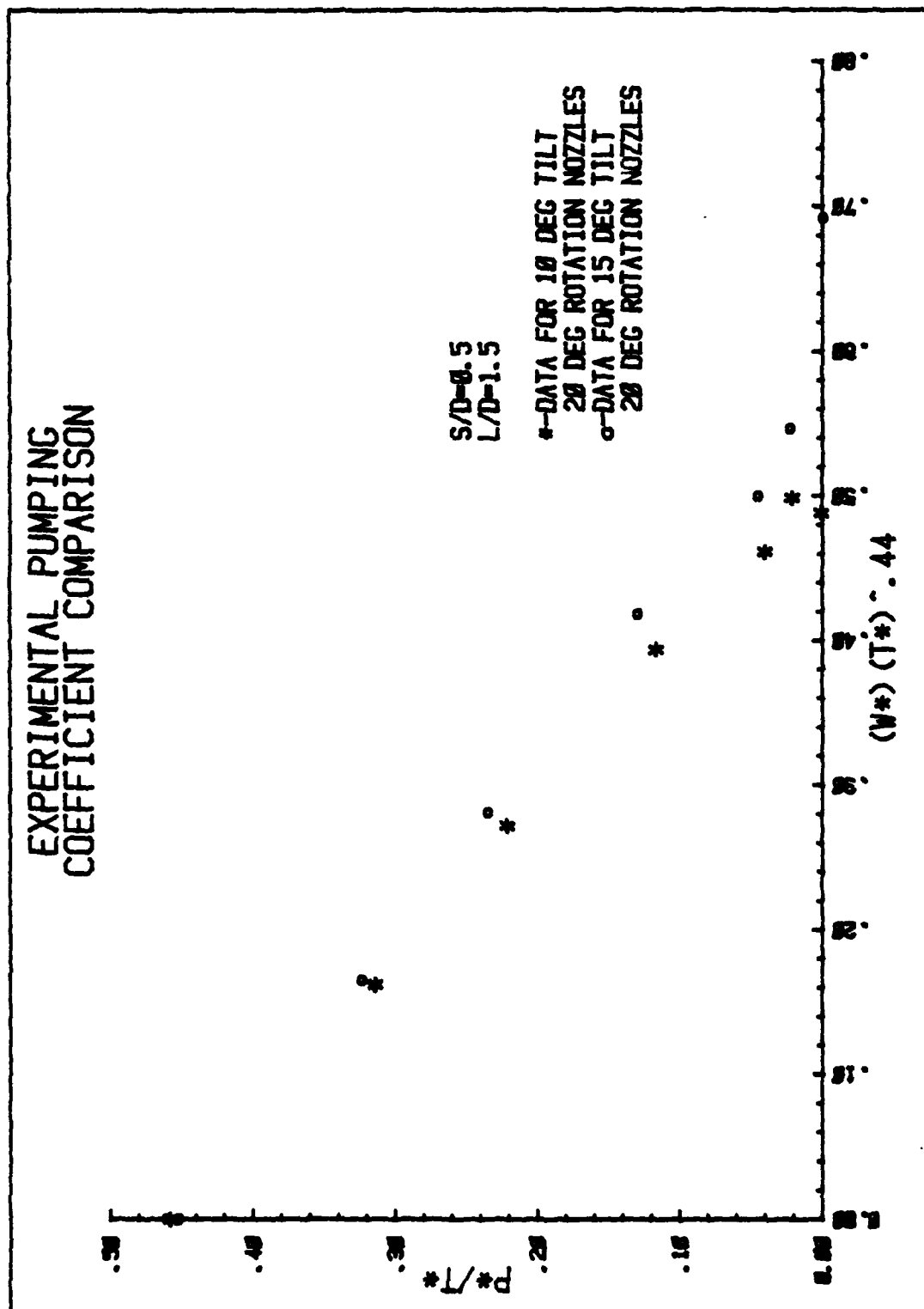


FIGURE 48.1

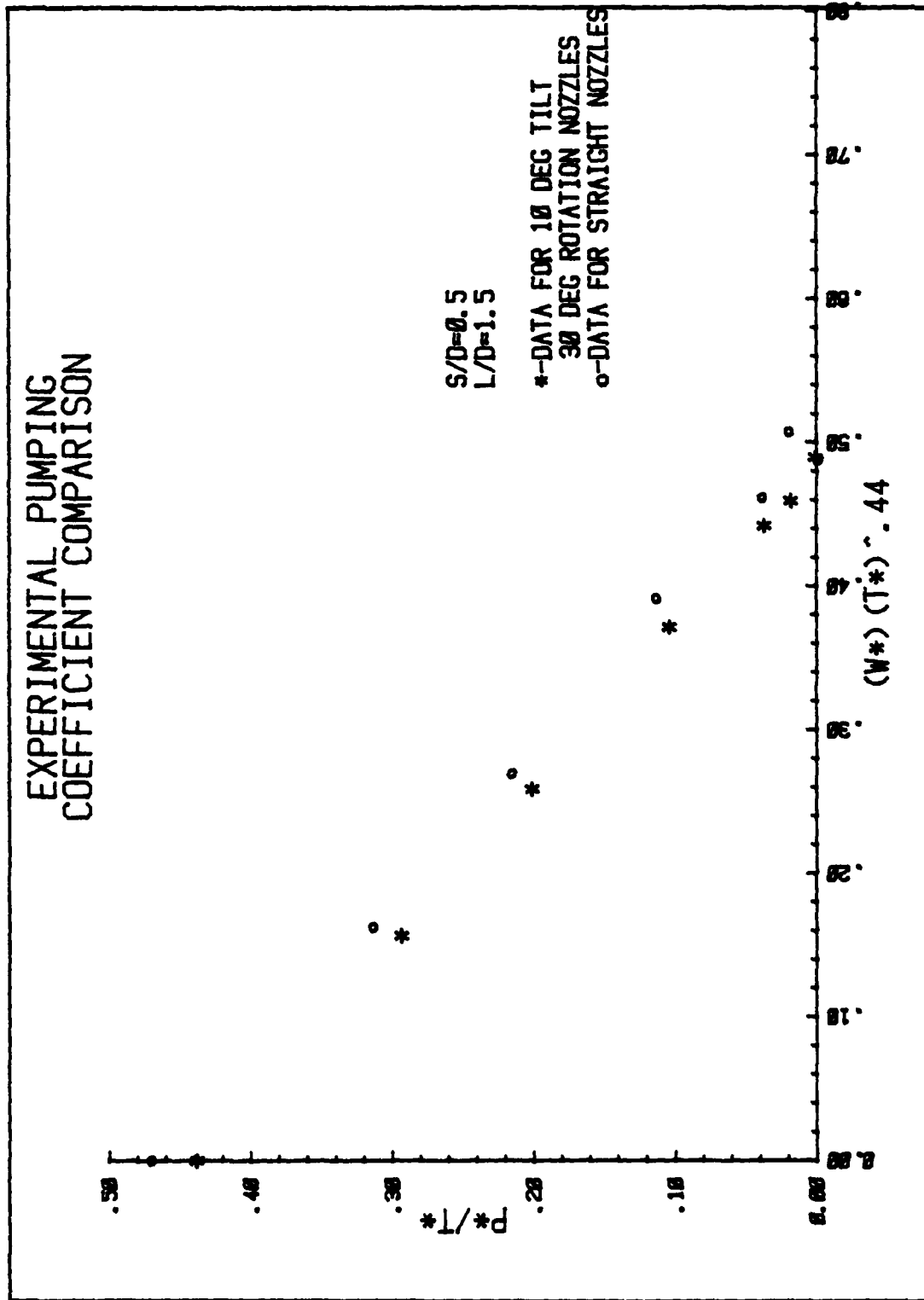


FIGURE 49

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

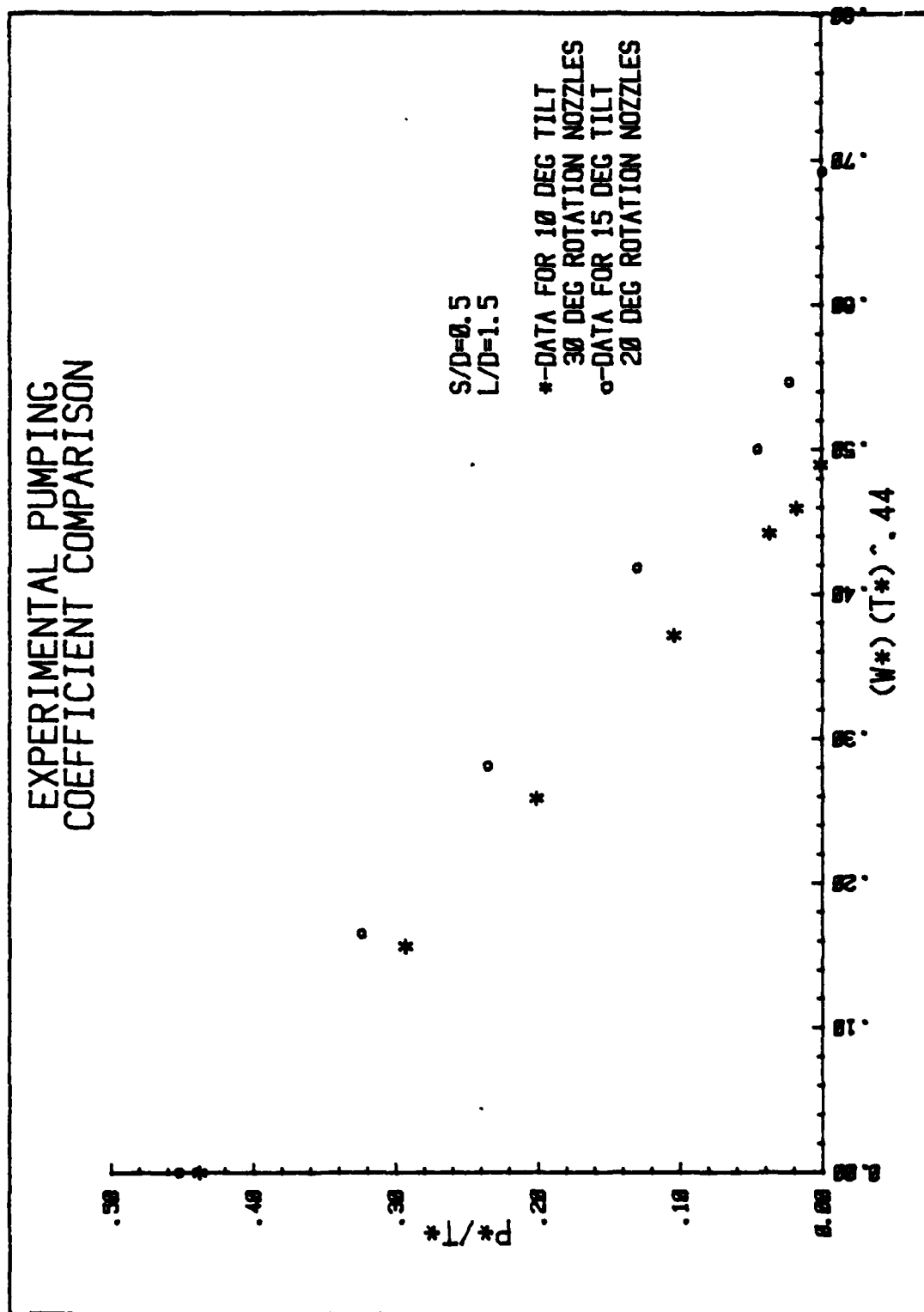


FIGURE 49.1

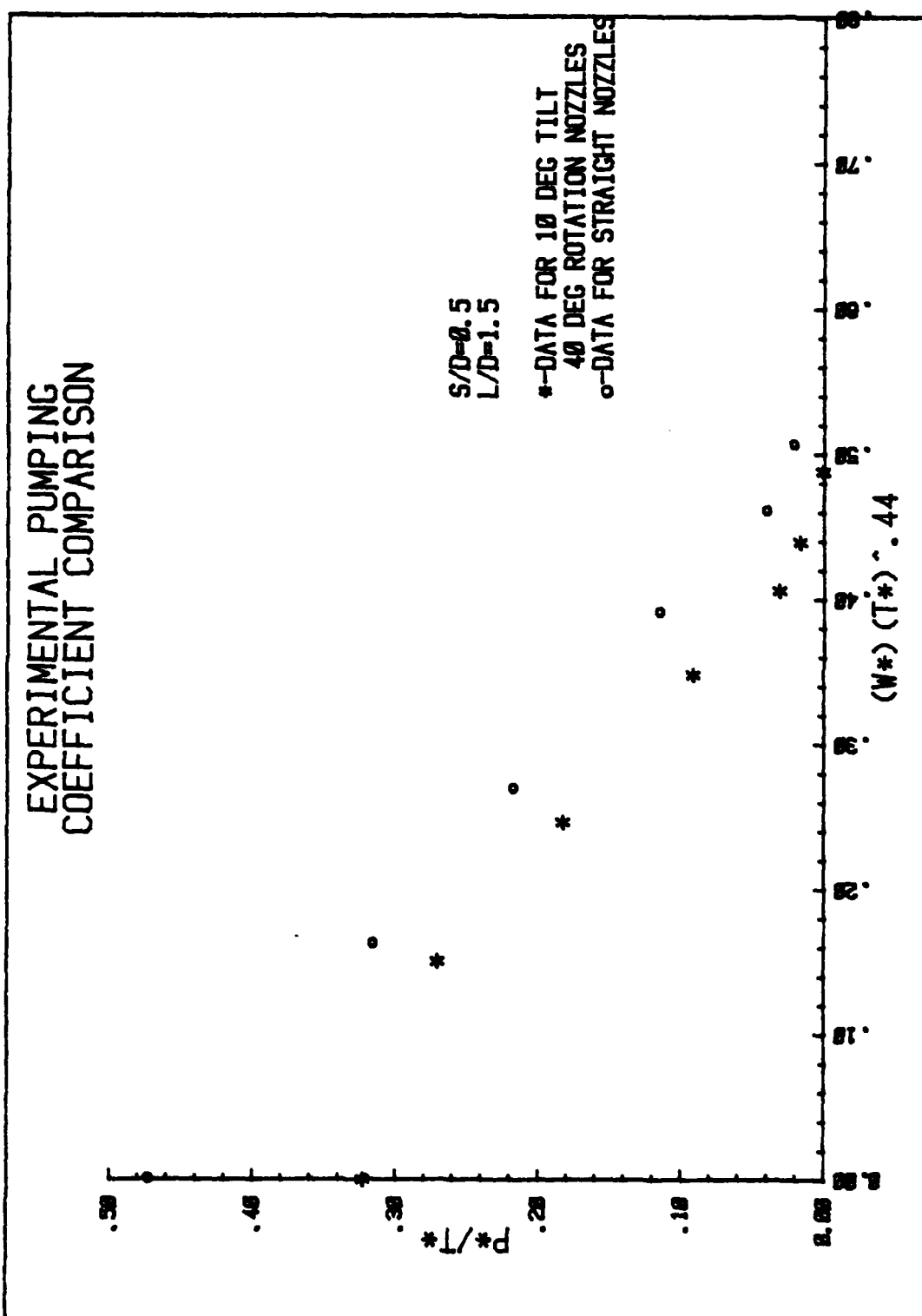


FIGURE 50

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

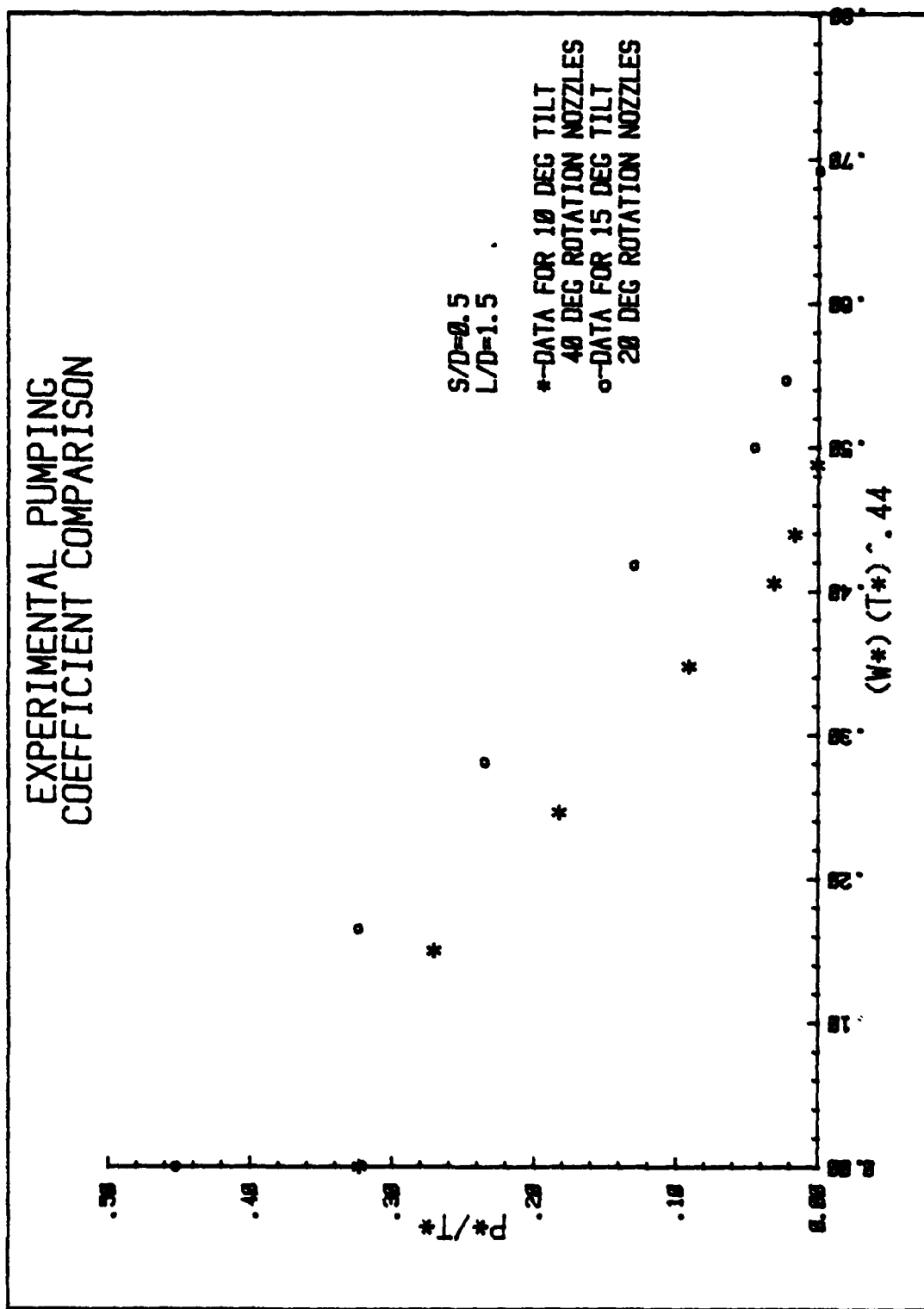


FIGURE 50.1



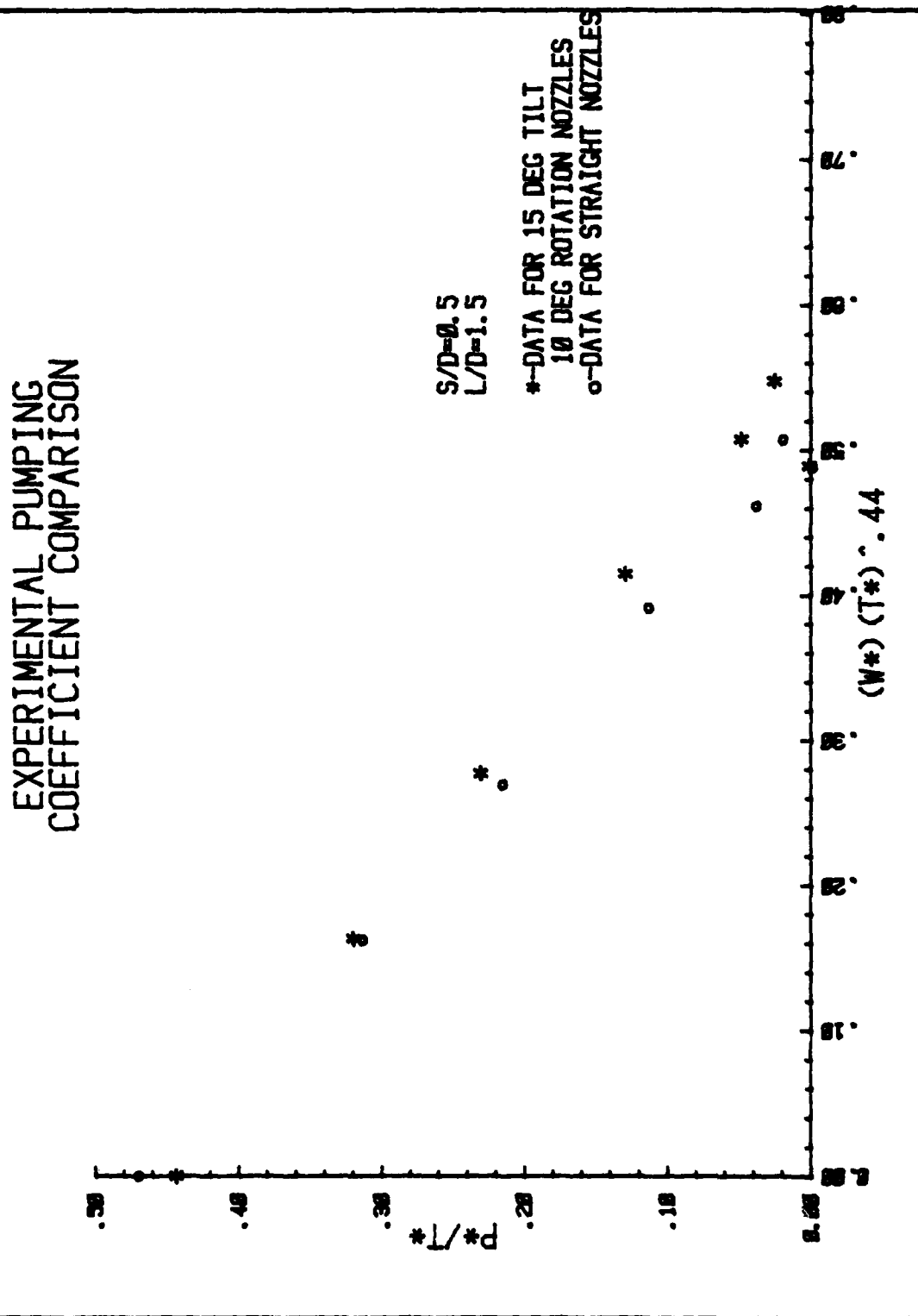


FIGURE 51

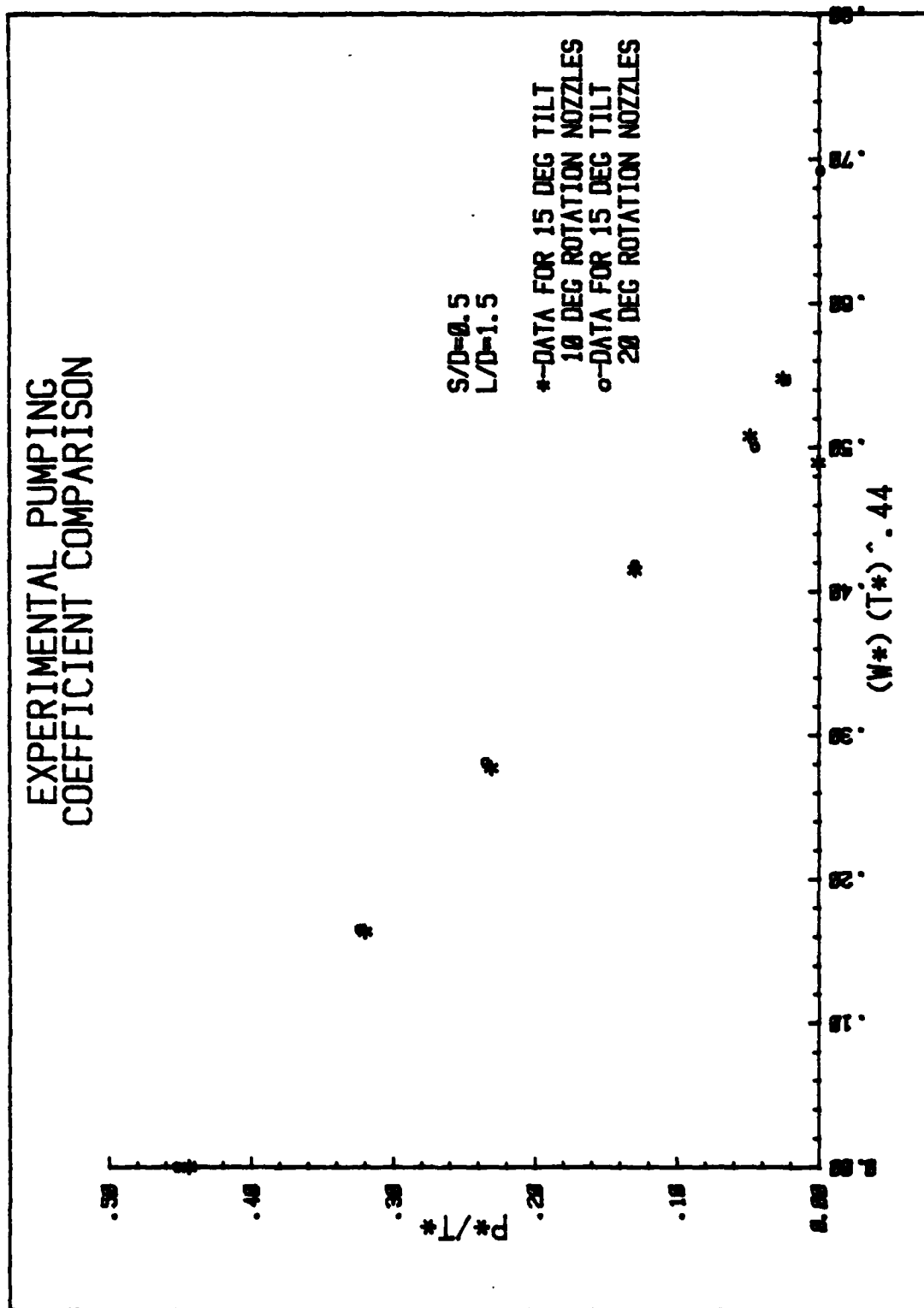


FIGURE 51.1

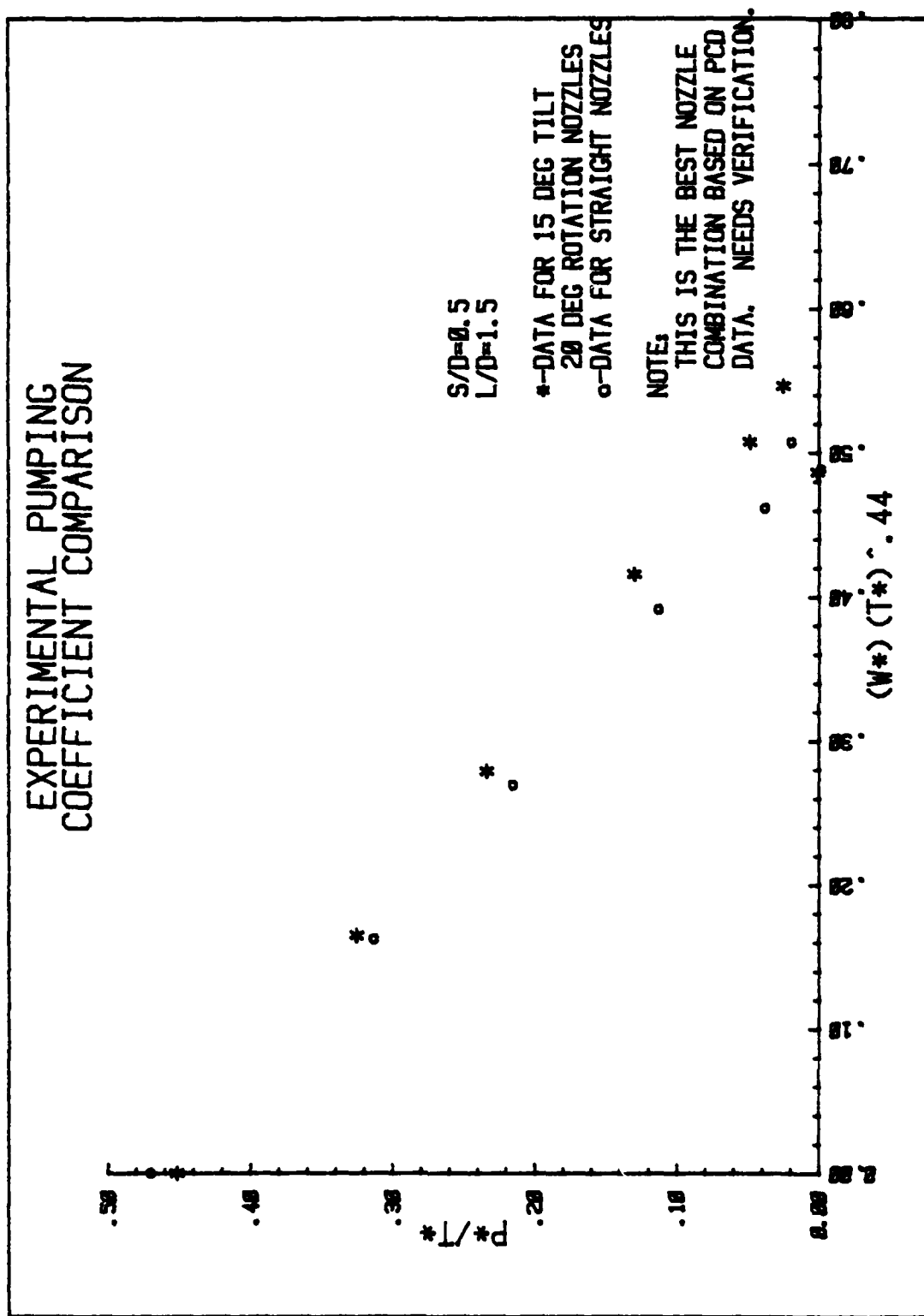
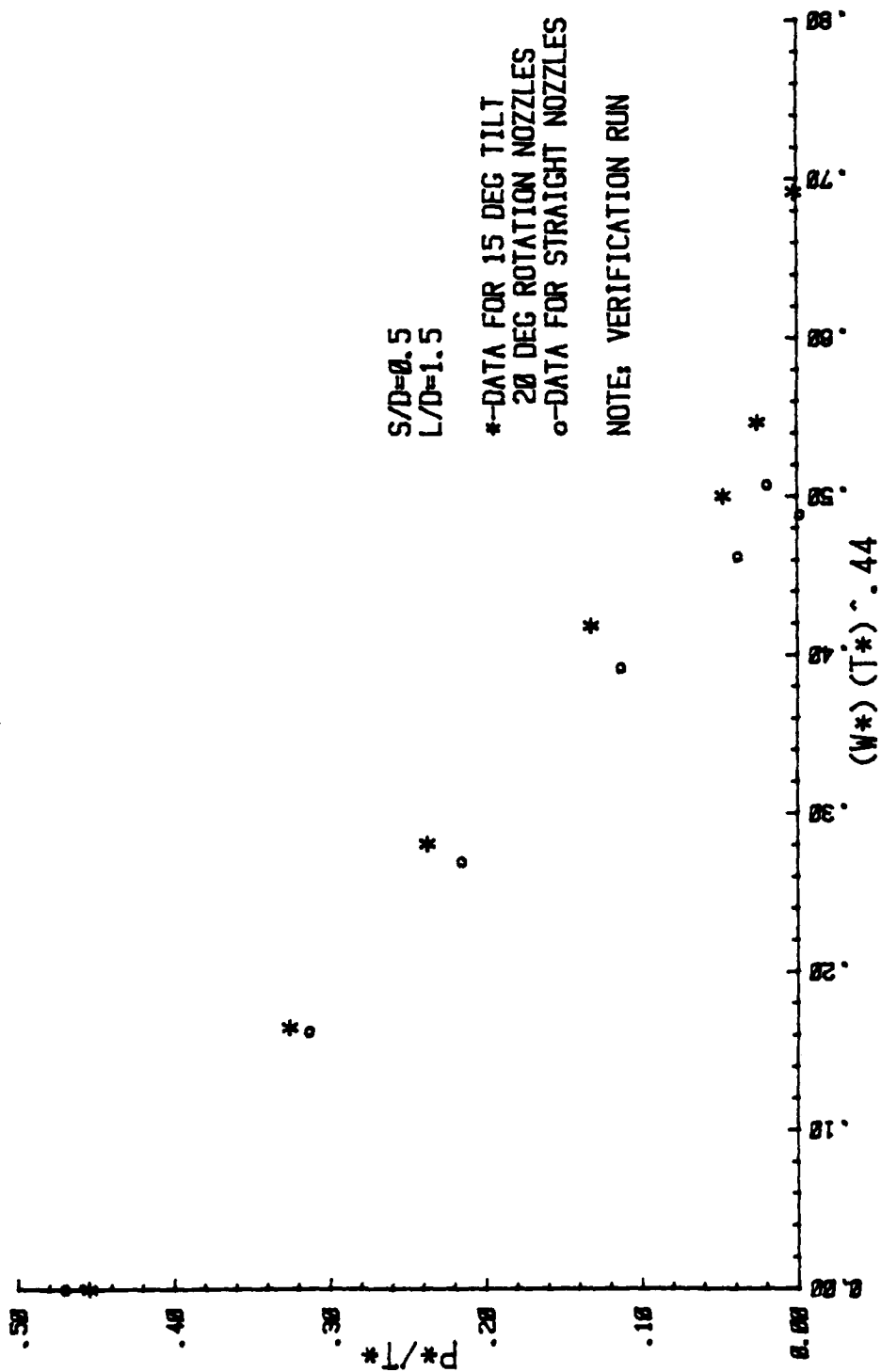


FIGURE 52

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON



S/D=0.5  
L/D=1.5

\*-DATA FOR 15 DEG TILT  
20 DEG ROTATION NOZZLES  
o-DATA FOR STRAIGHT NOZZLES

NOTE: VERIFICATION RUN

FIGURE 53

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

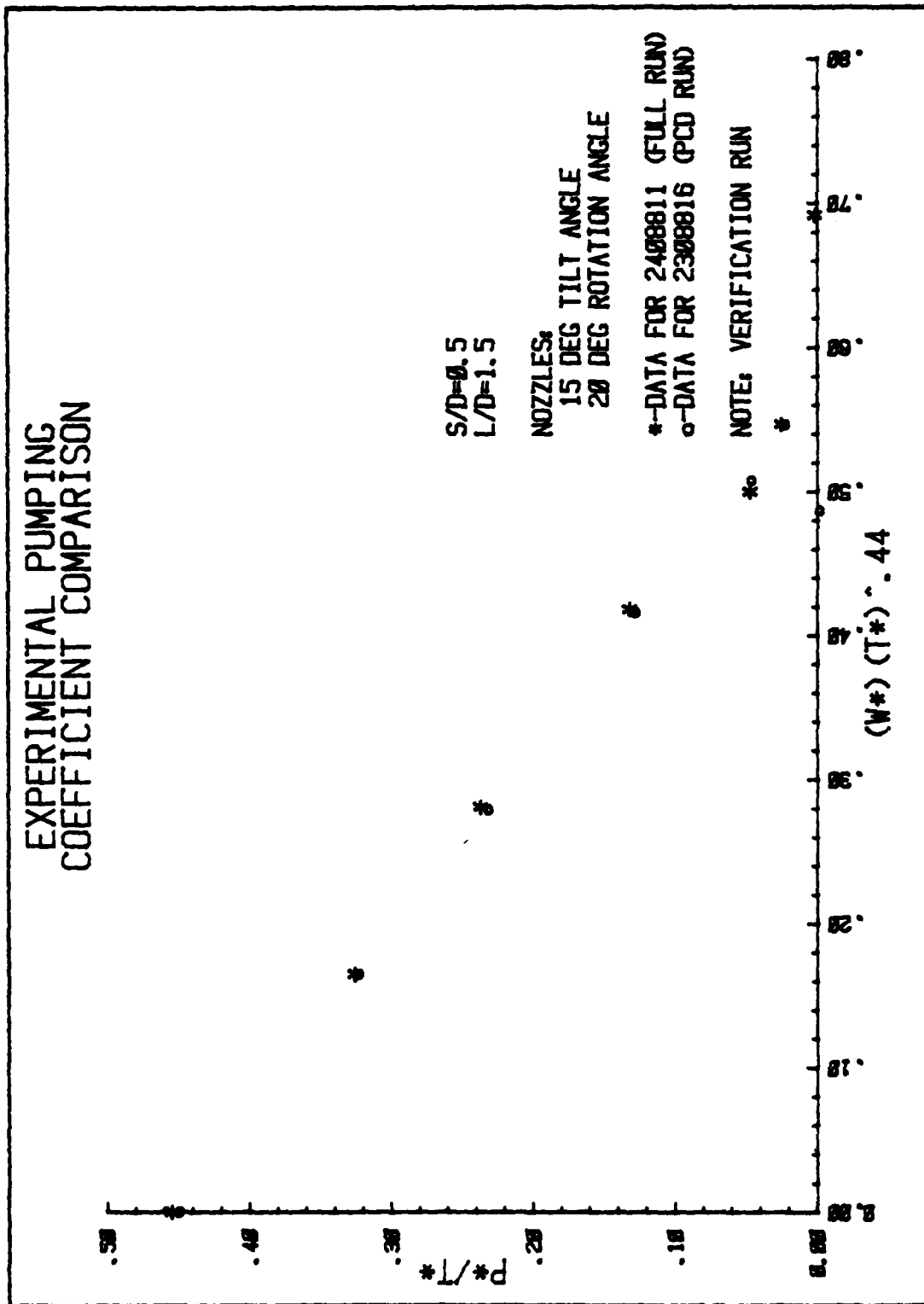


FIGURE 53.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

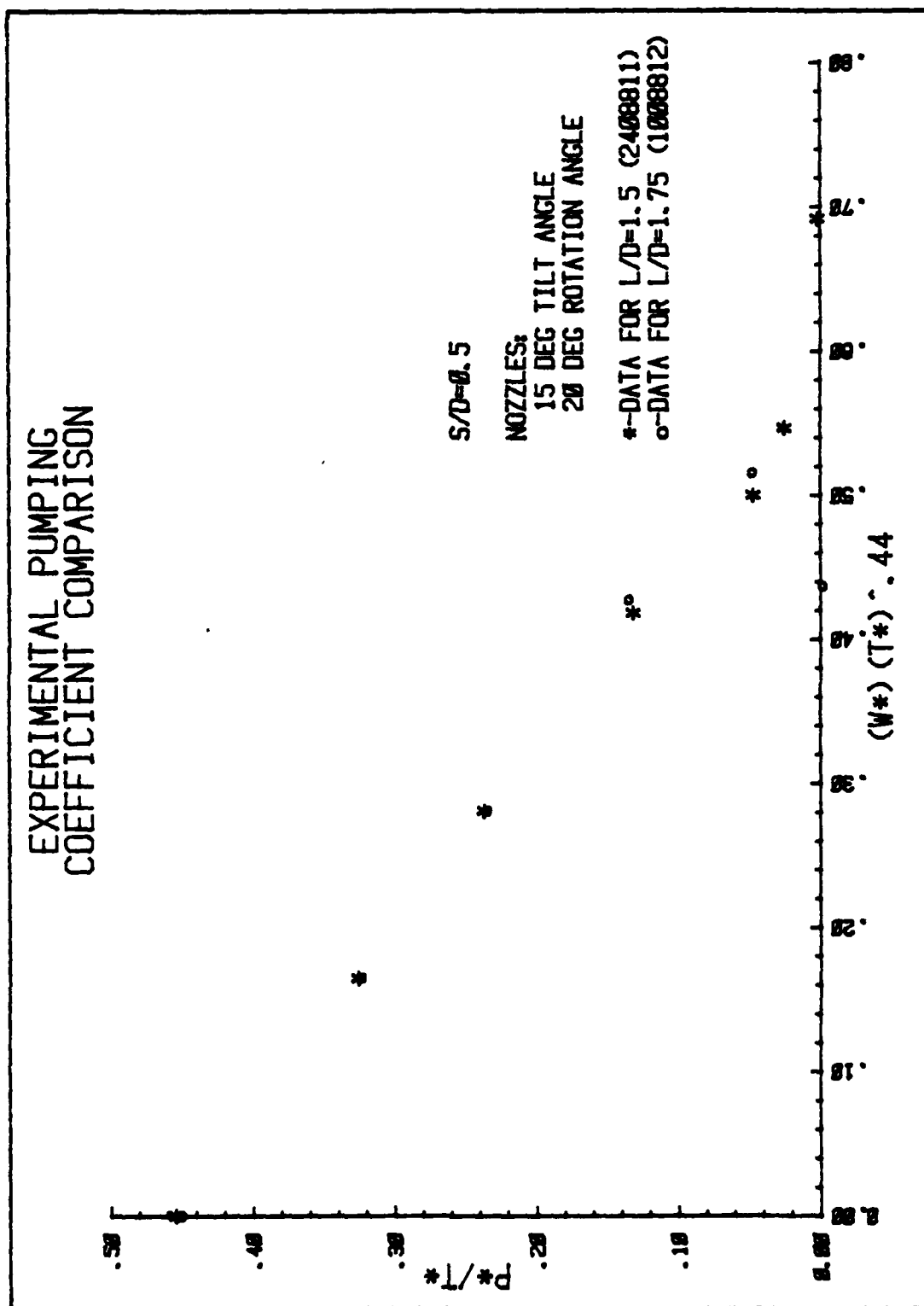


FIGURE 53.2

# AXIAL PRESSURE DISTRIBUTION COMPARISON

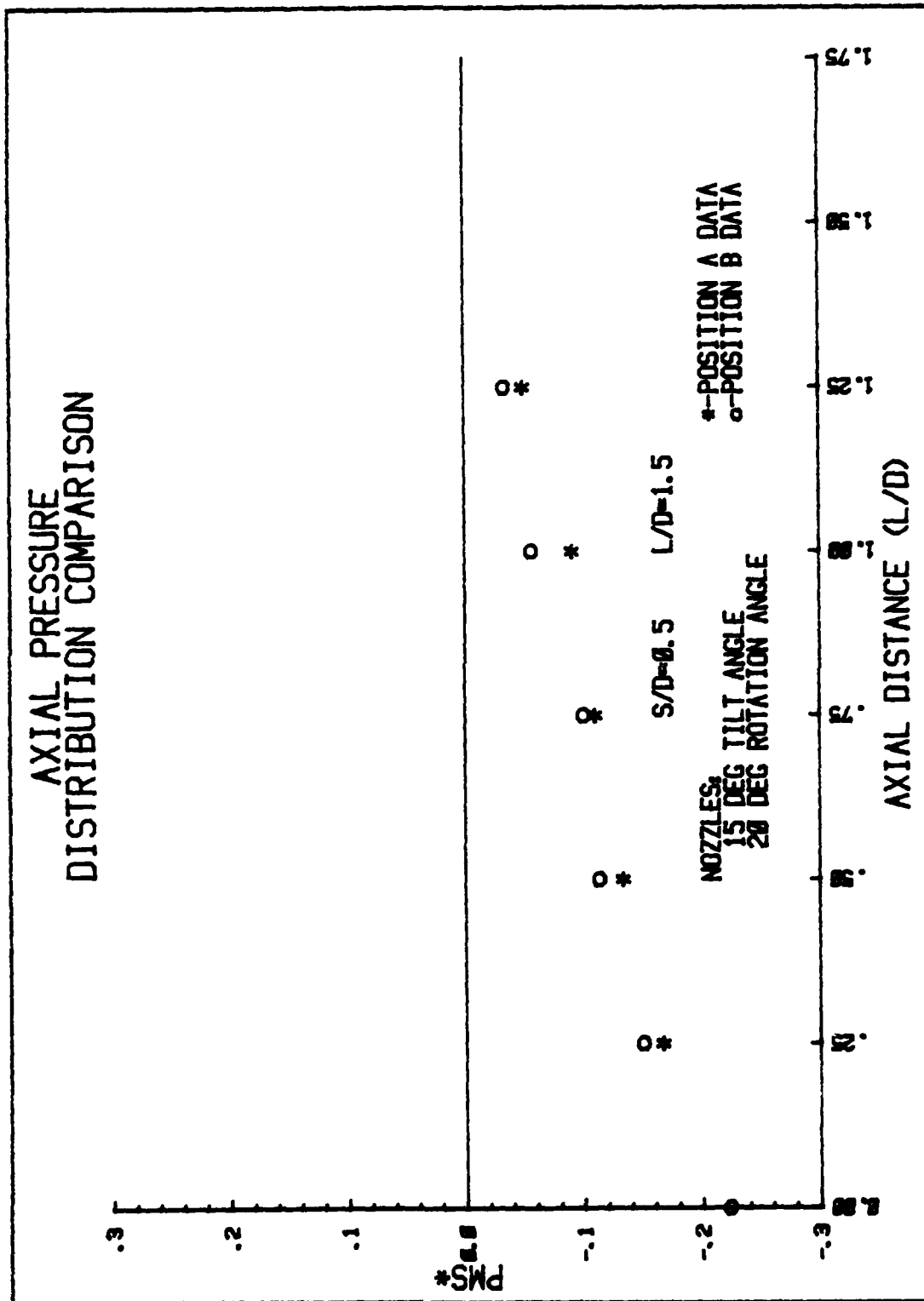


FIGURE 53.3

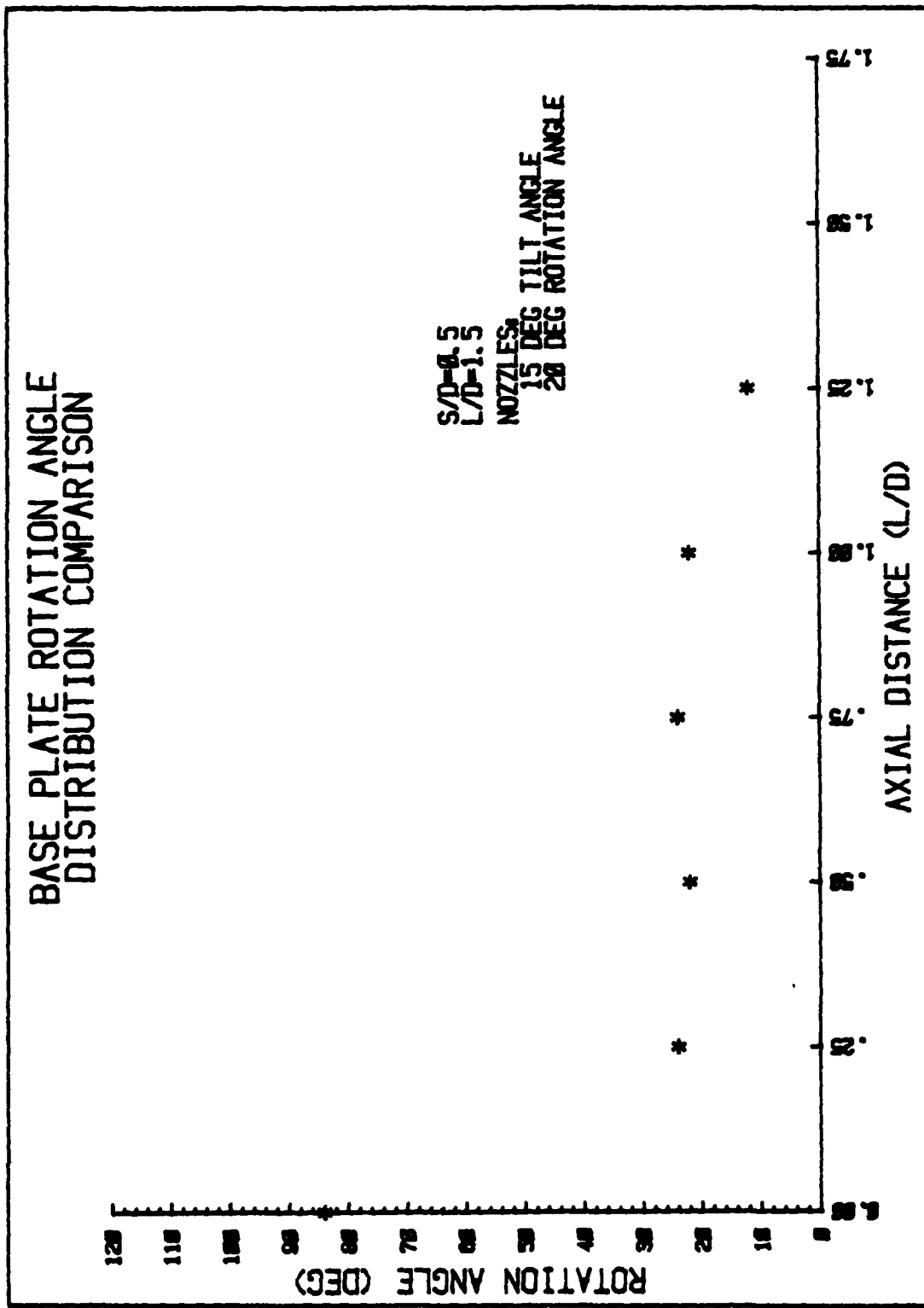


FIGURE 53.4



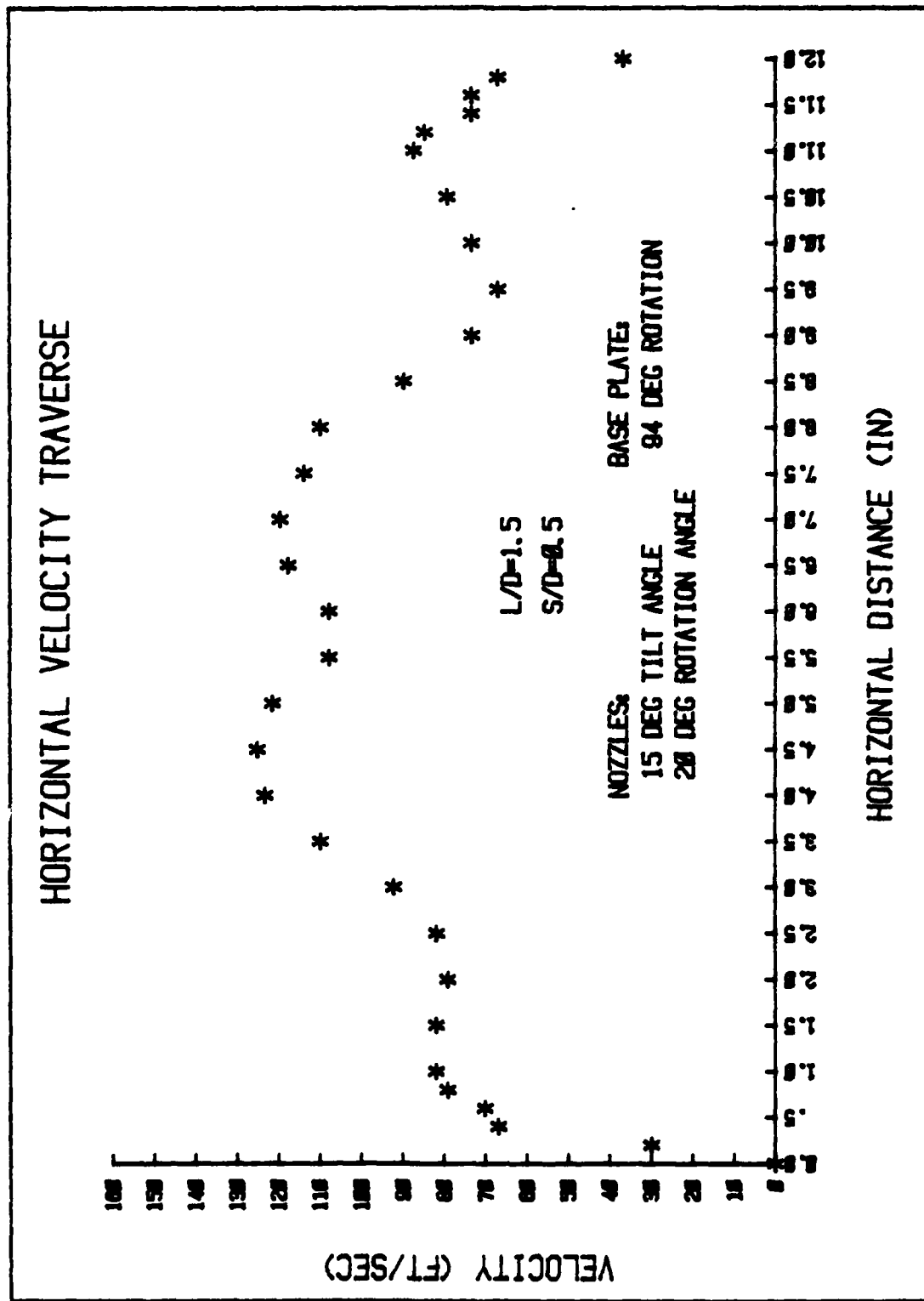


FIGURE 53.5

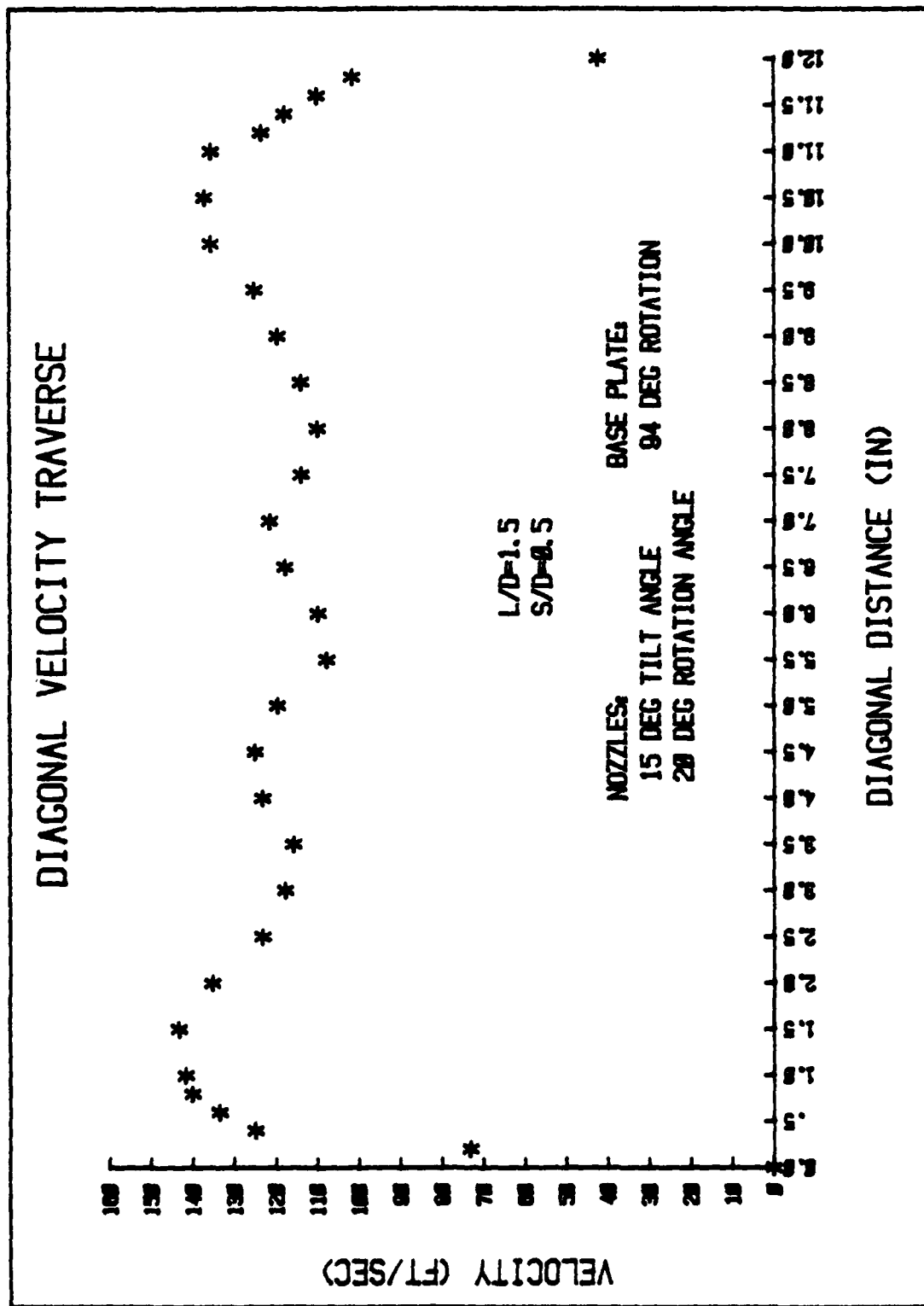


FIGURE 53.8

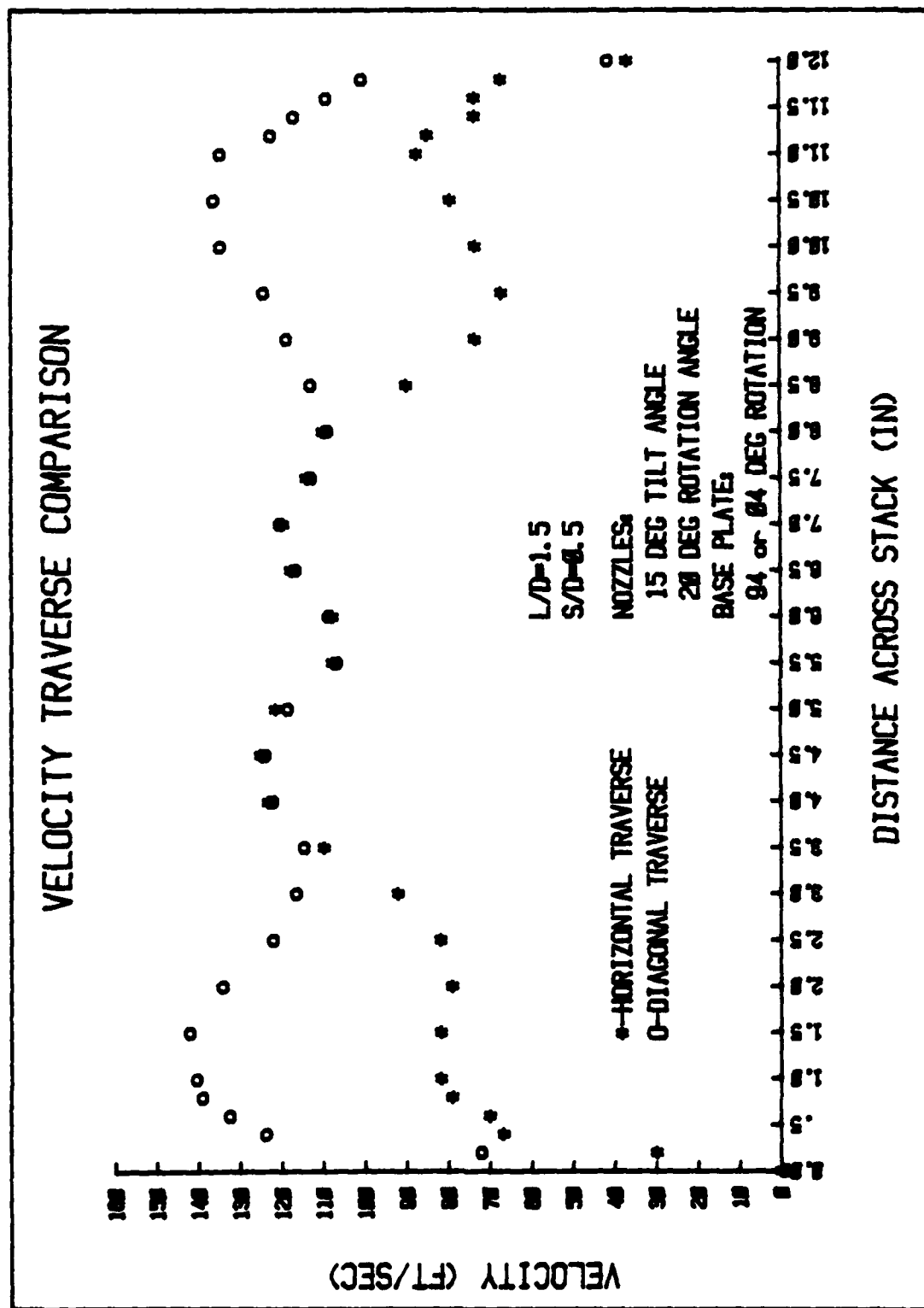


FIGURE 53.7

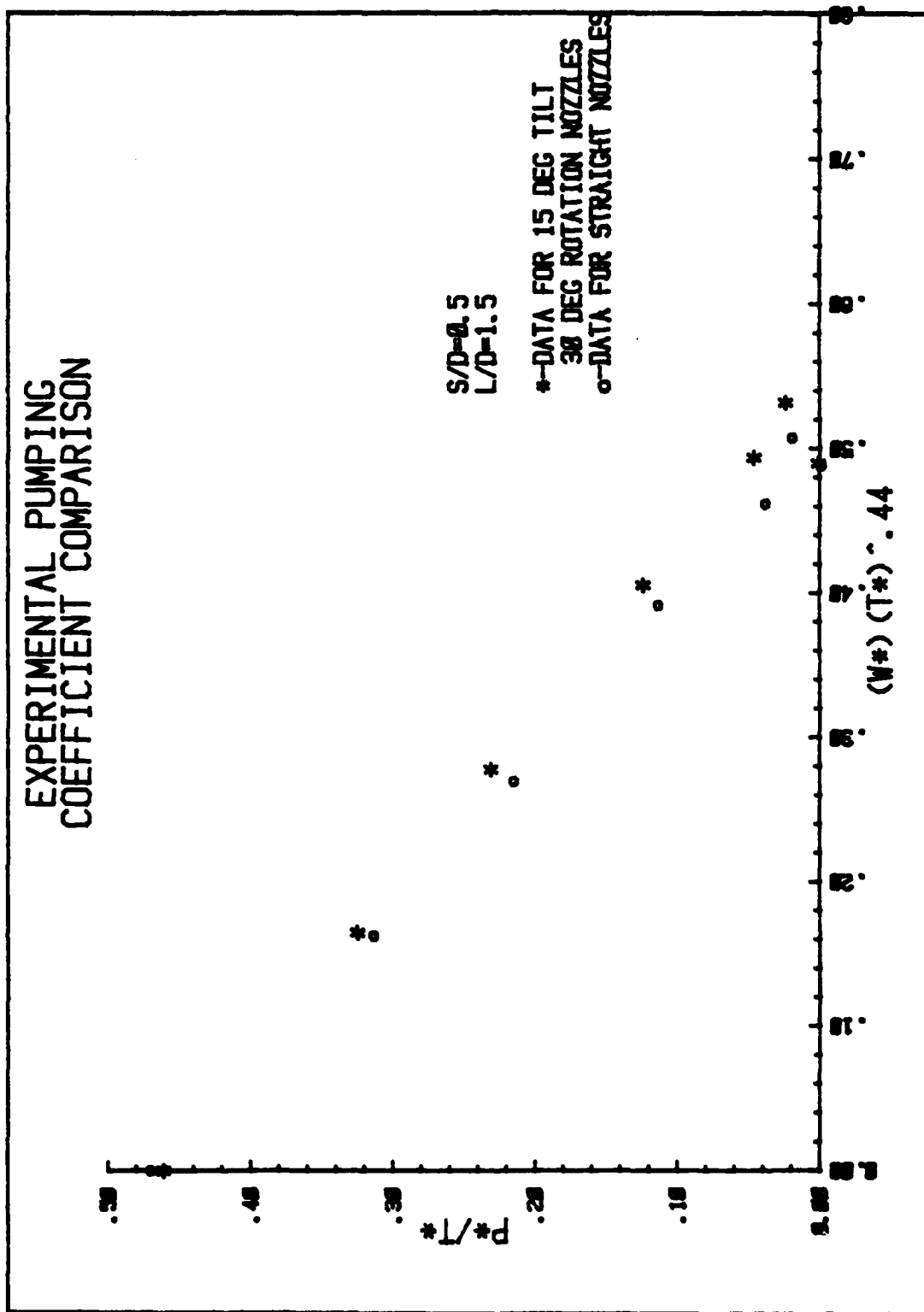


FIGURE 54

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

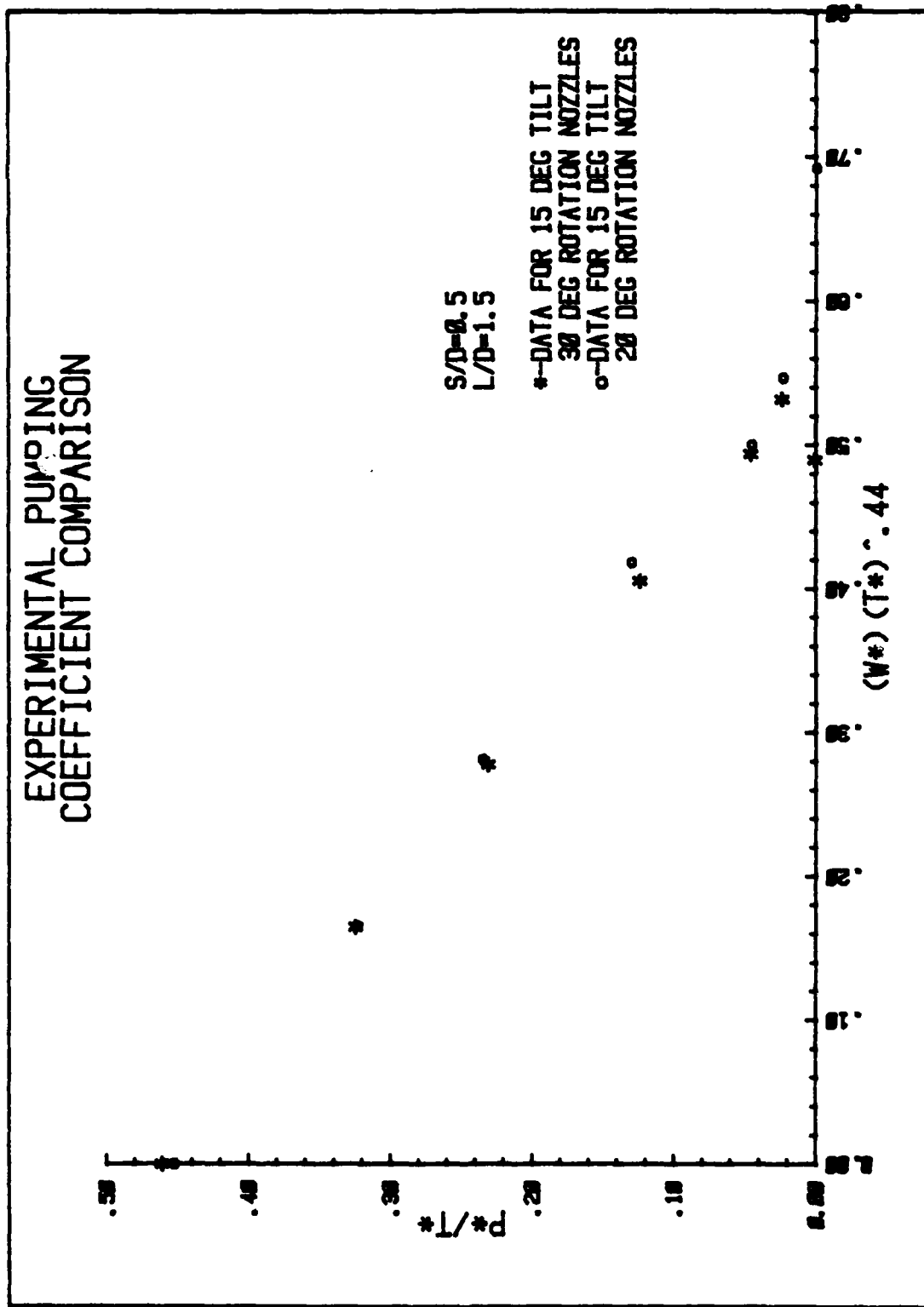


FIGURE 54.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

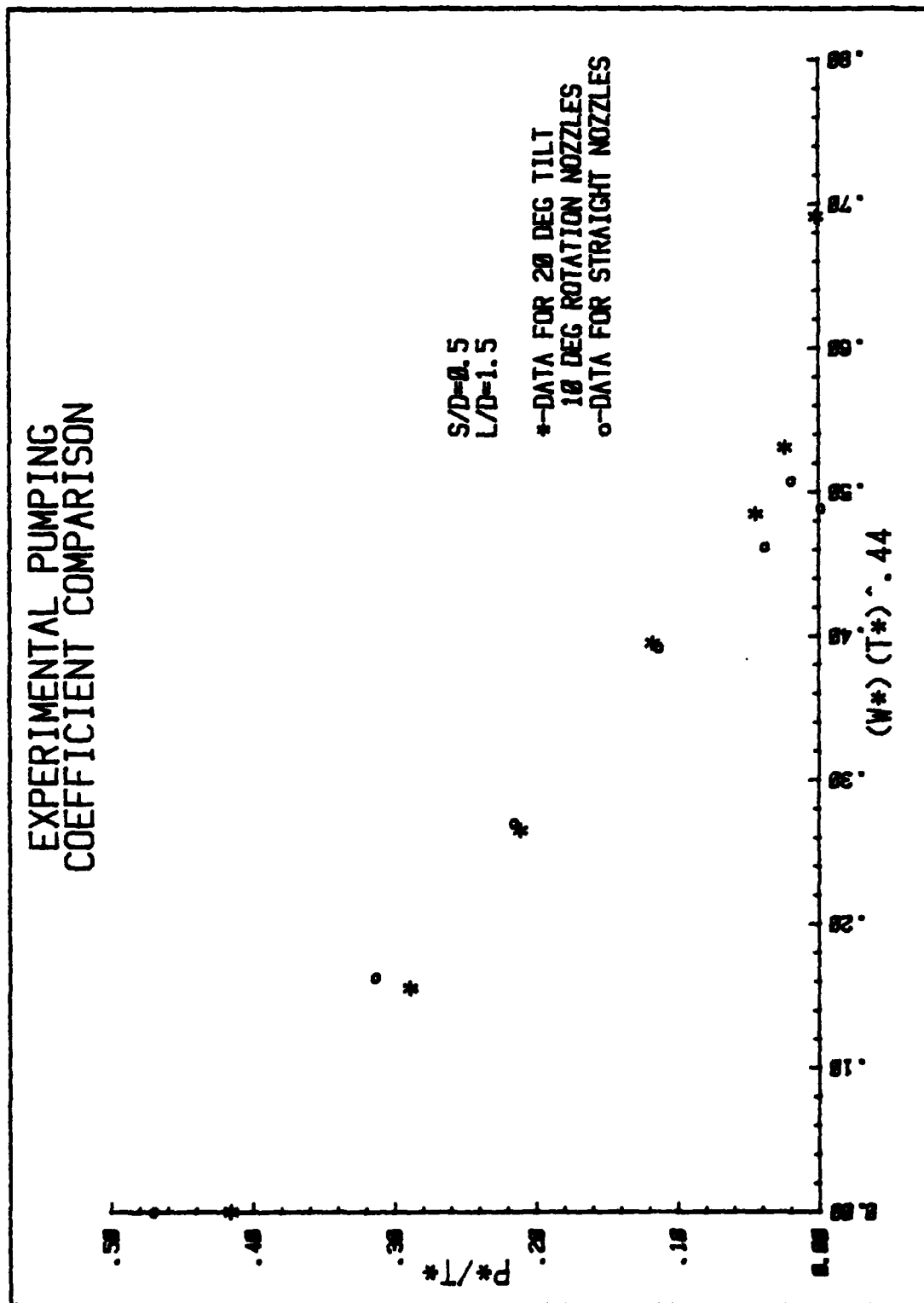


FIGURE 55

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

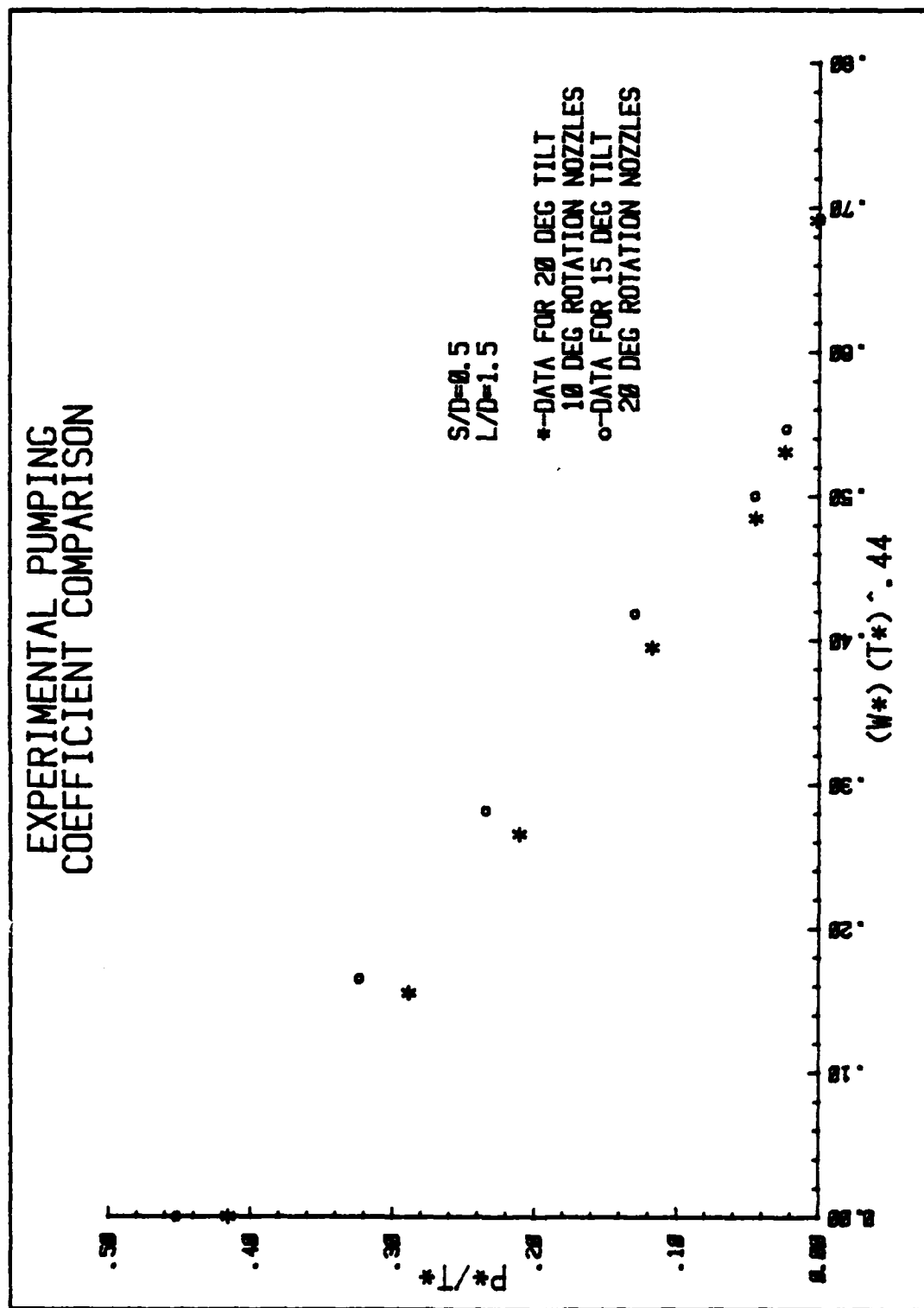
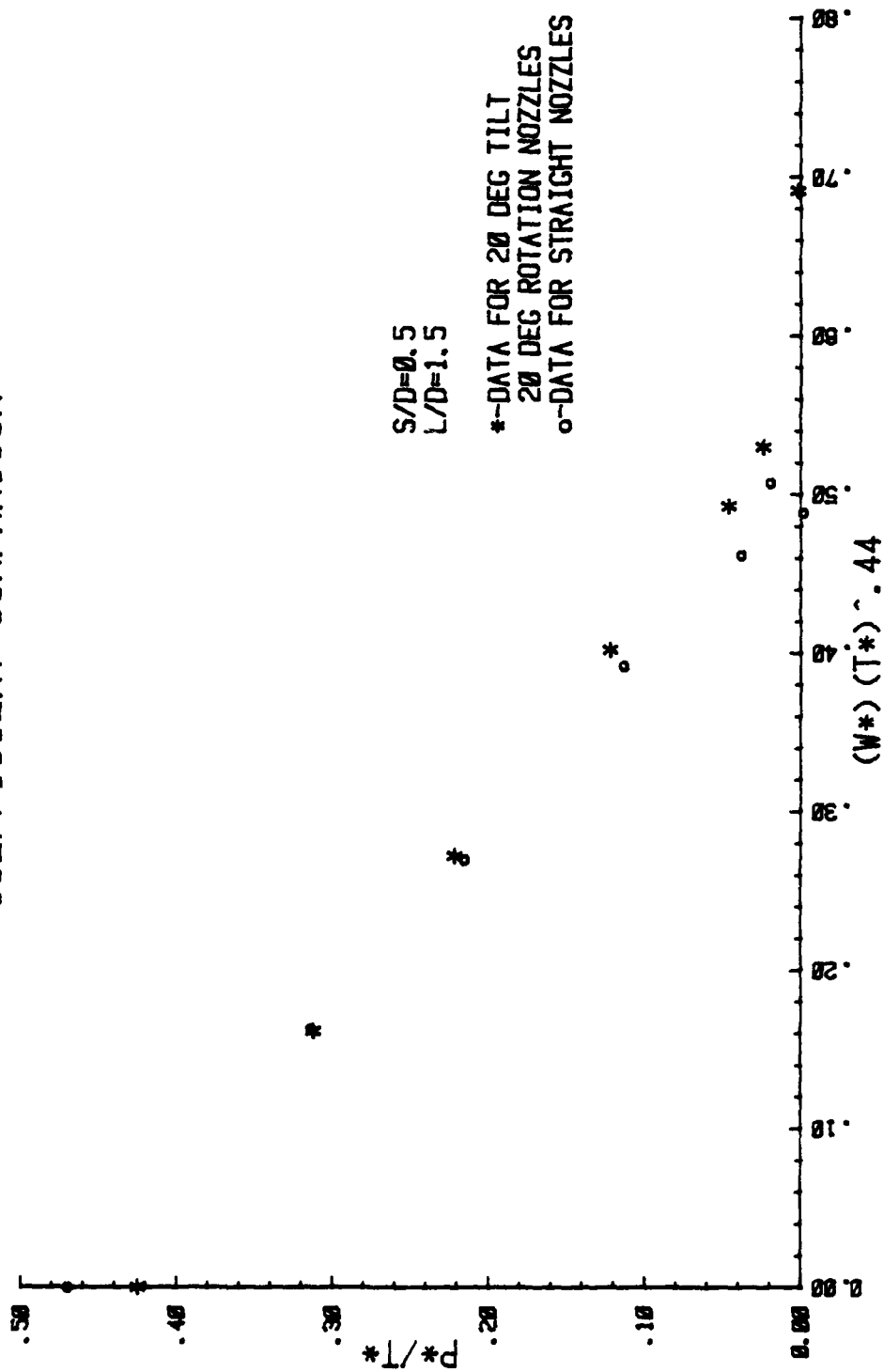


FIGURE 55.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

S/D=0.5  
L/D=1.5

\*-DATA FOR 20 DEG TILT  
20 DEG ROTATION NOZZLES  
o-DATA FOR STRAIGHT NOZZLES





# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

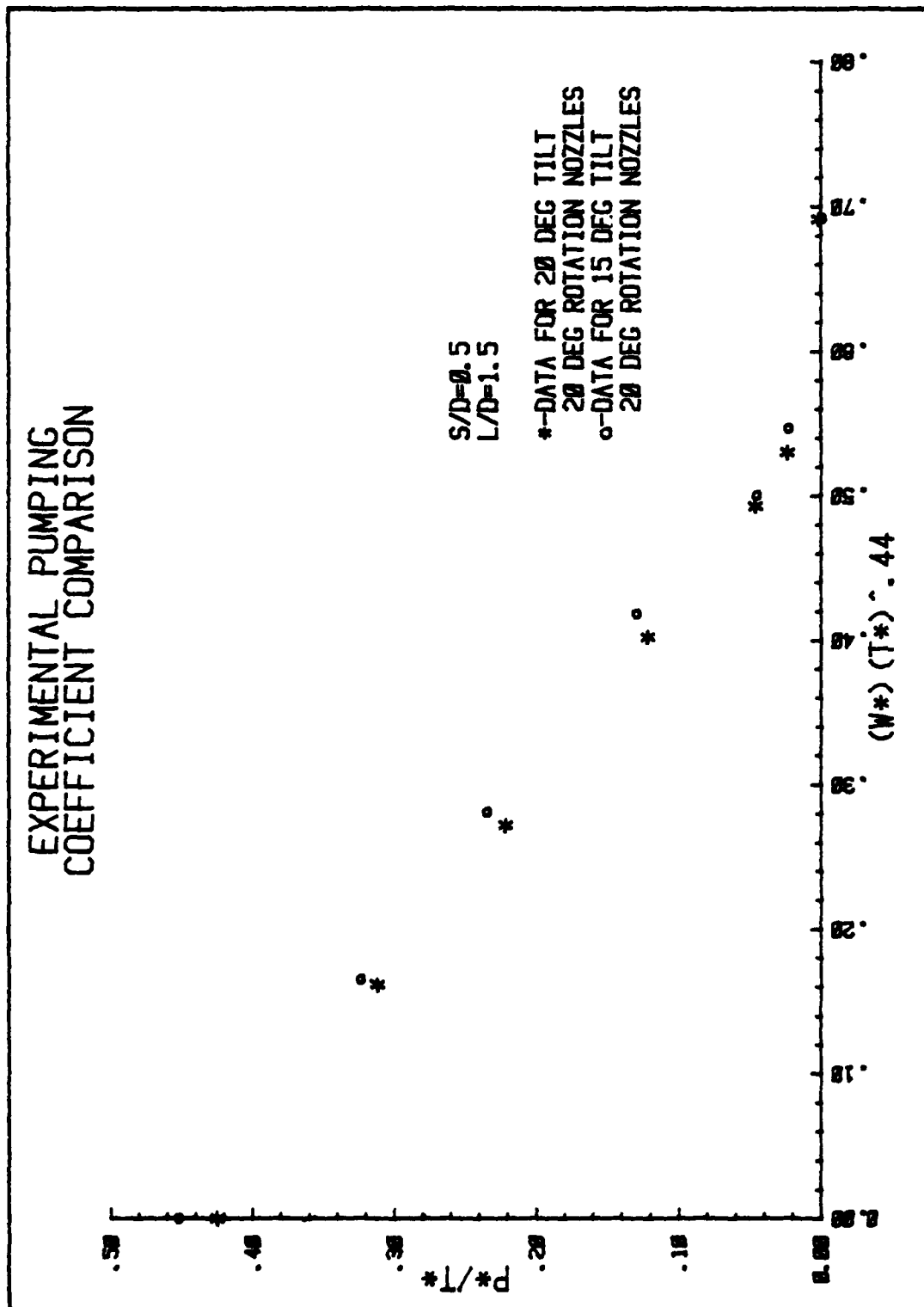


FIGURE 58.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

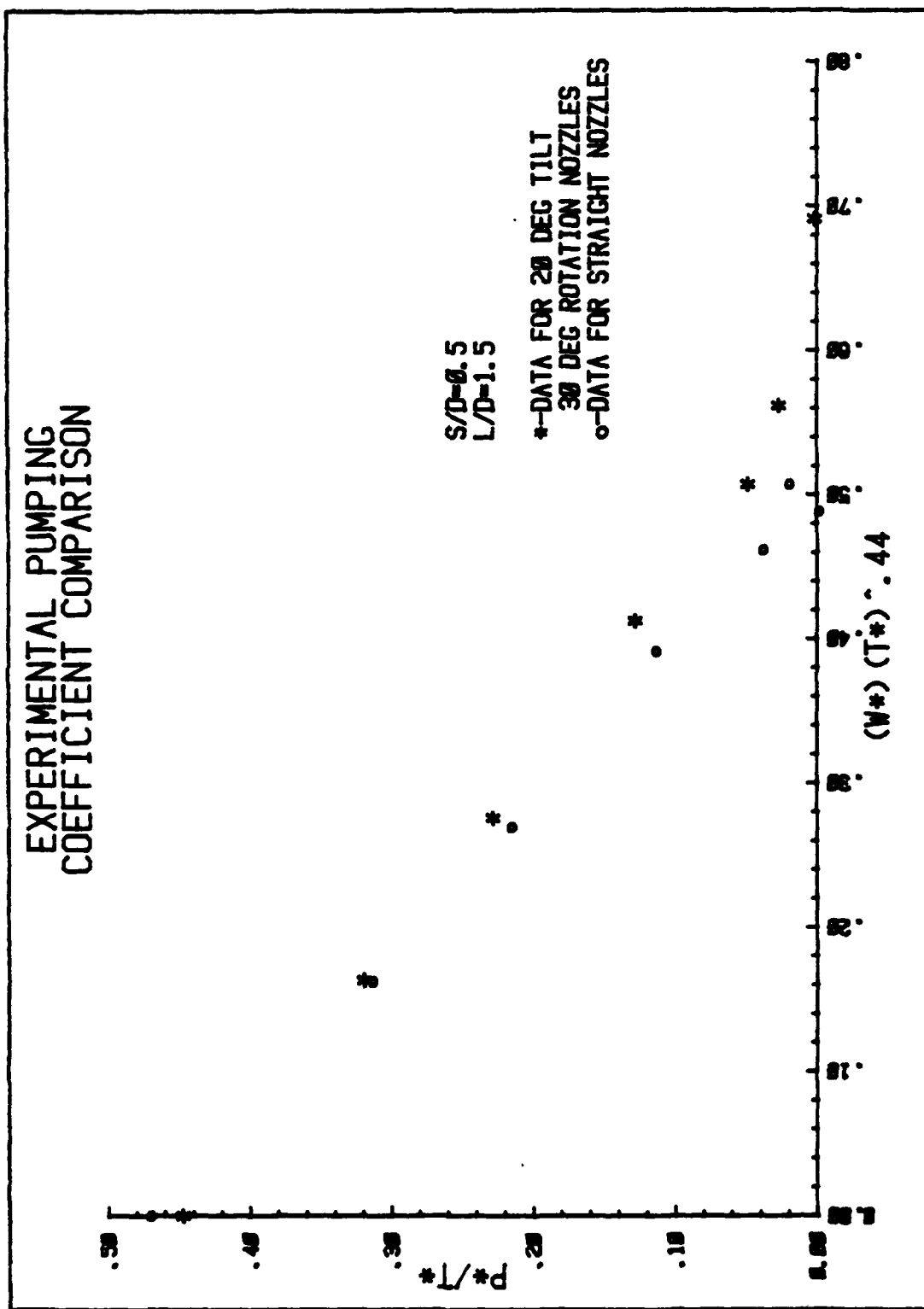


FIGURE 57

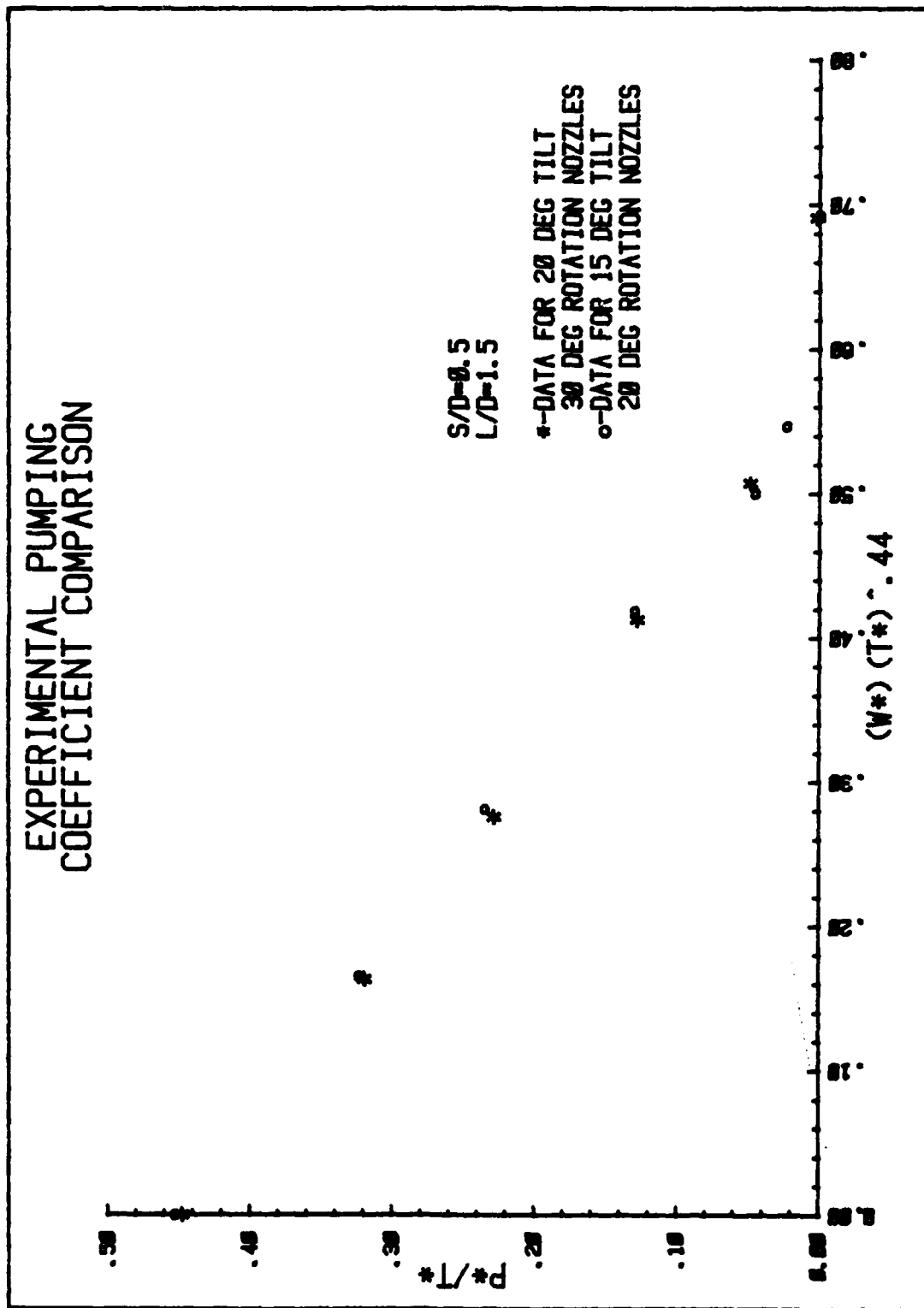


FIGURE 57.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

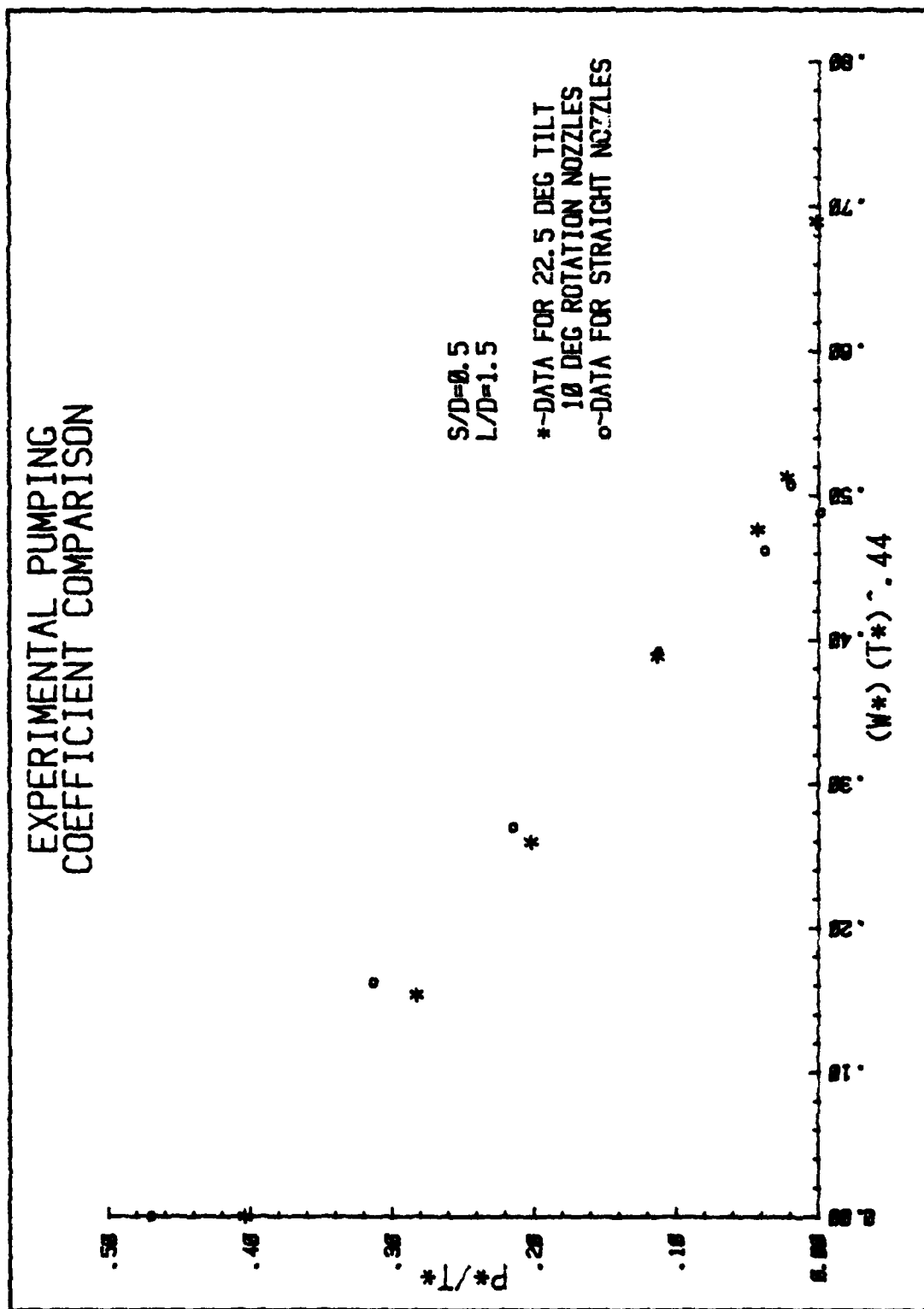


FIGURE 58

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

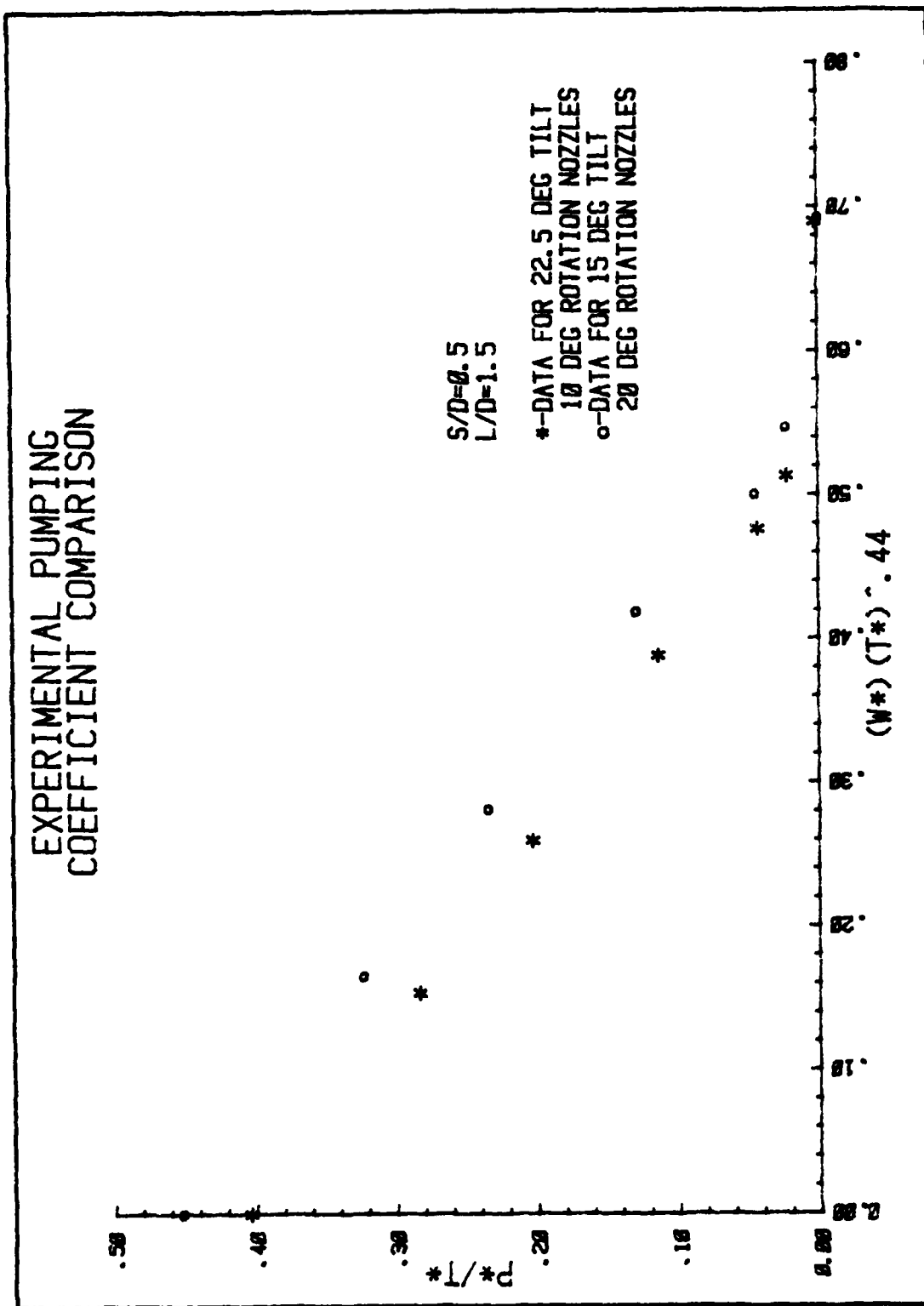


FIGURE 58.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

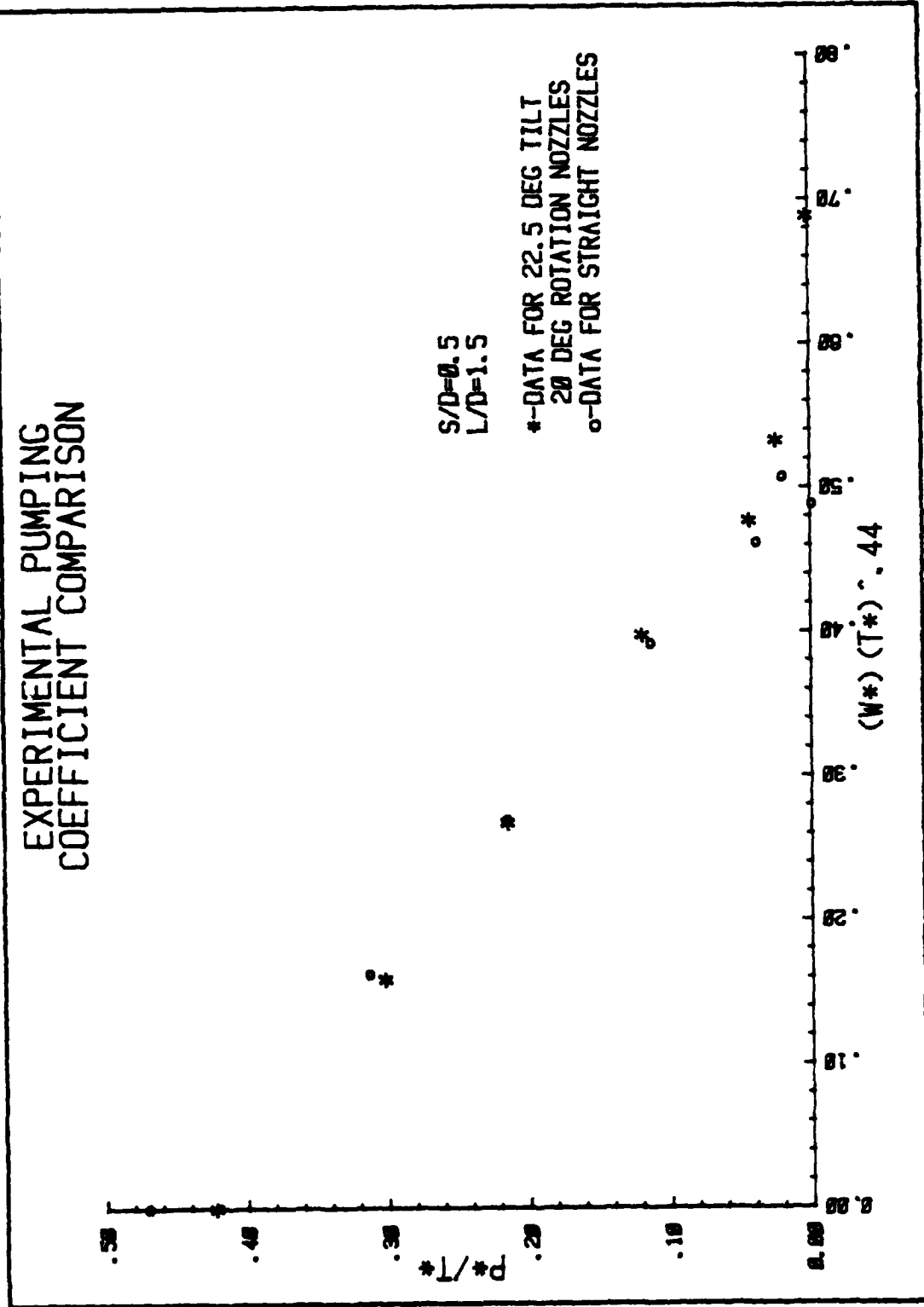


FIGURE 50

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

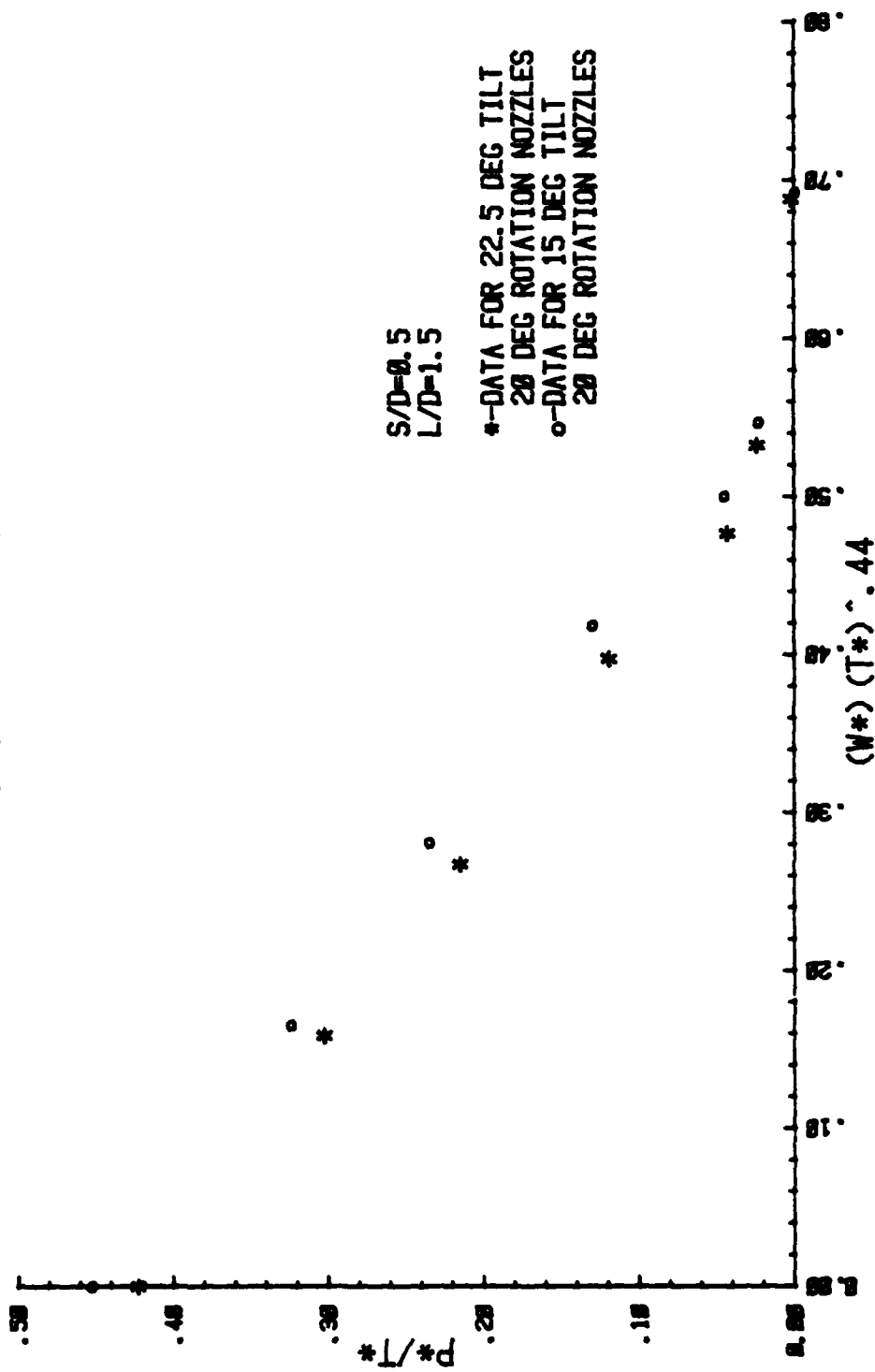


FIGURE 59.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

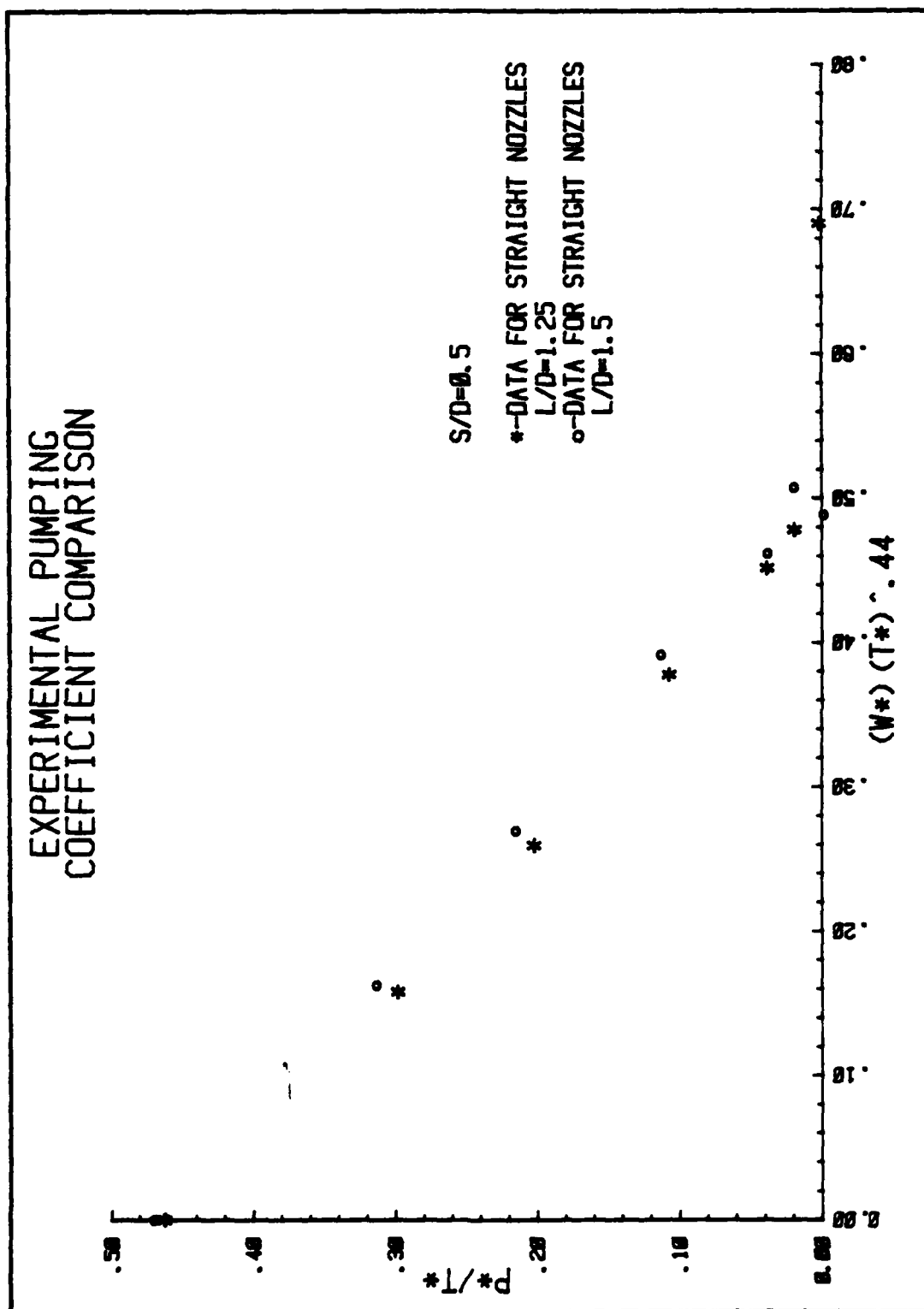


FIGURE 68



# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

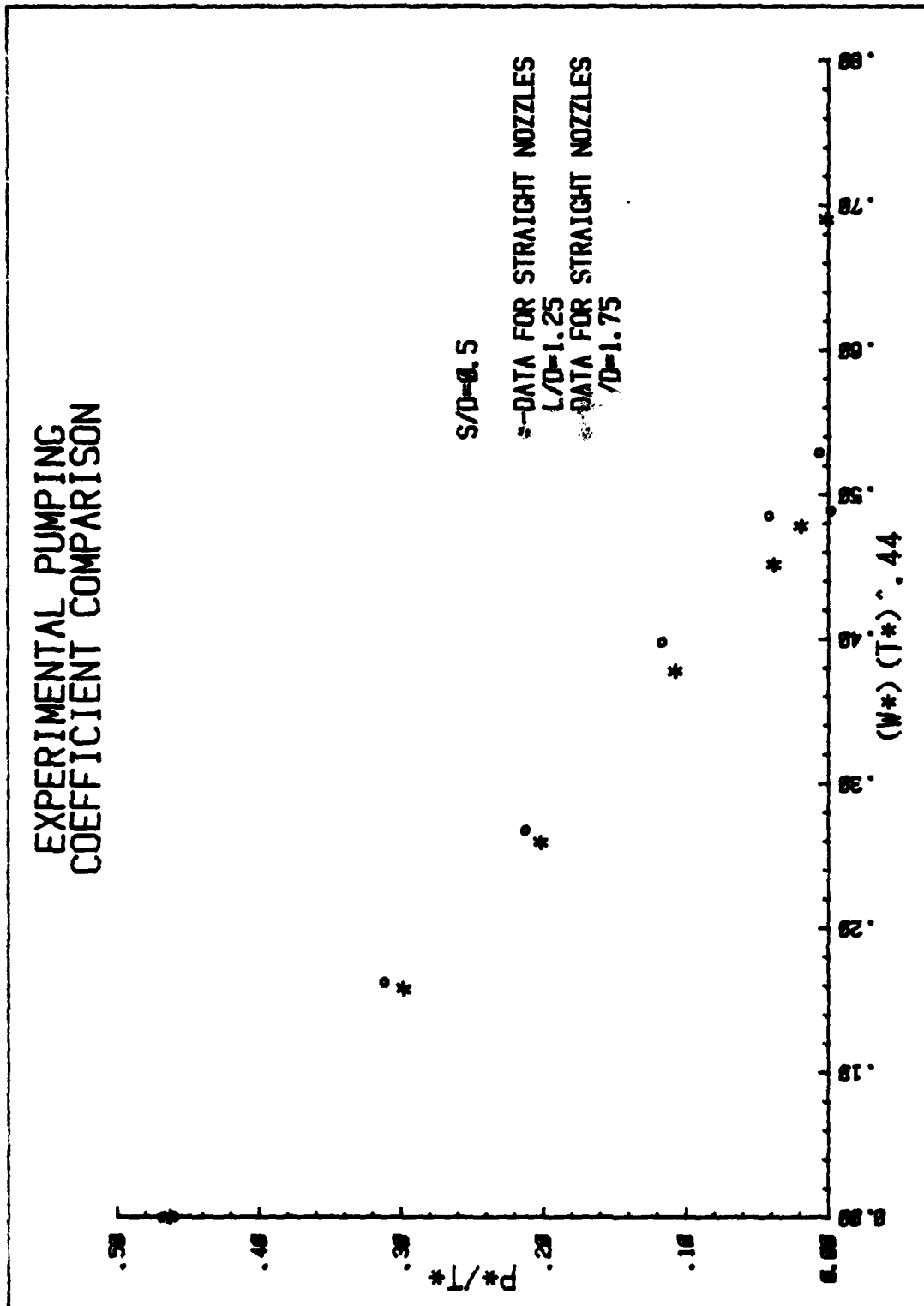


FIGURE 60.1

# AXIAL PRESSURE DISTRIBUTION COMPARISON

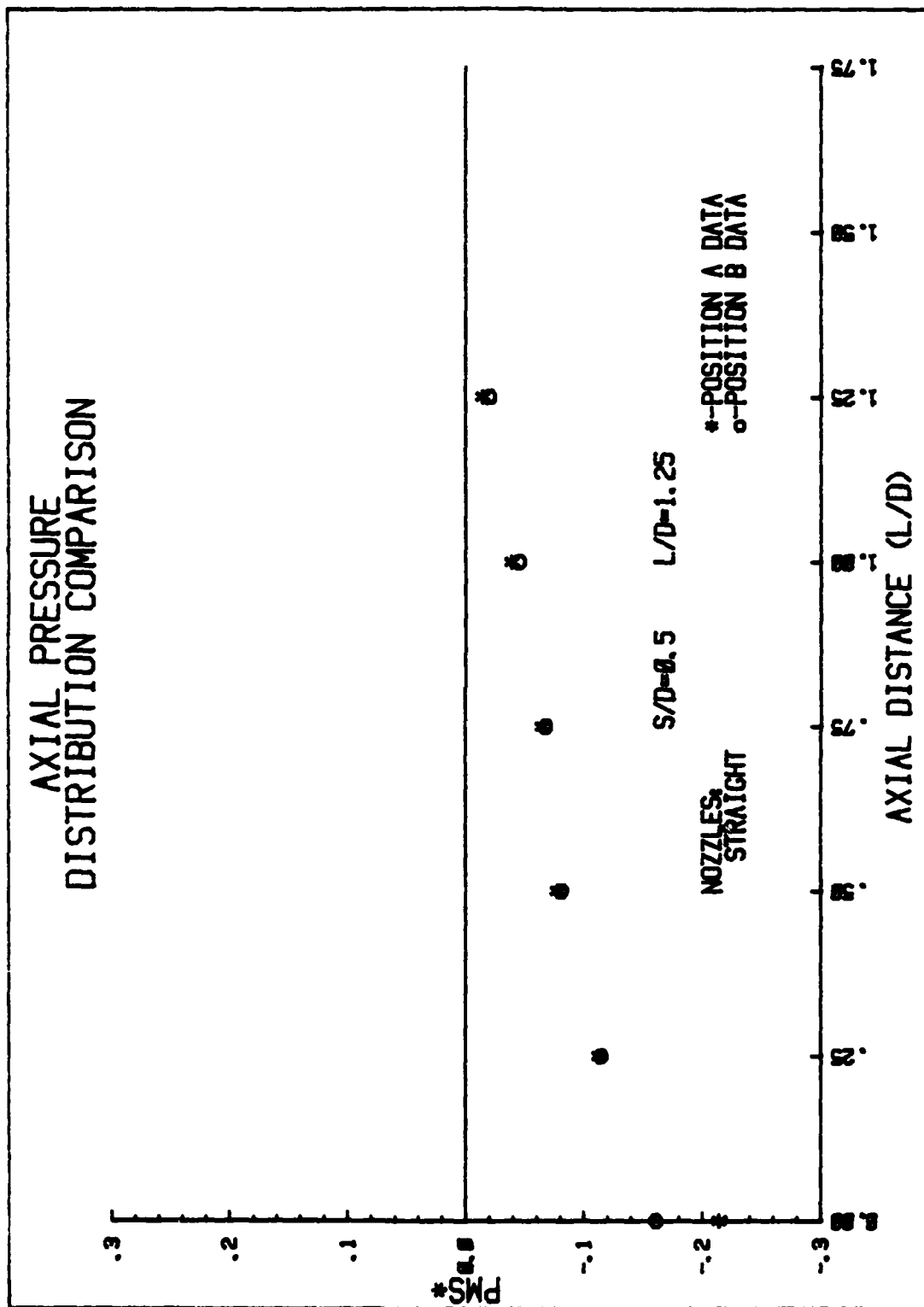


FIGURE 80.2

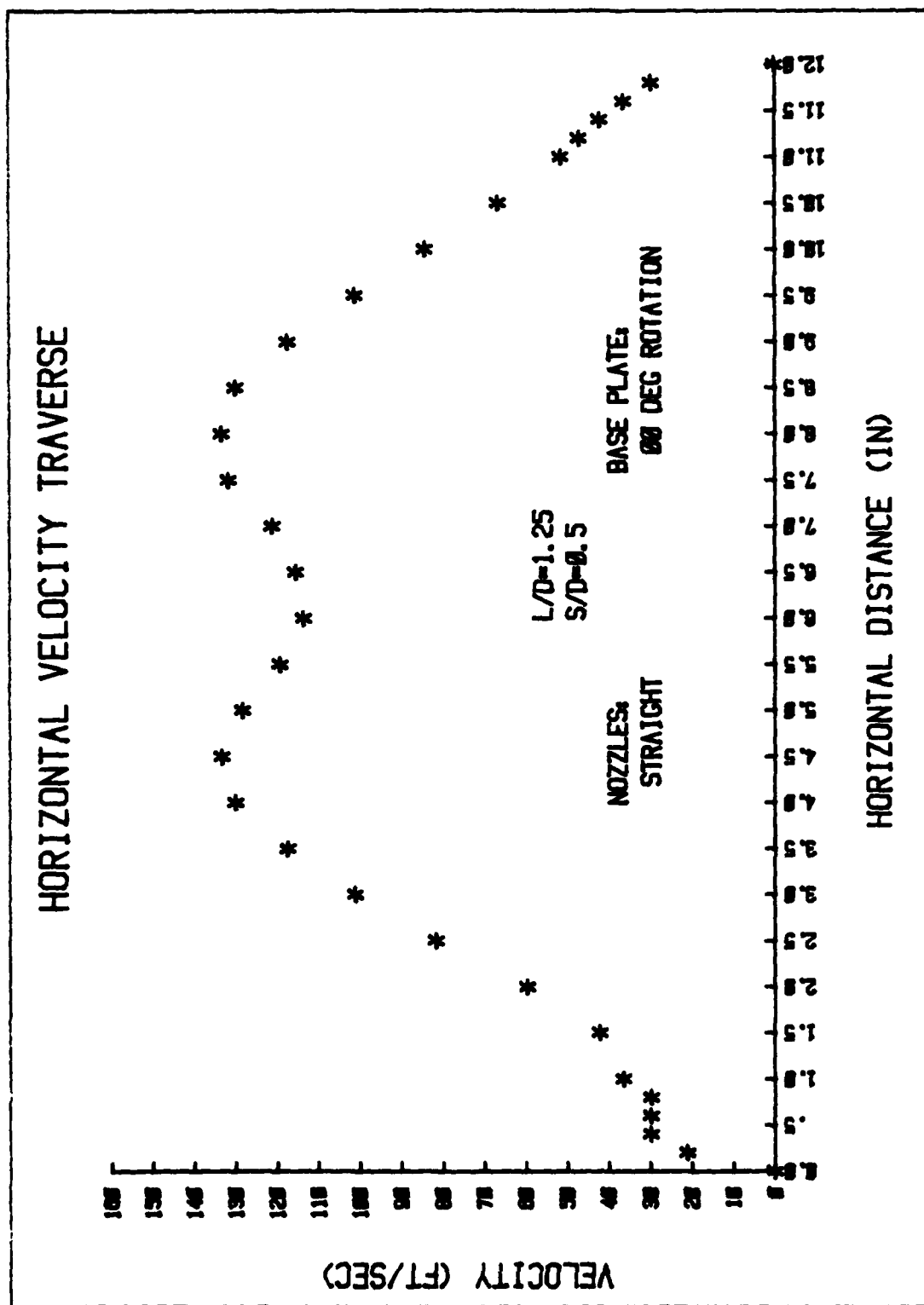


FIGURE 60.3

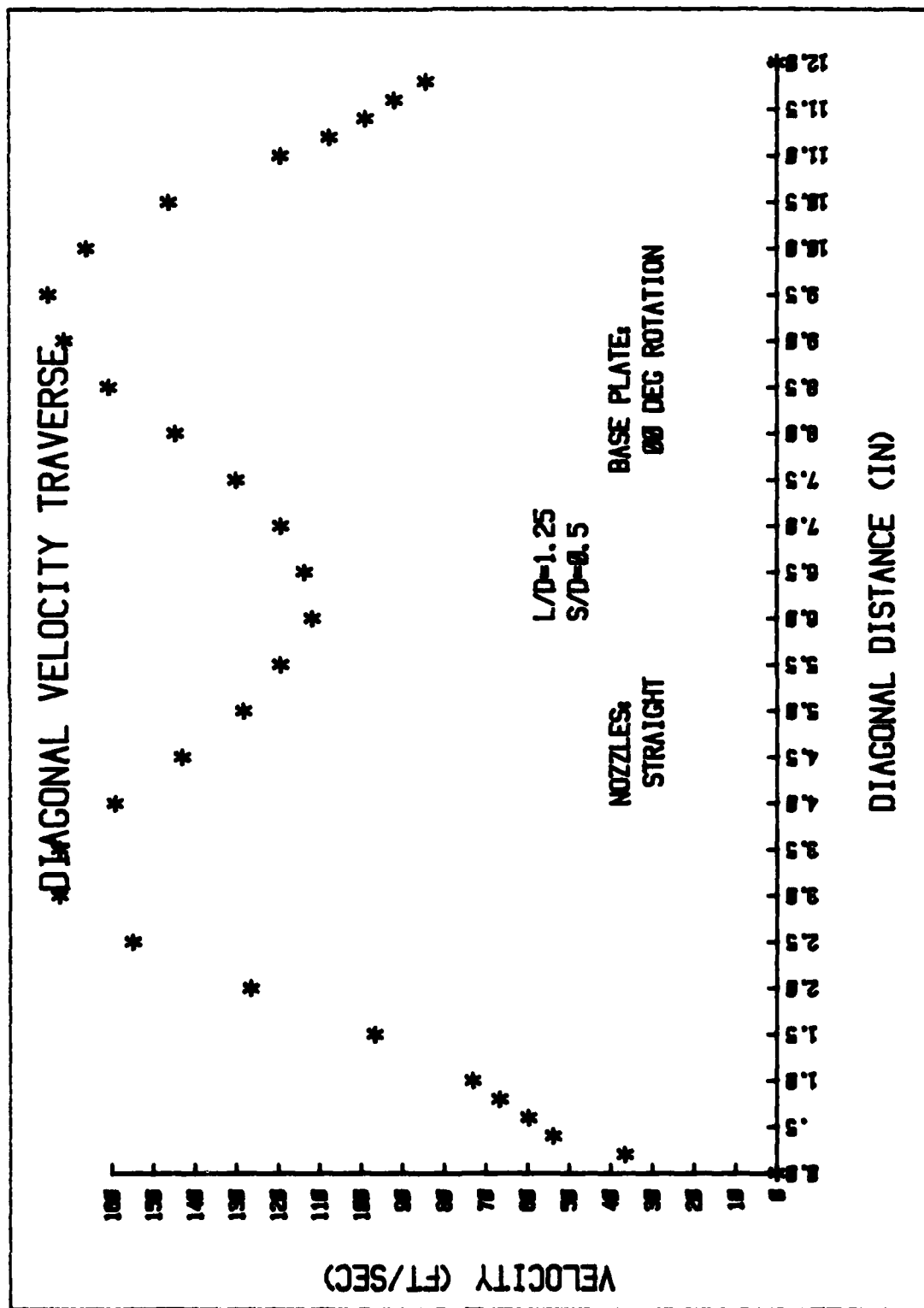


FIGURE 60.4

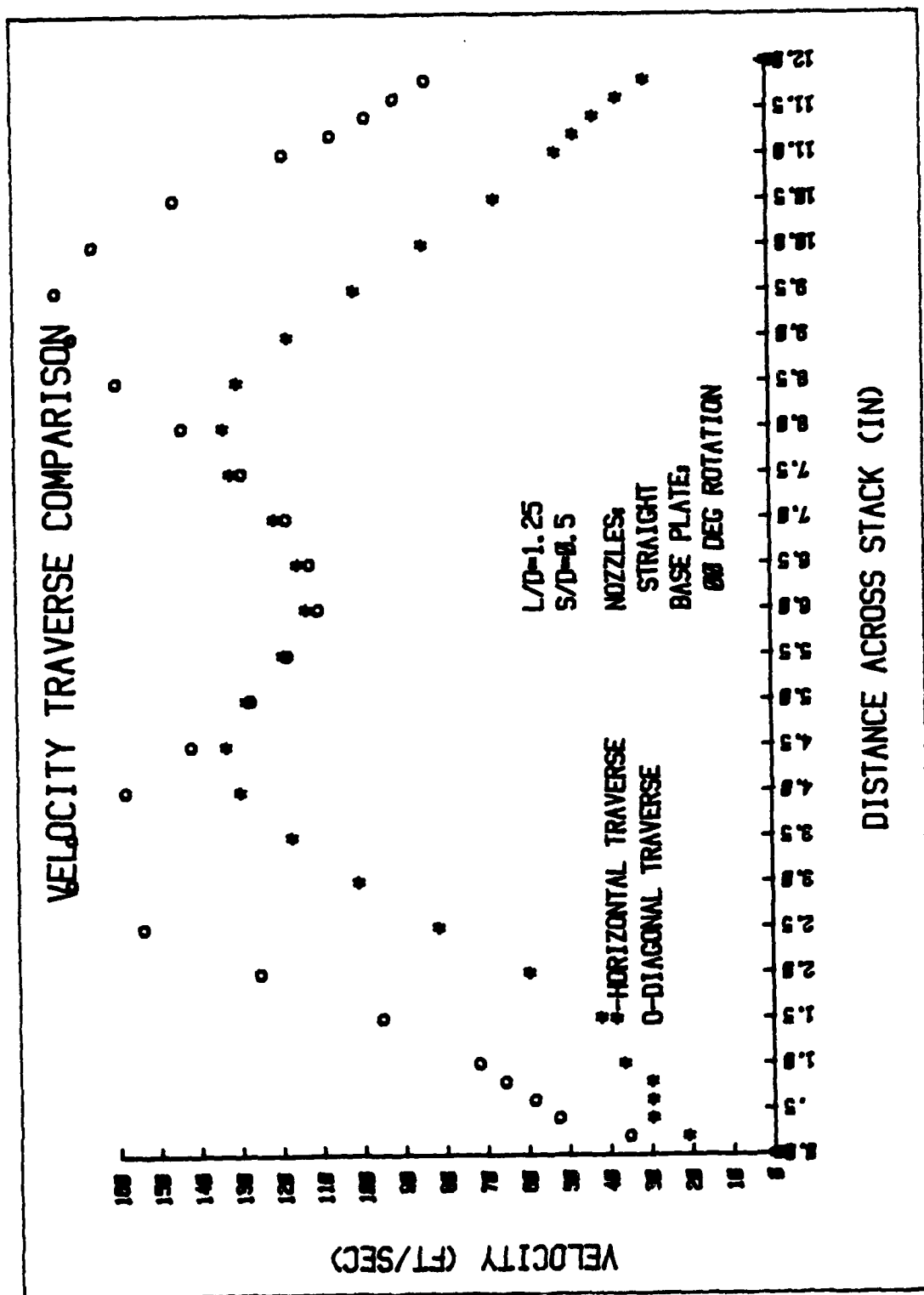


FIGURE 60.5

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

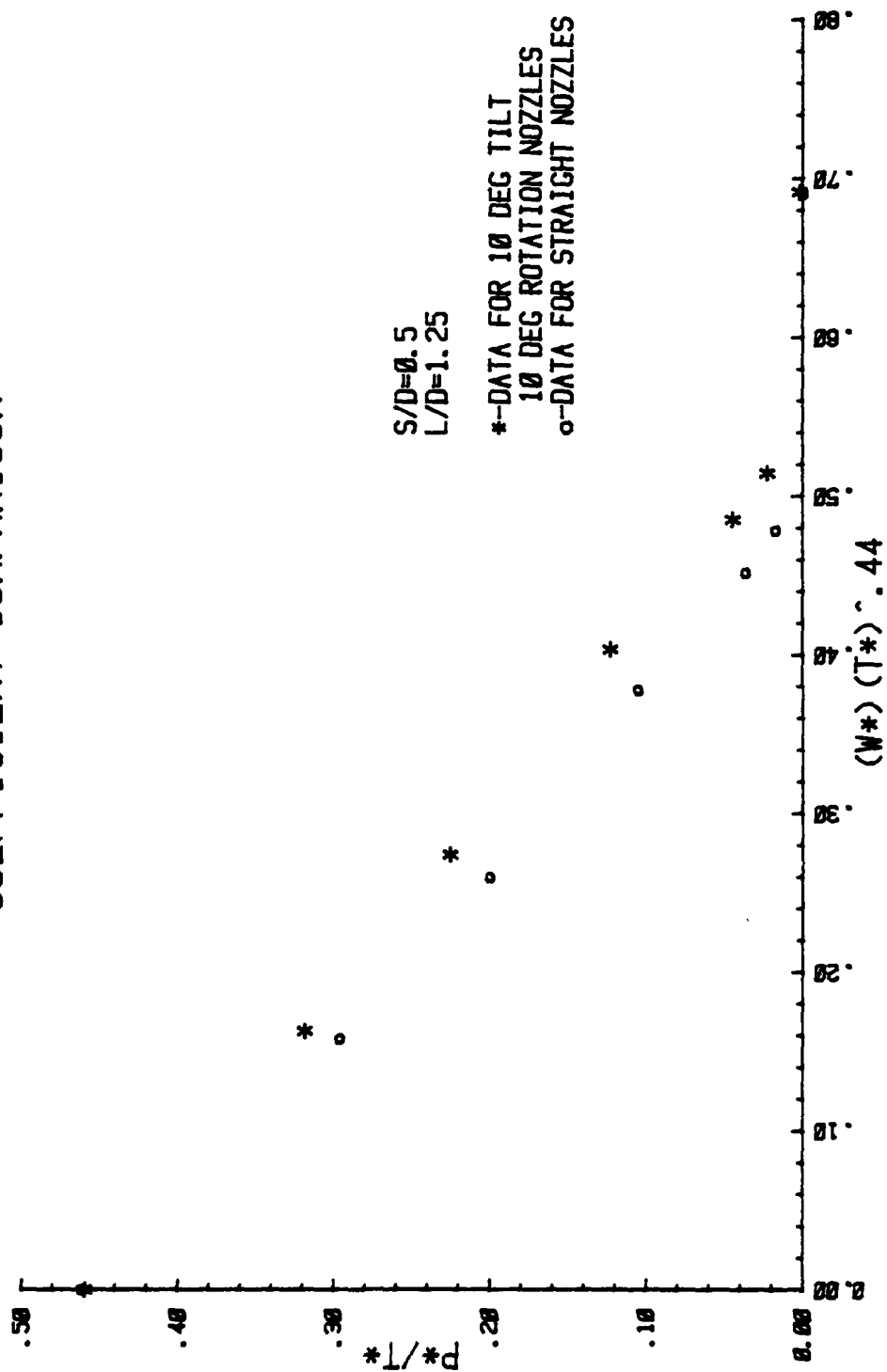


FIGURE 61

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

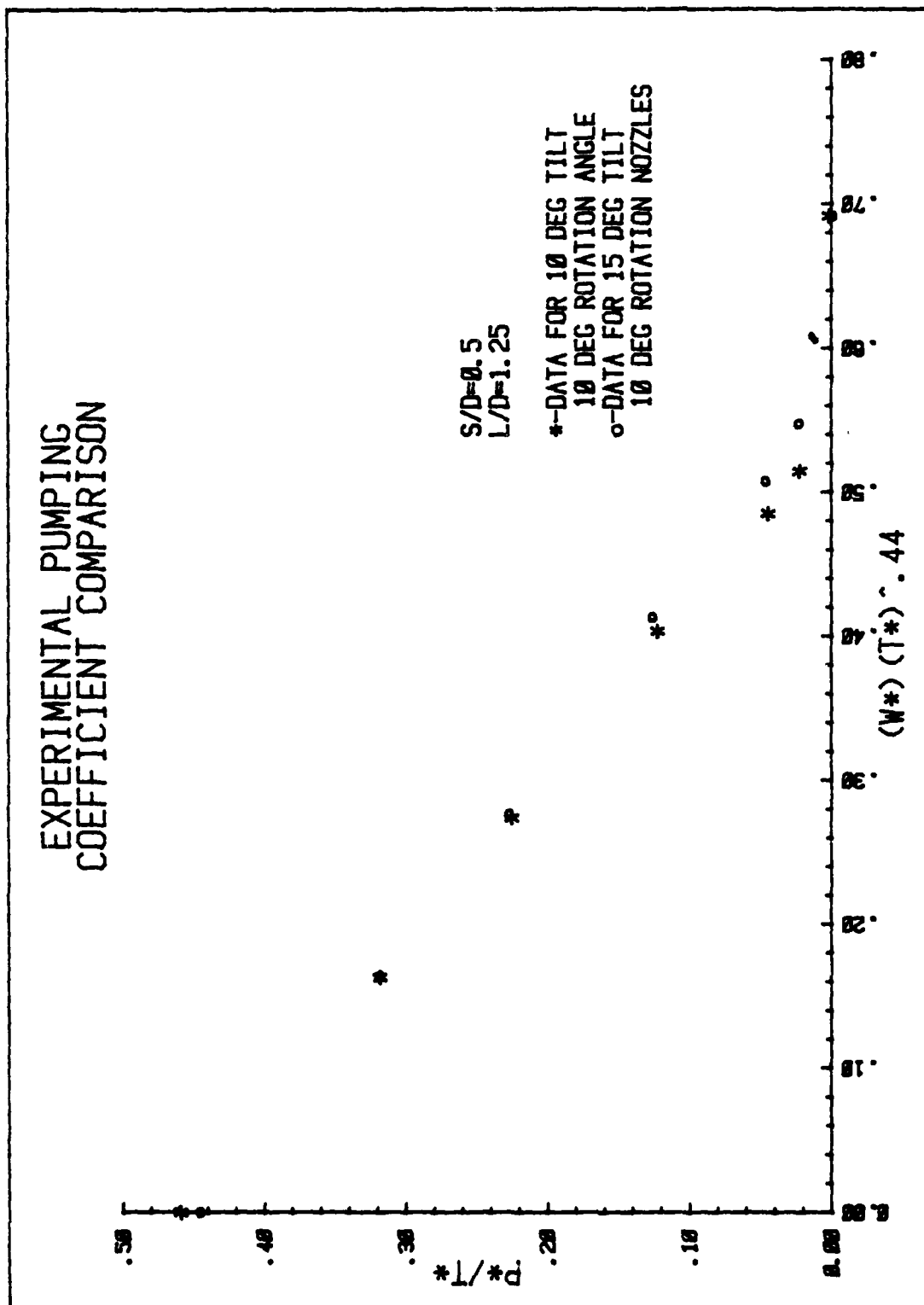


FIGURE 61.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

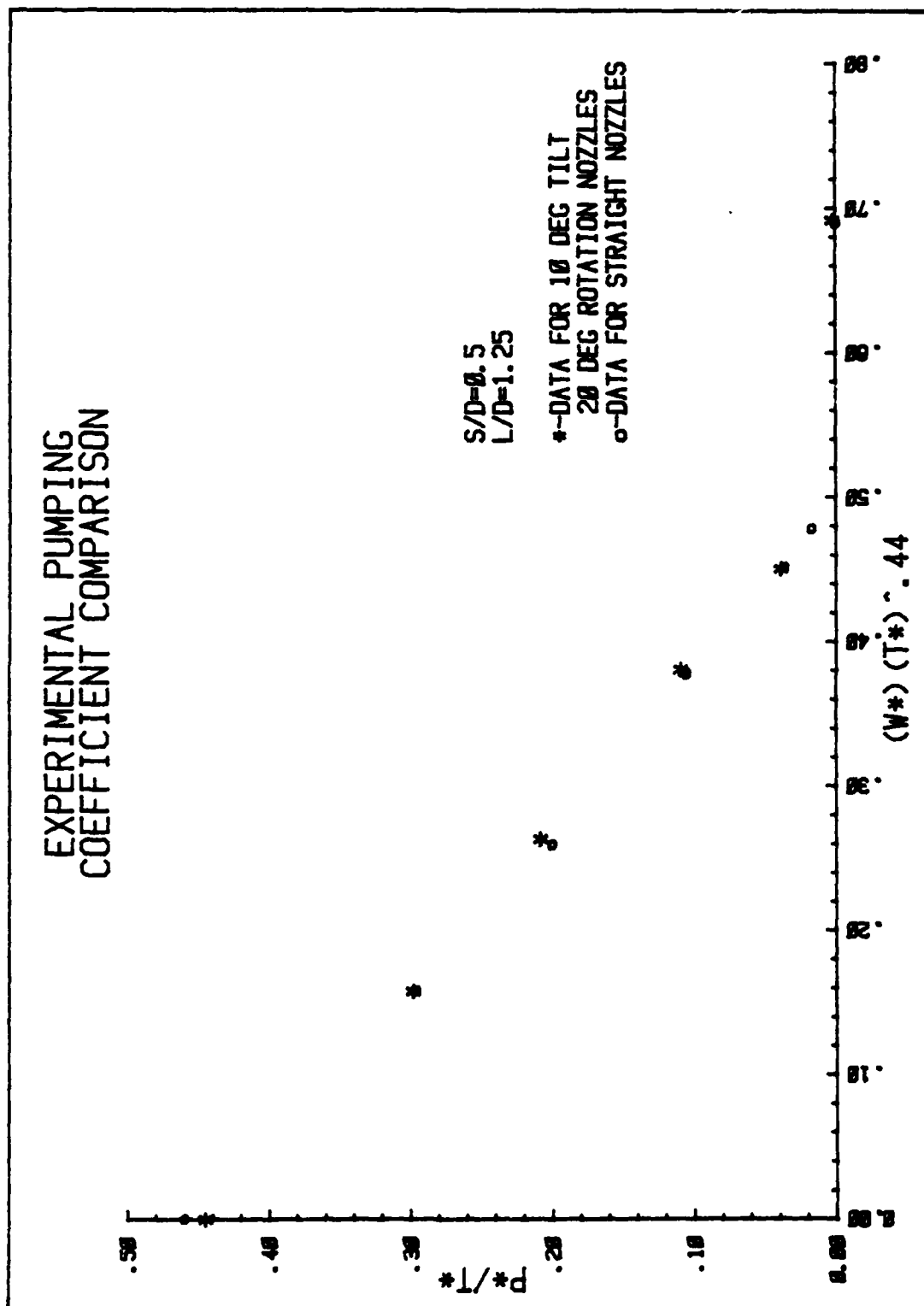


FIGURE 62



# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

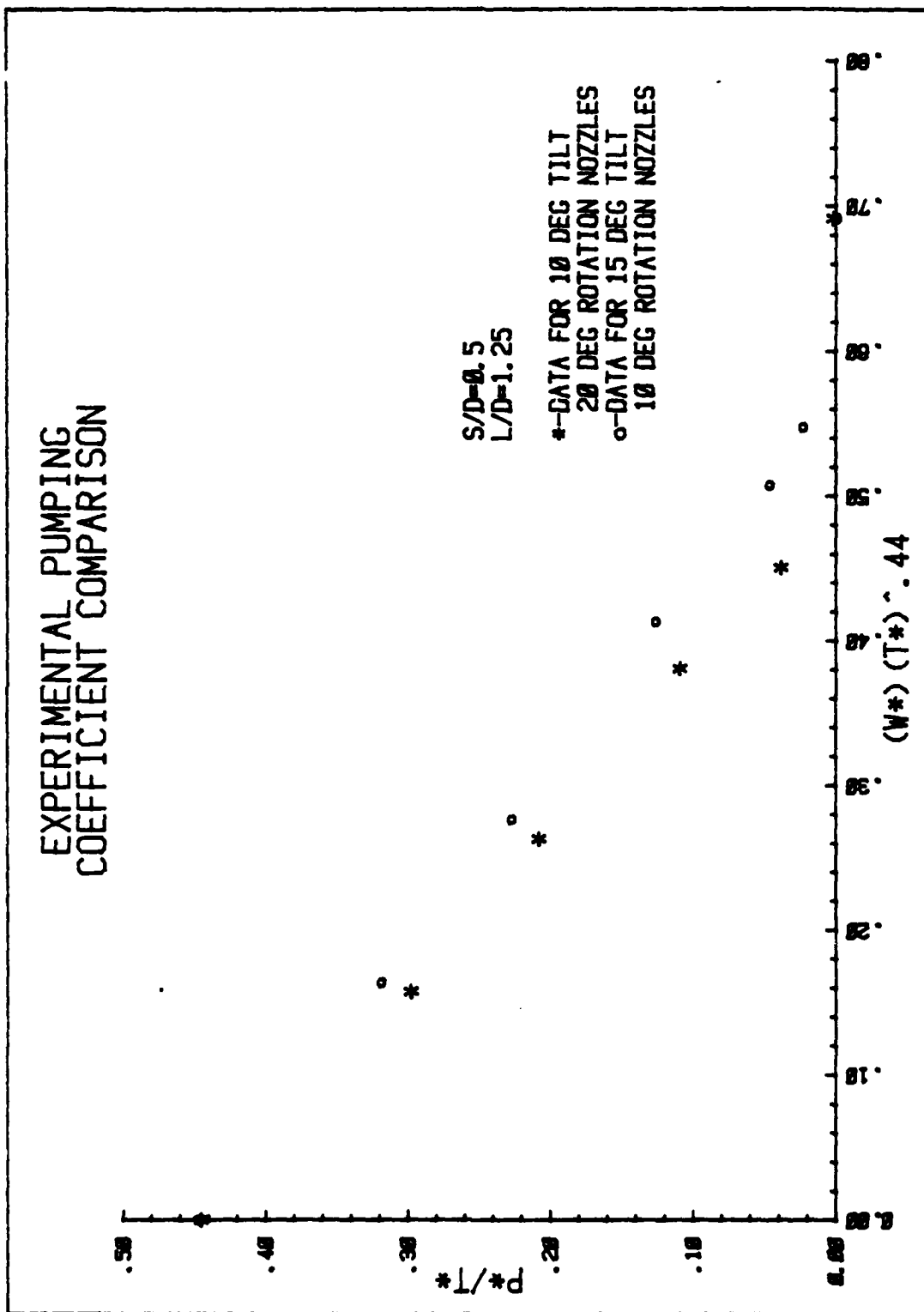


FIGURE 62.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

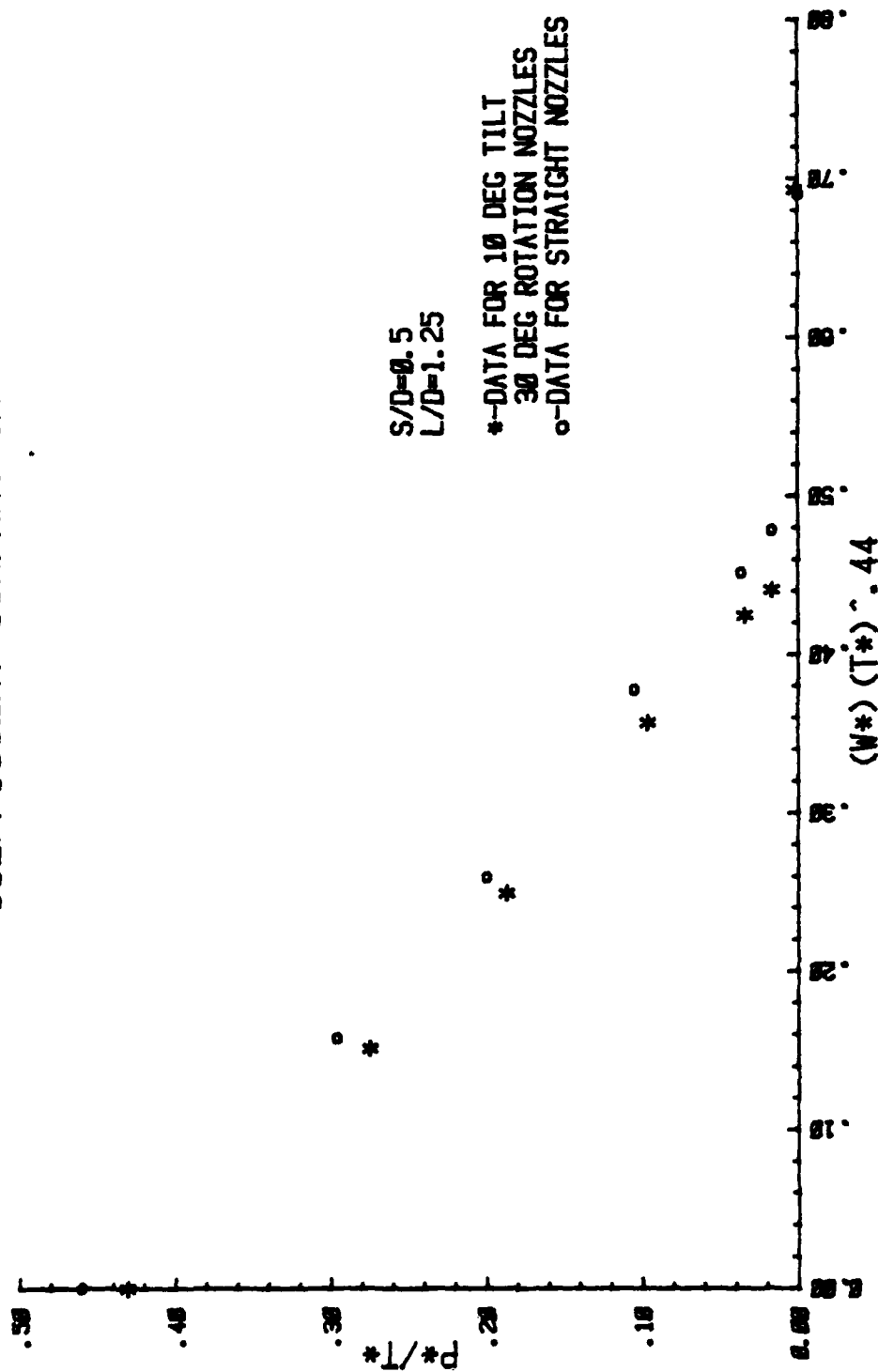


FIGURE 63

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

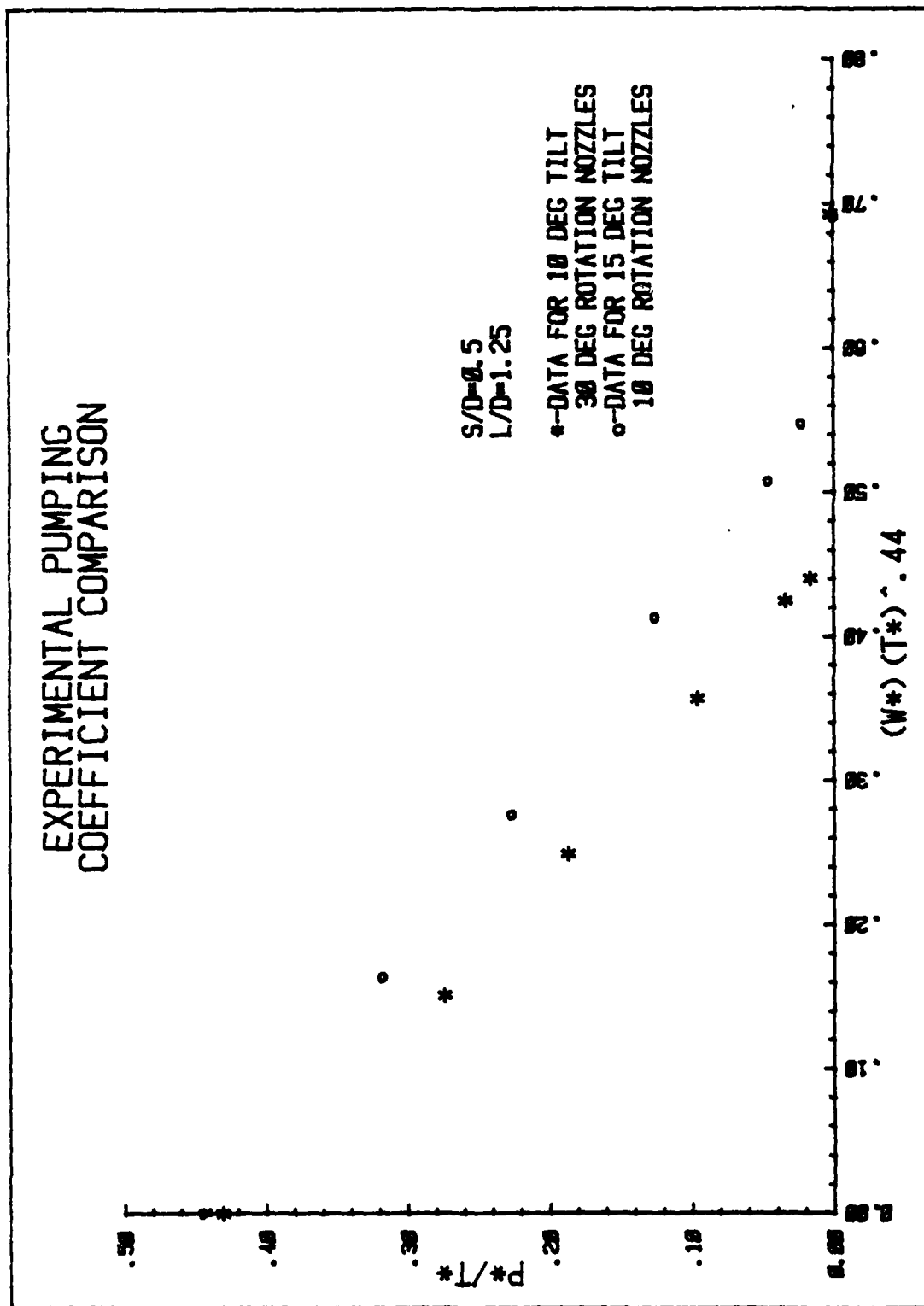


FIGURE 63.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

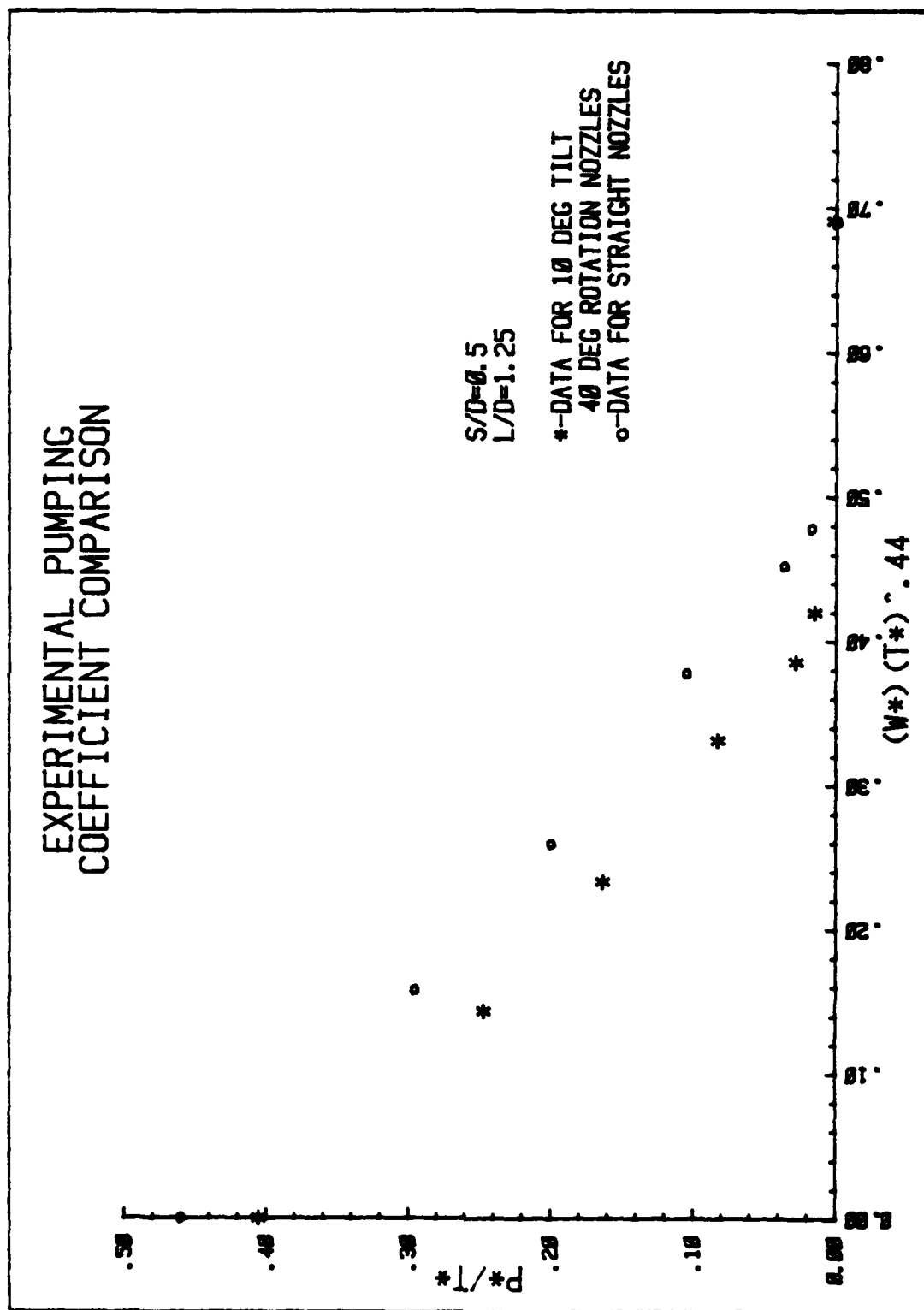


FIGURE 64

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

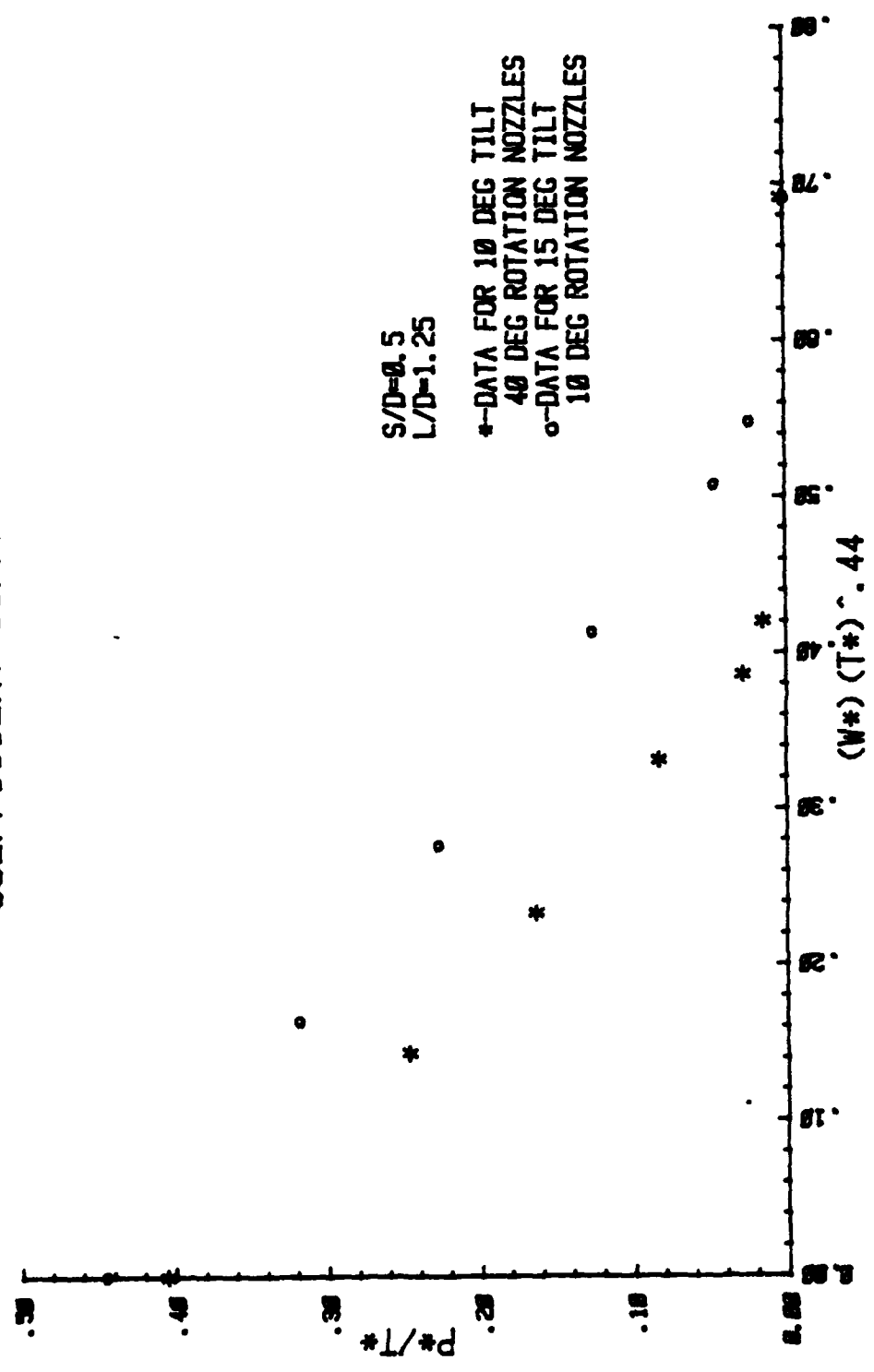


FIGURE 64.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

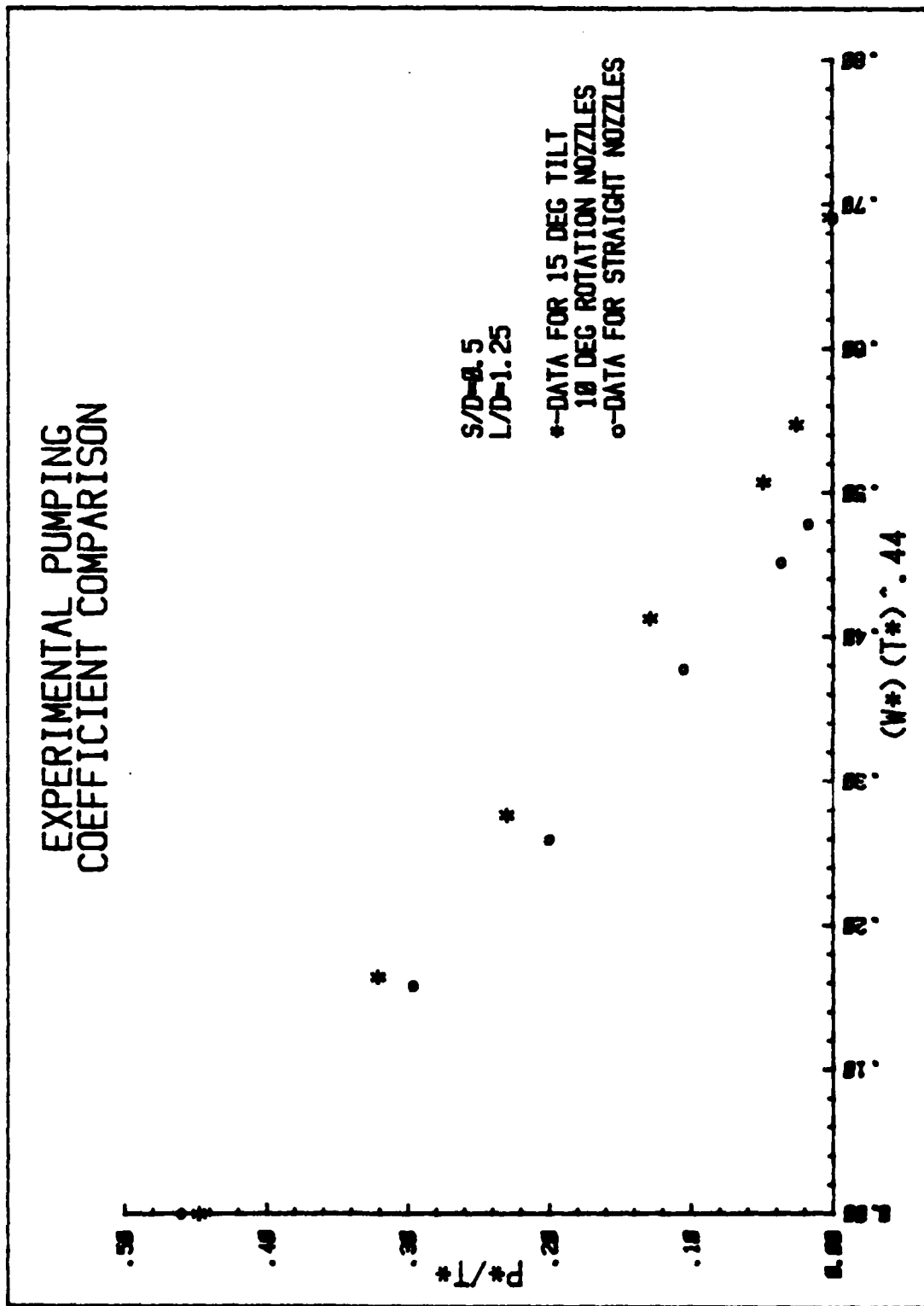


FIGURE 65

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

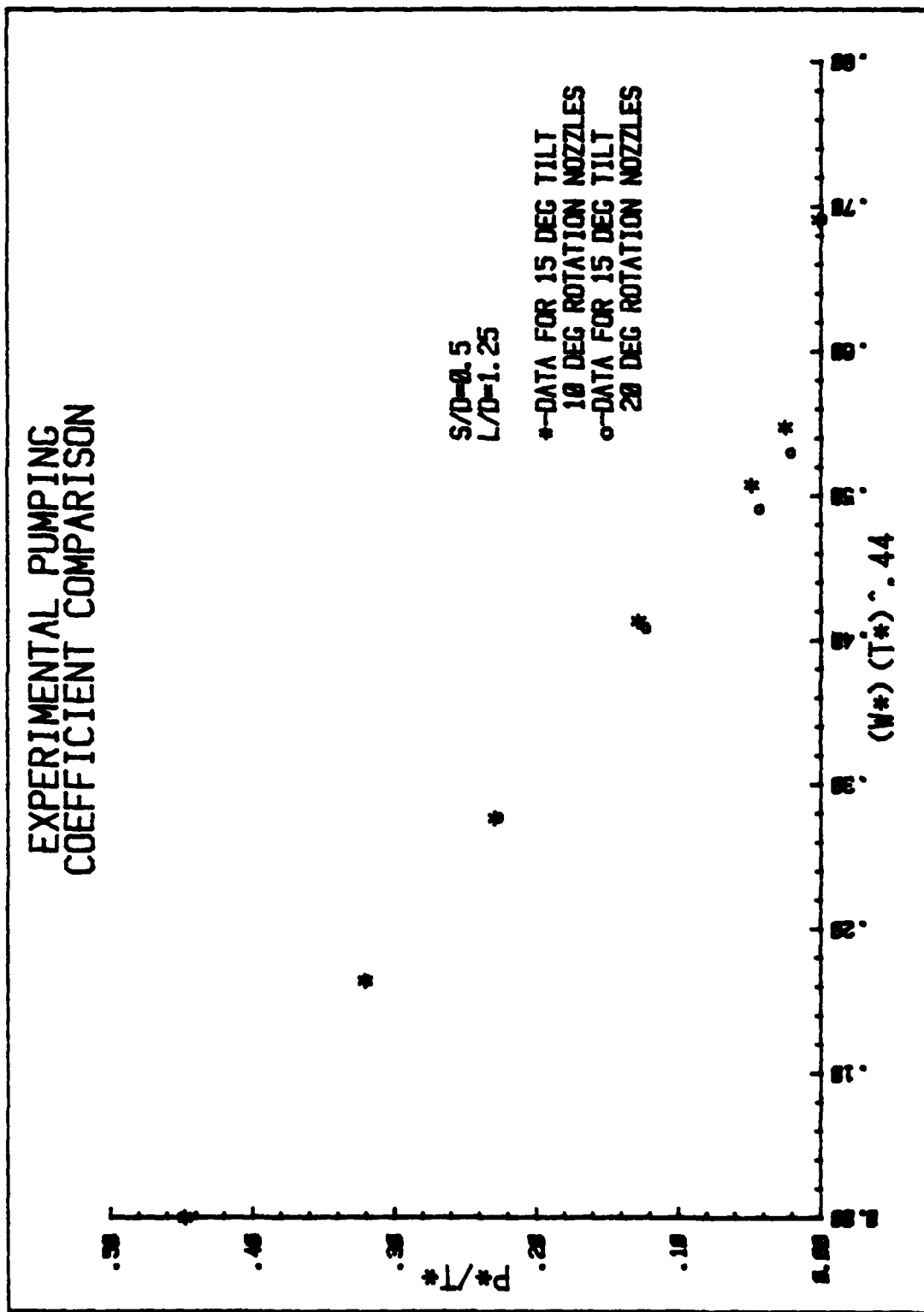


FIGURE 85.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

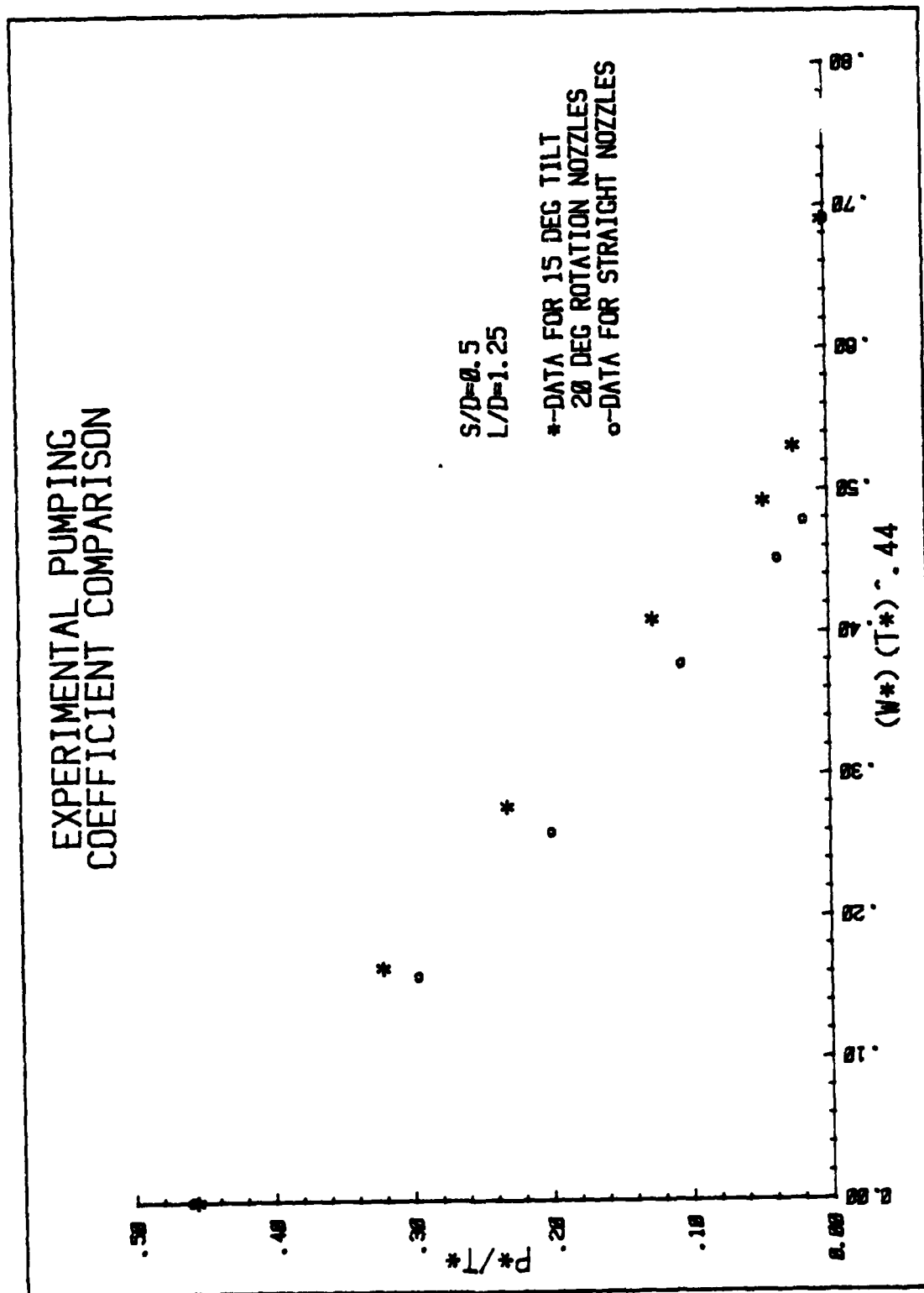


FIGURE 88



# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

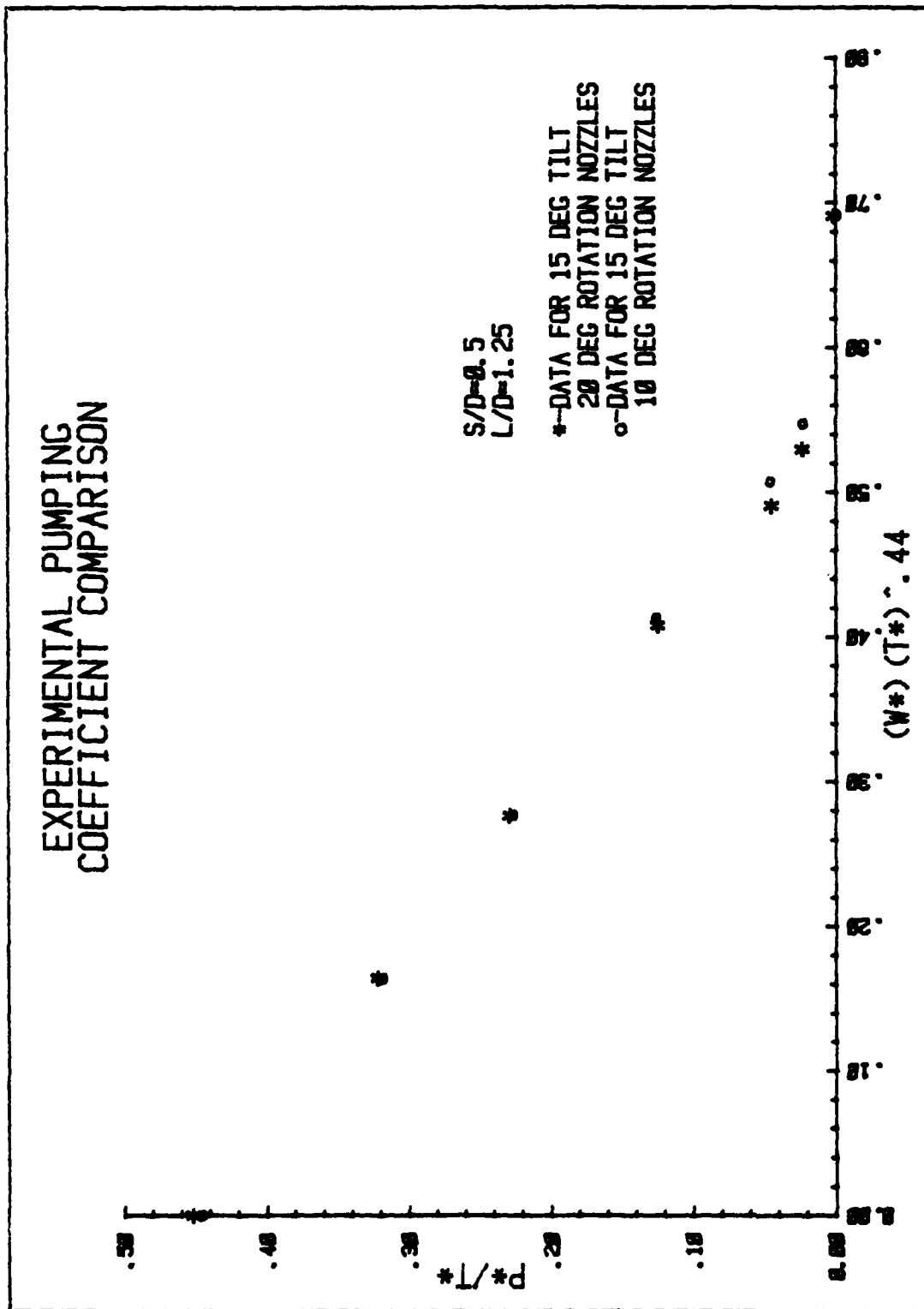


FIGURE 68.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

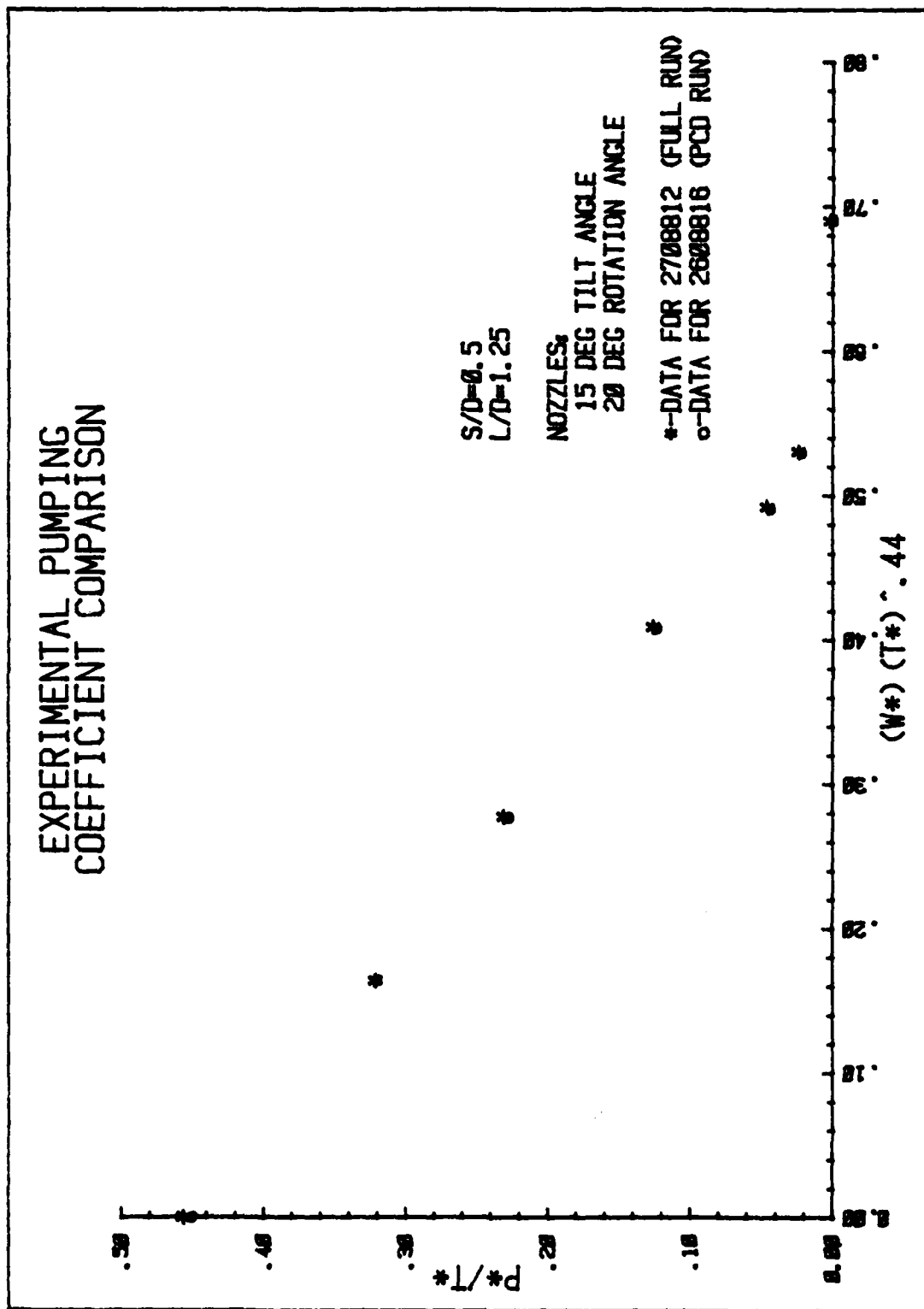


FIGURE 67

# AXIAL PRESSURE DISTRIBUTION COMPARISON

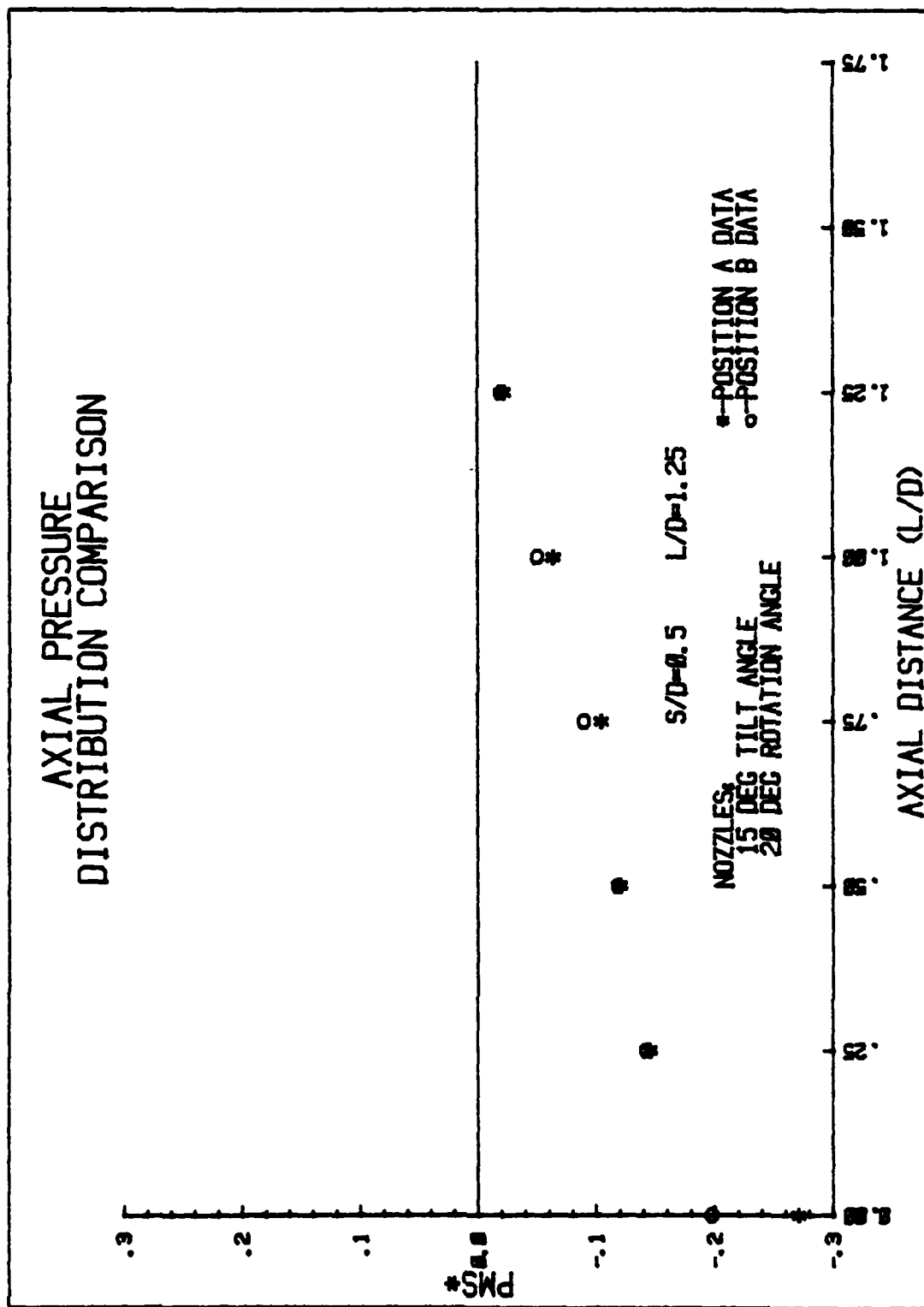


FIGURE 07.1

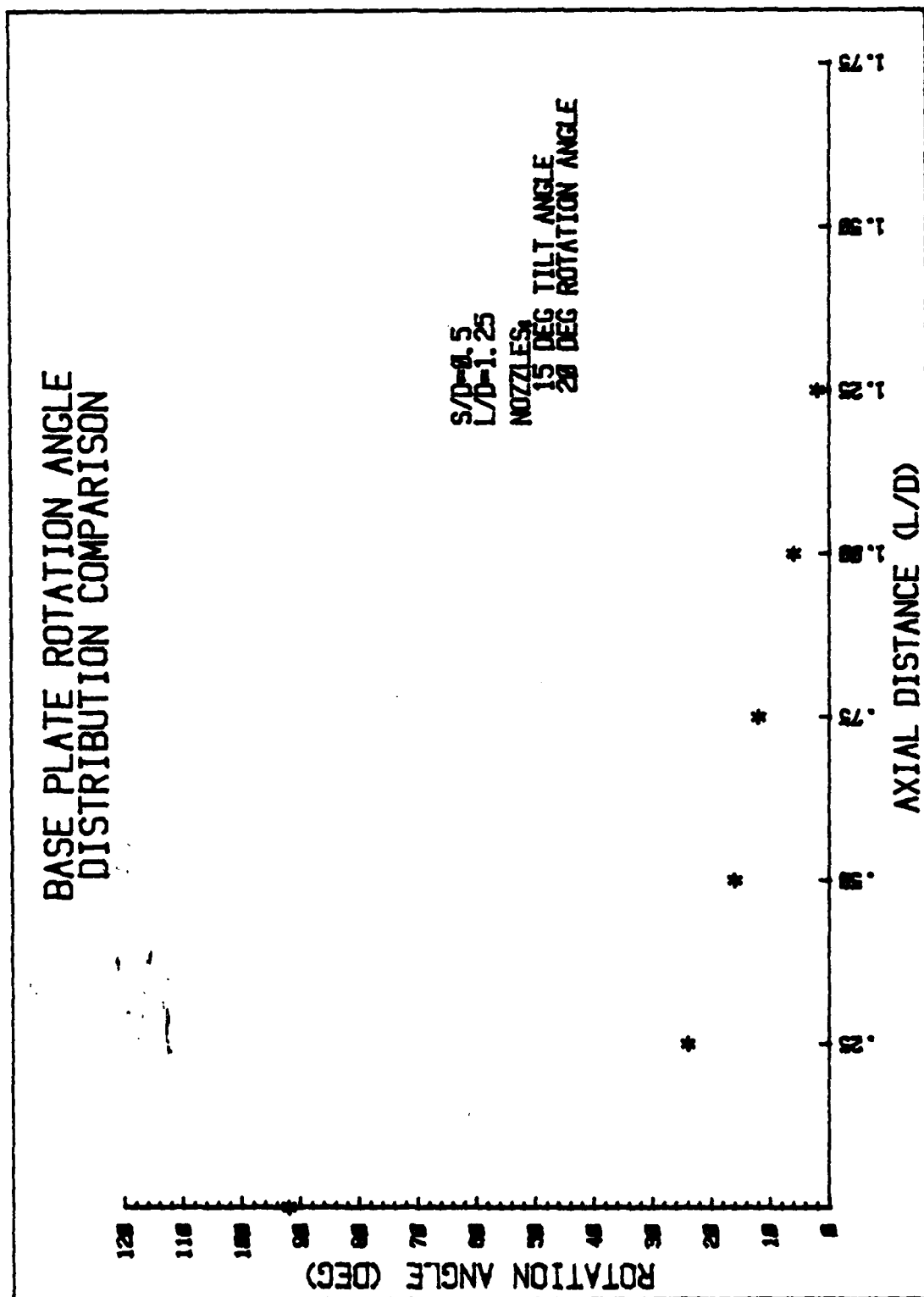
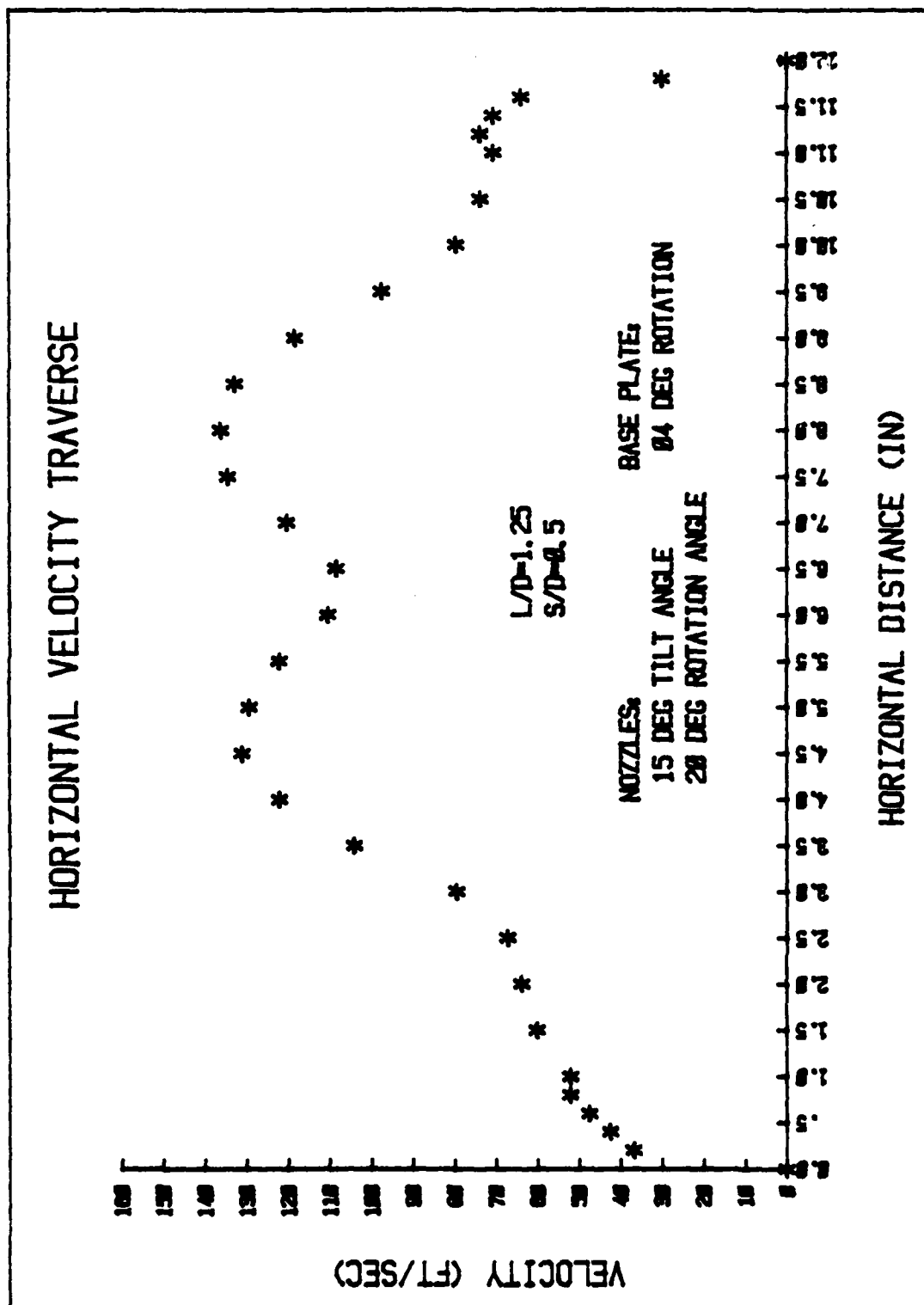


FIGURE 67.2



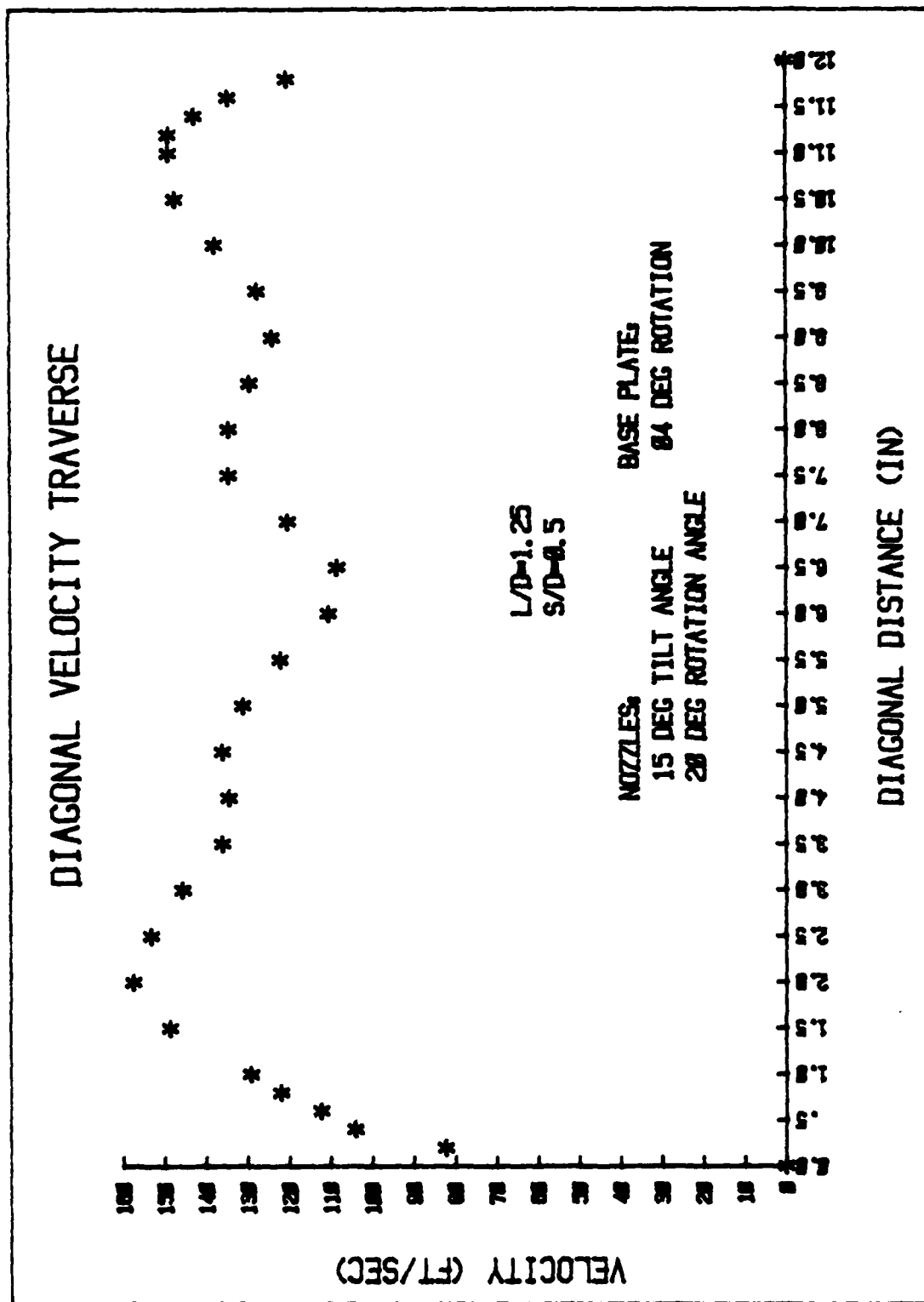


FIGURE 87.4

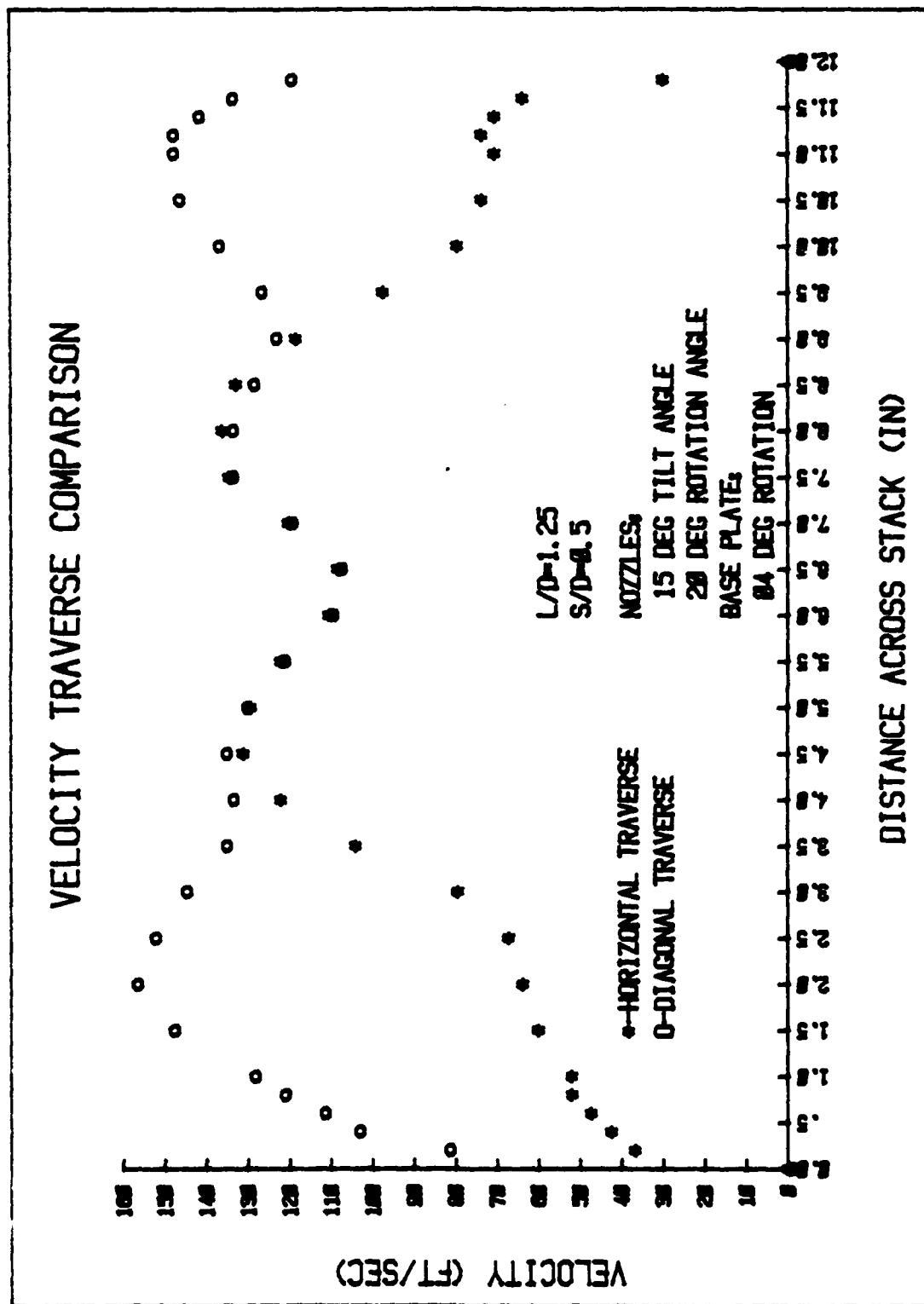
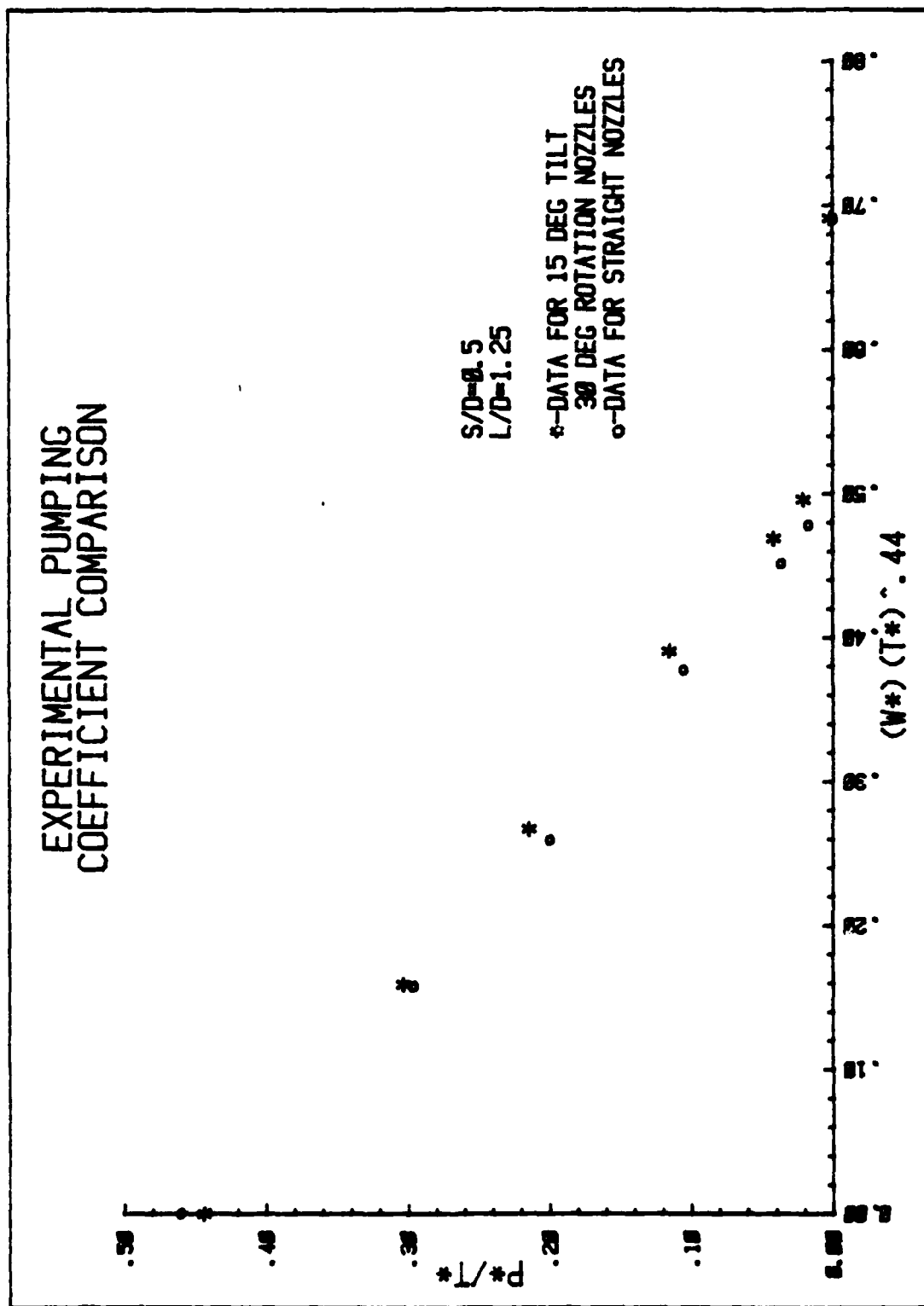


FIGURE 67.5

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON





# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

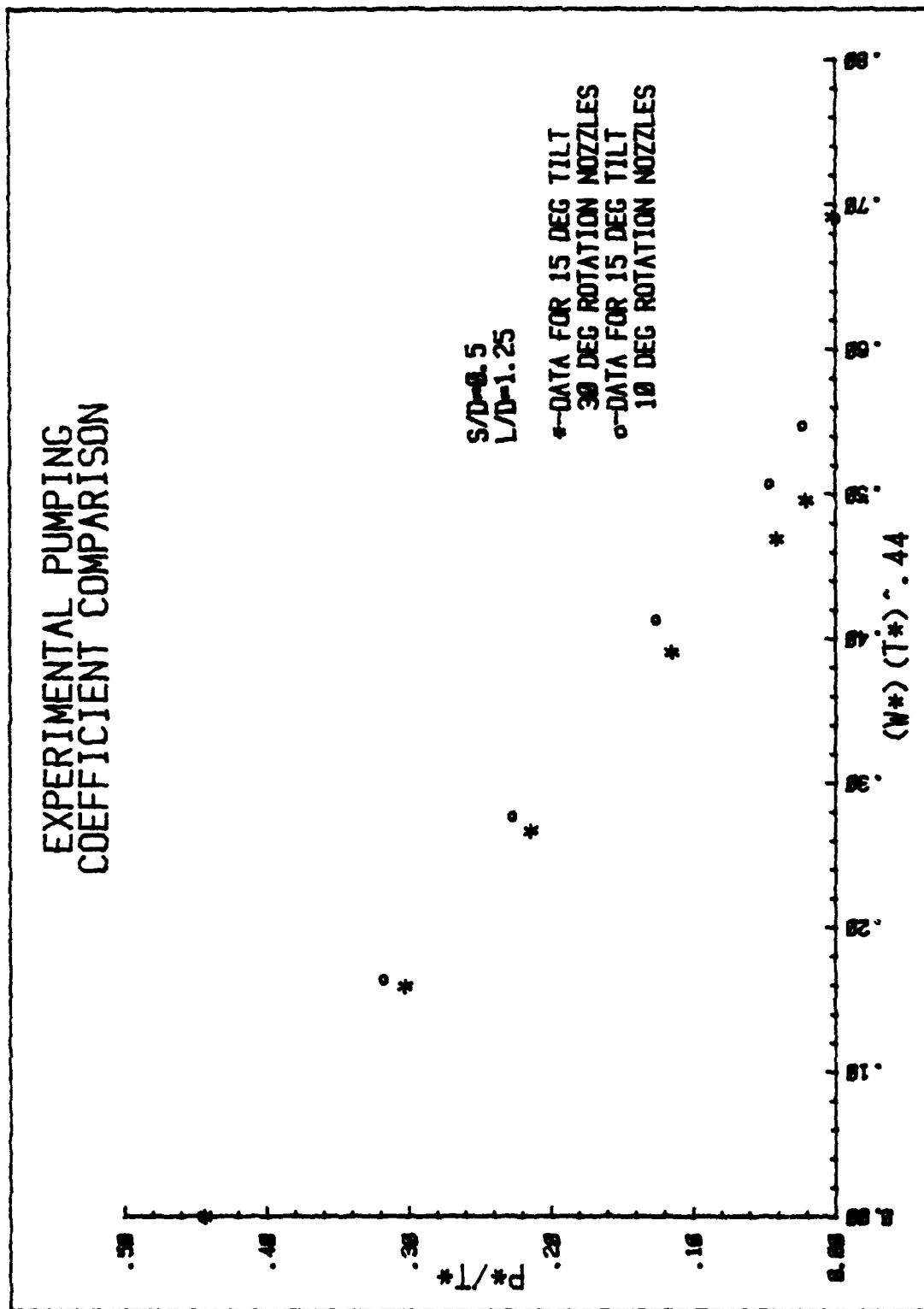


FIGURE 68.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

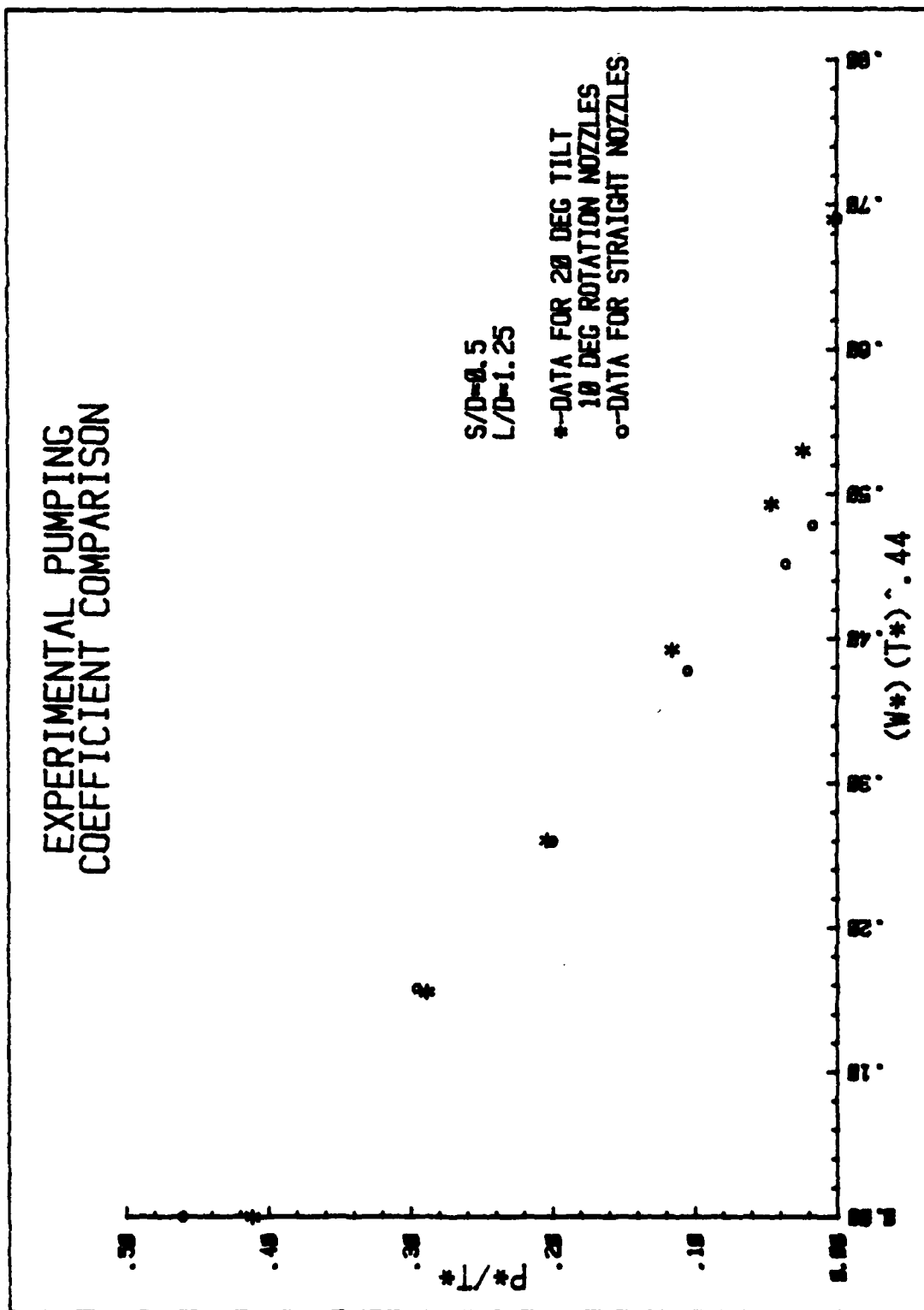


FIGURE 88

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

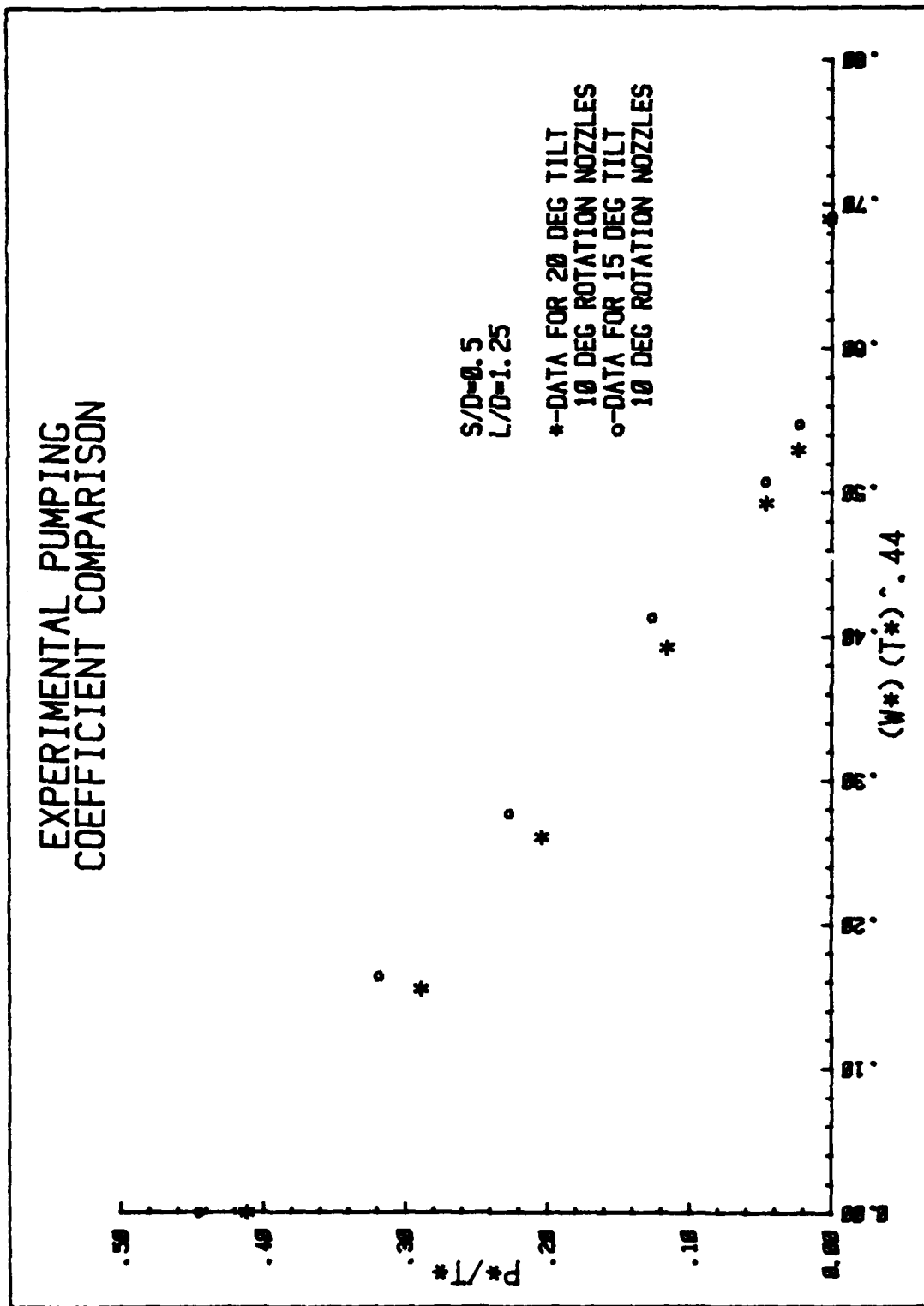


FIGURE 69.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

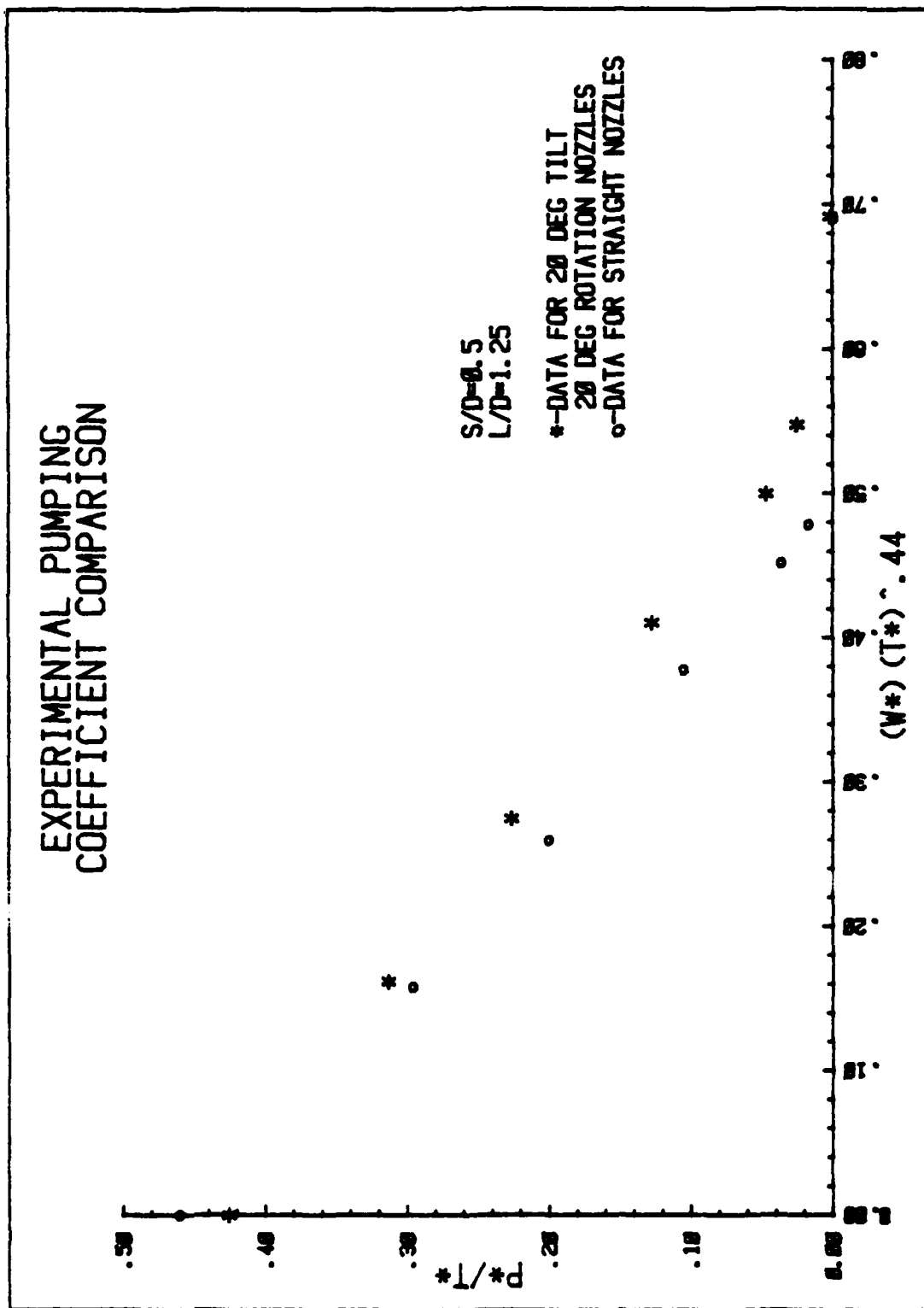


FIGURE 70

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

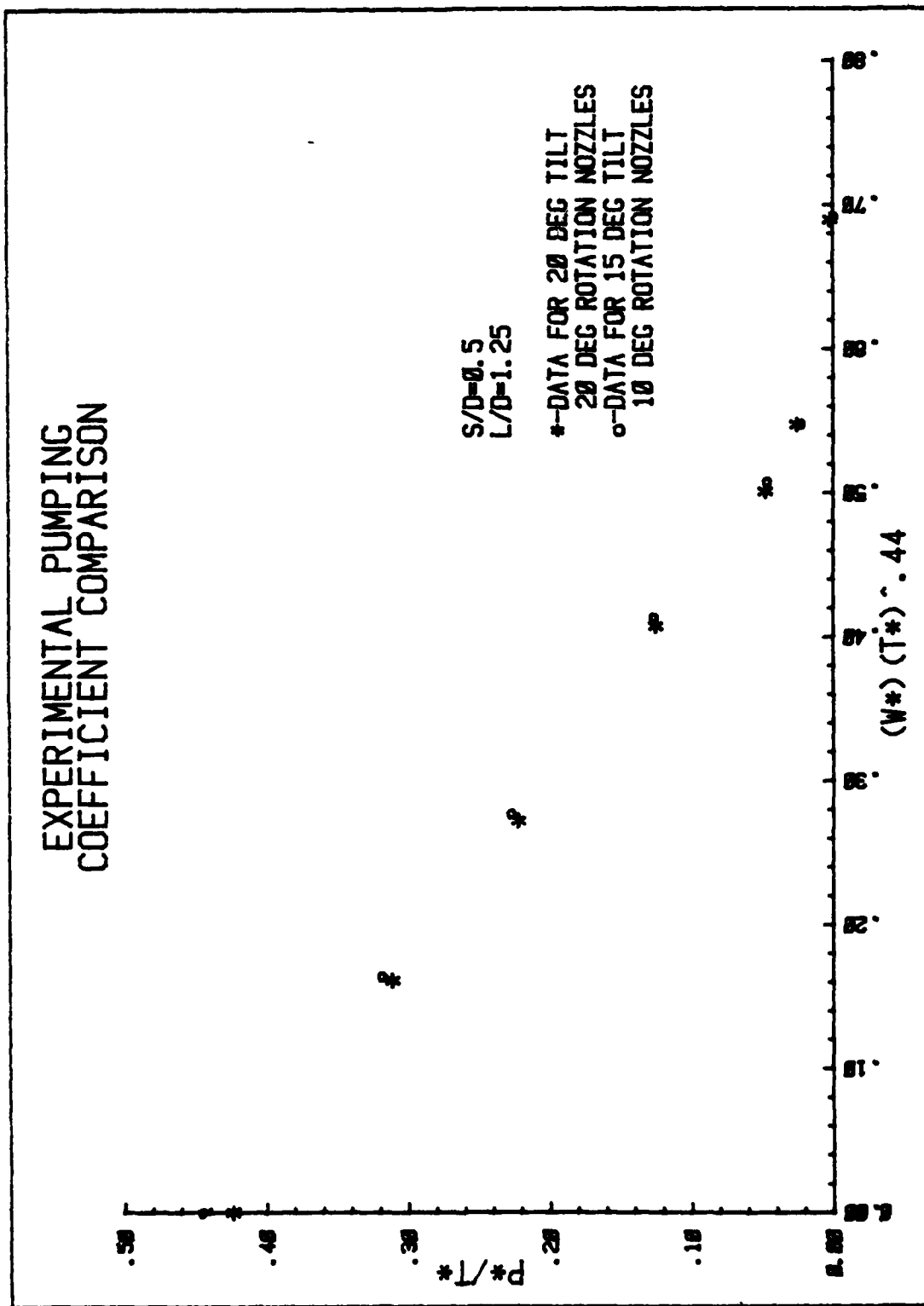


FIGURE 70.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

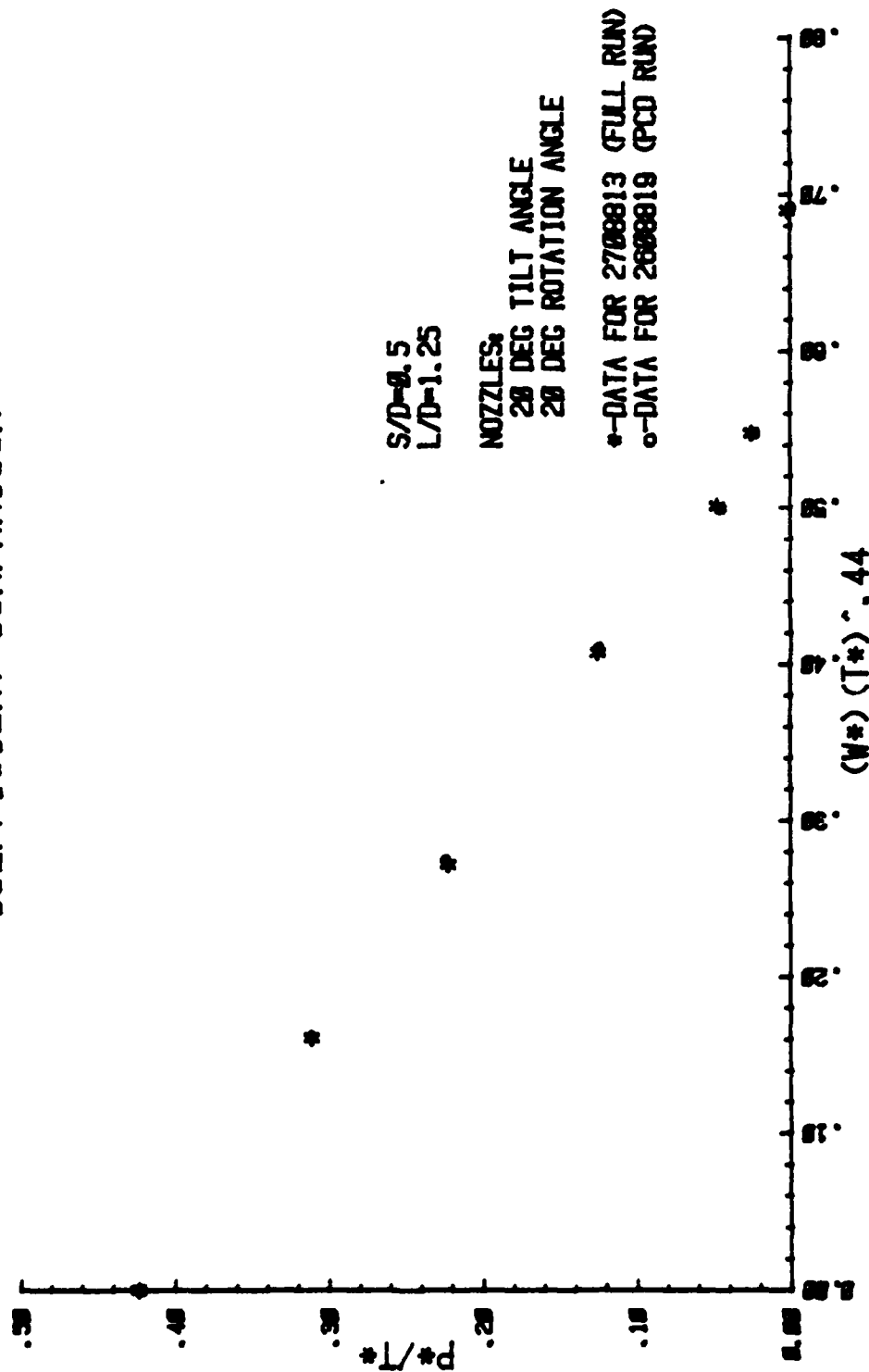


FIGURE 71

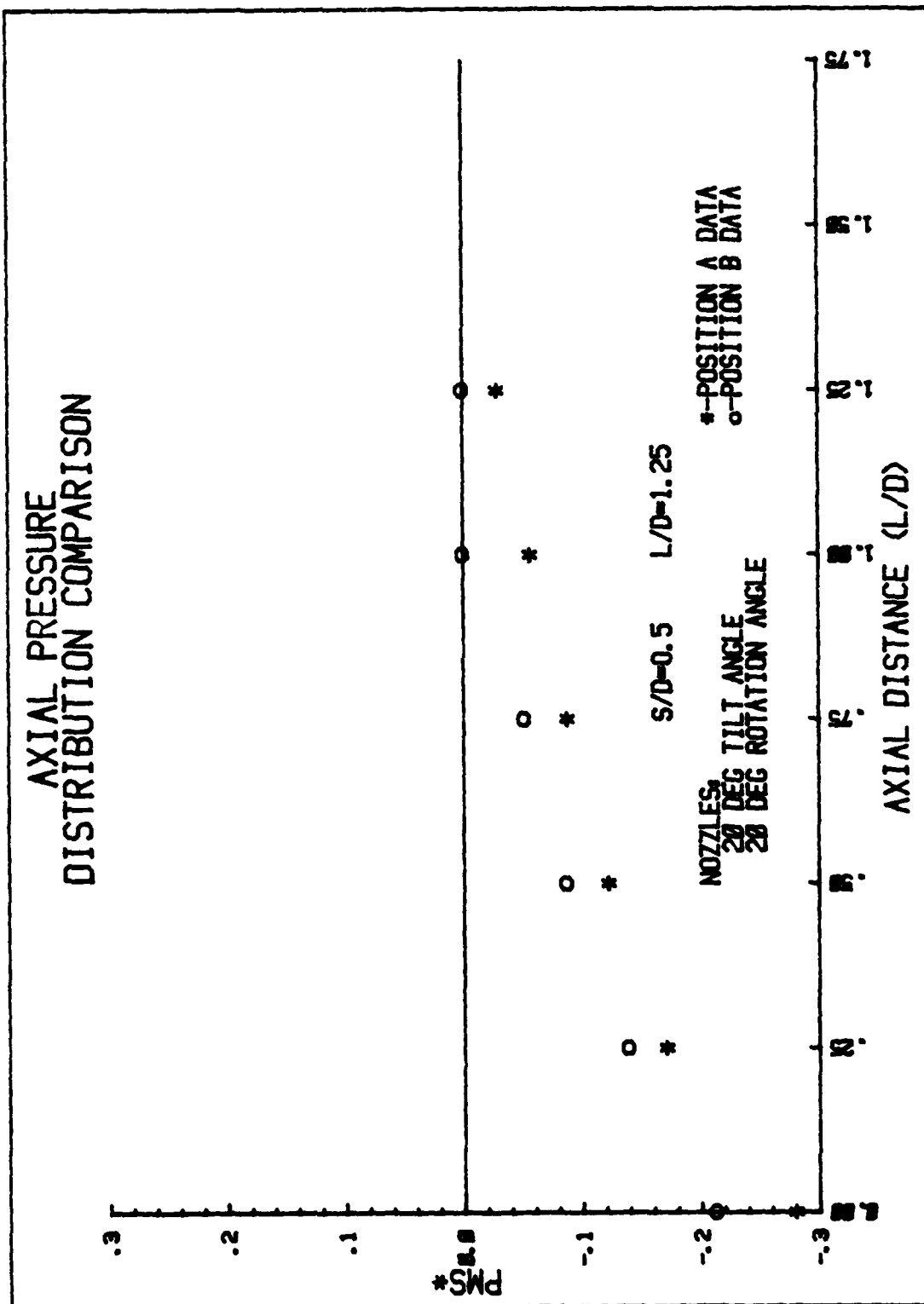


FIGURE 71.1

# BASE PLATE ROTATION ANGLE DISTRIBUTION COMPARISON

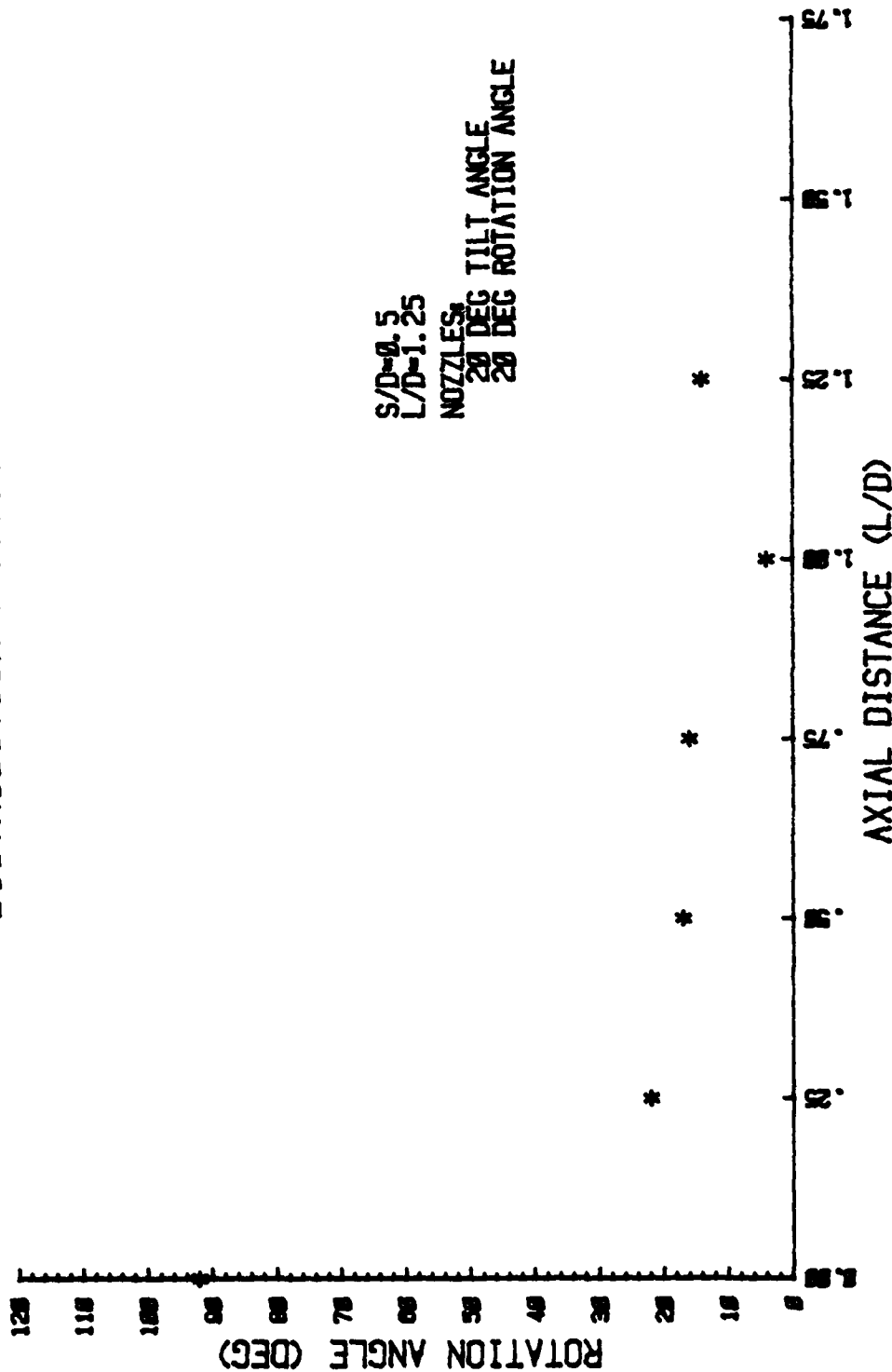


FIGURE 71.2



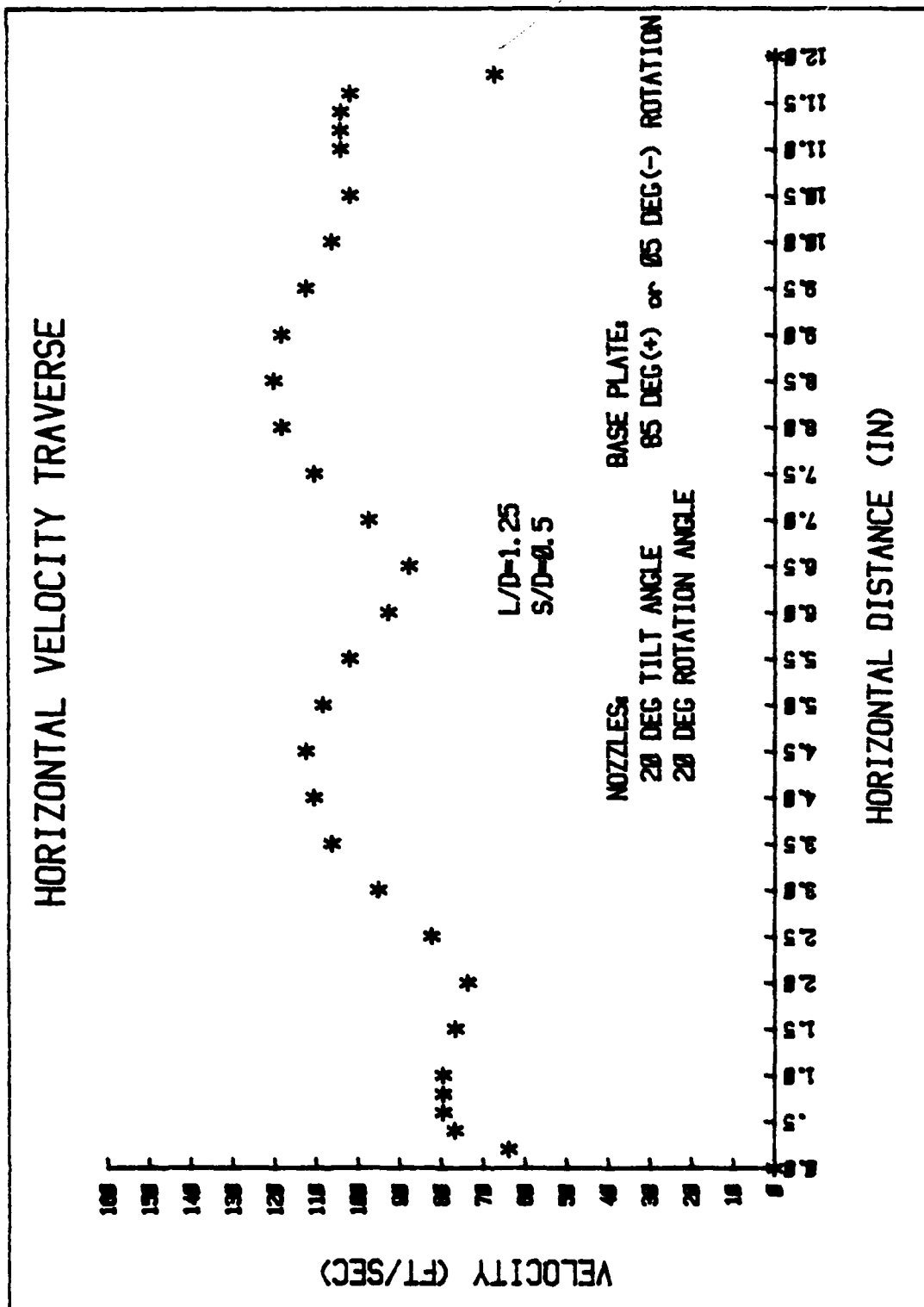


FIGURE 71.3

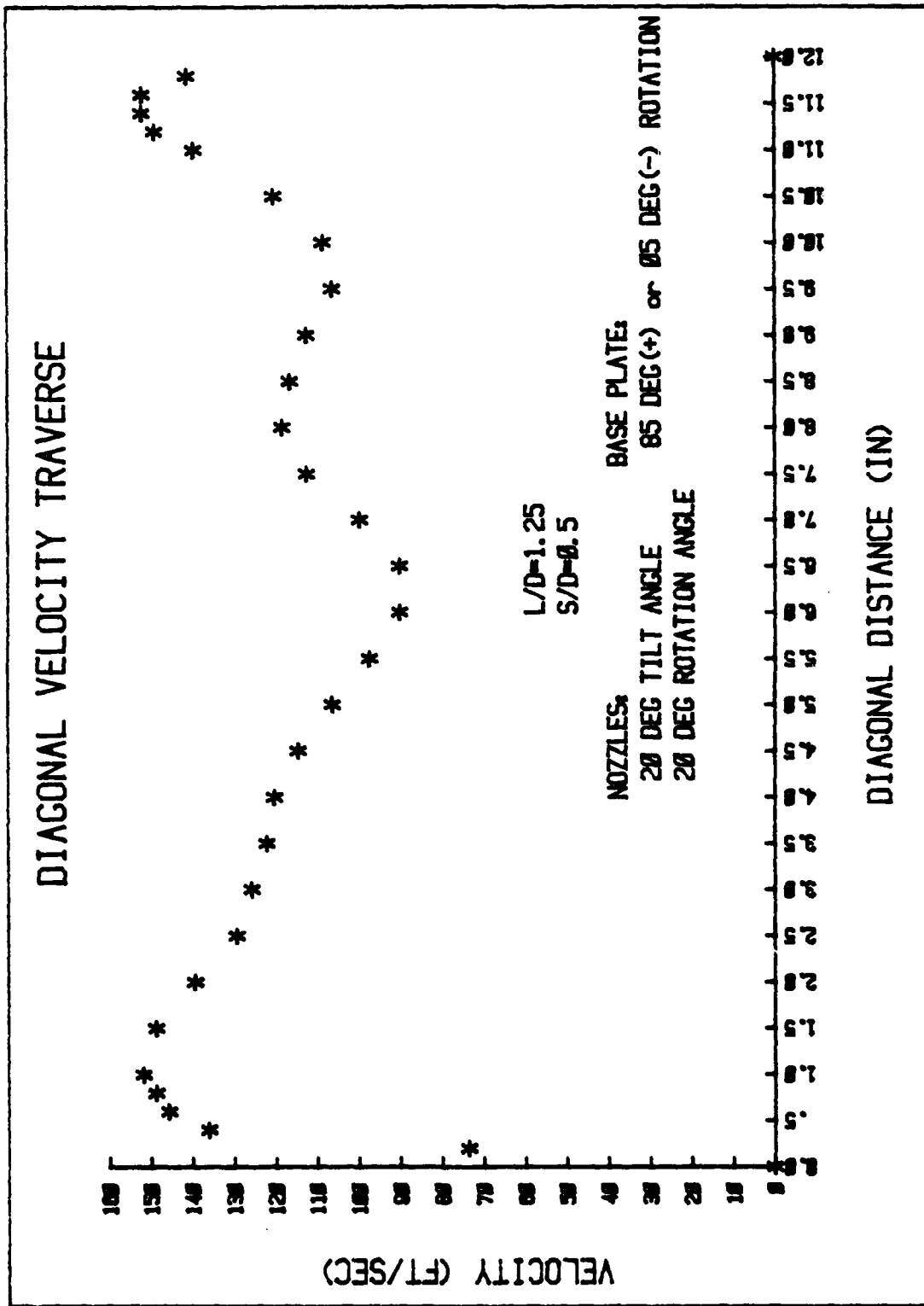


FIGURE 71.4

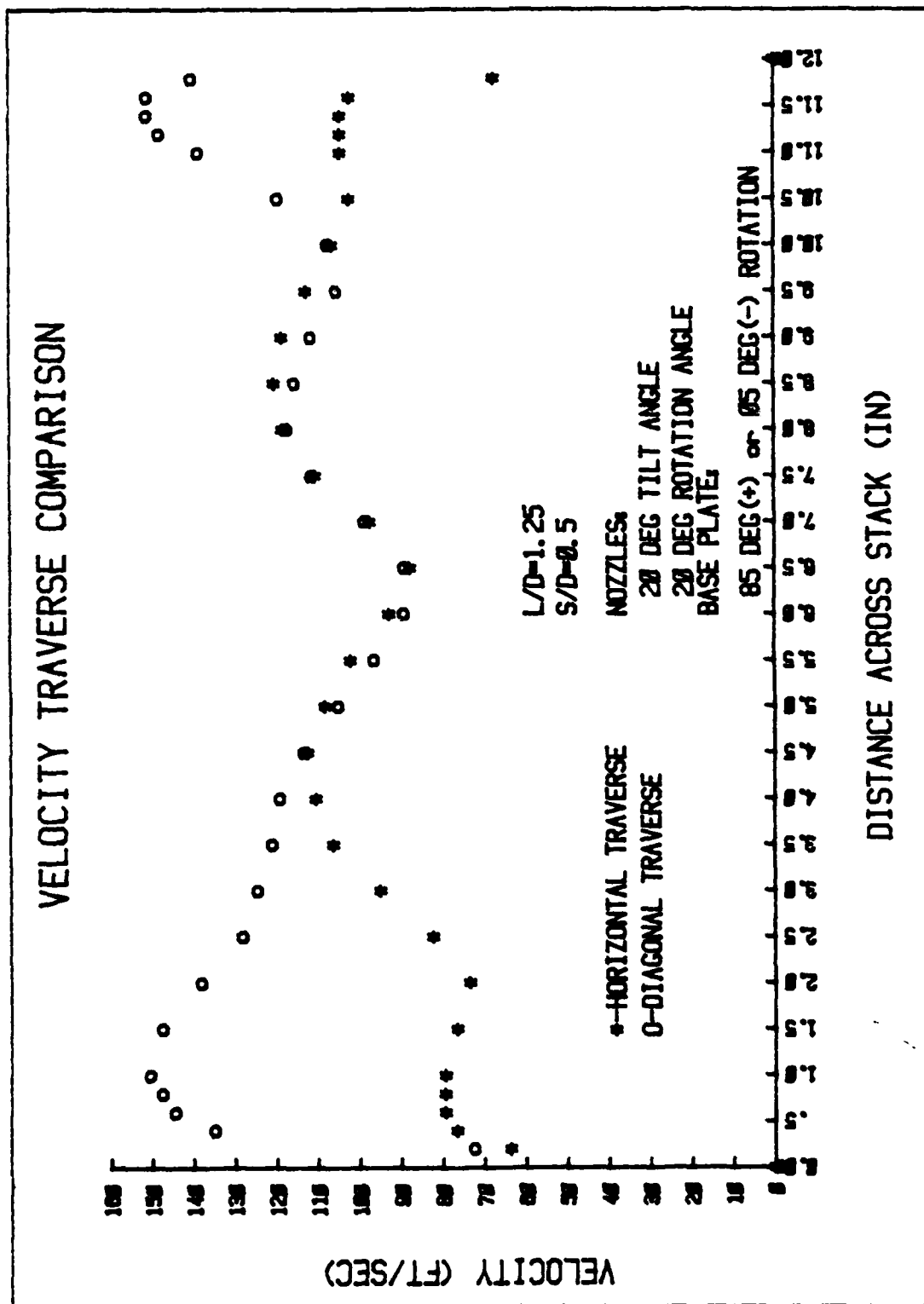


FIGURE 71.5

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

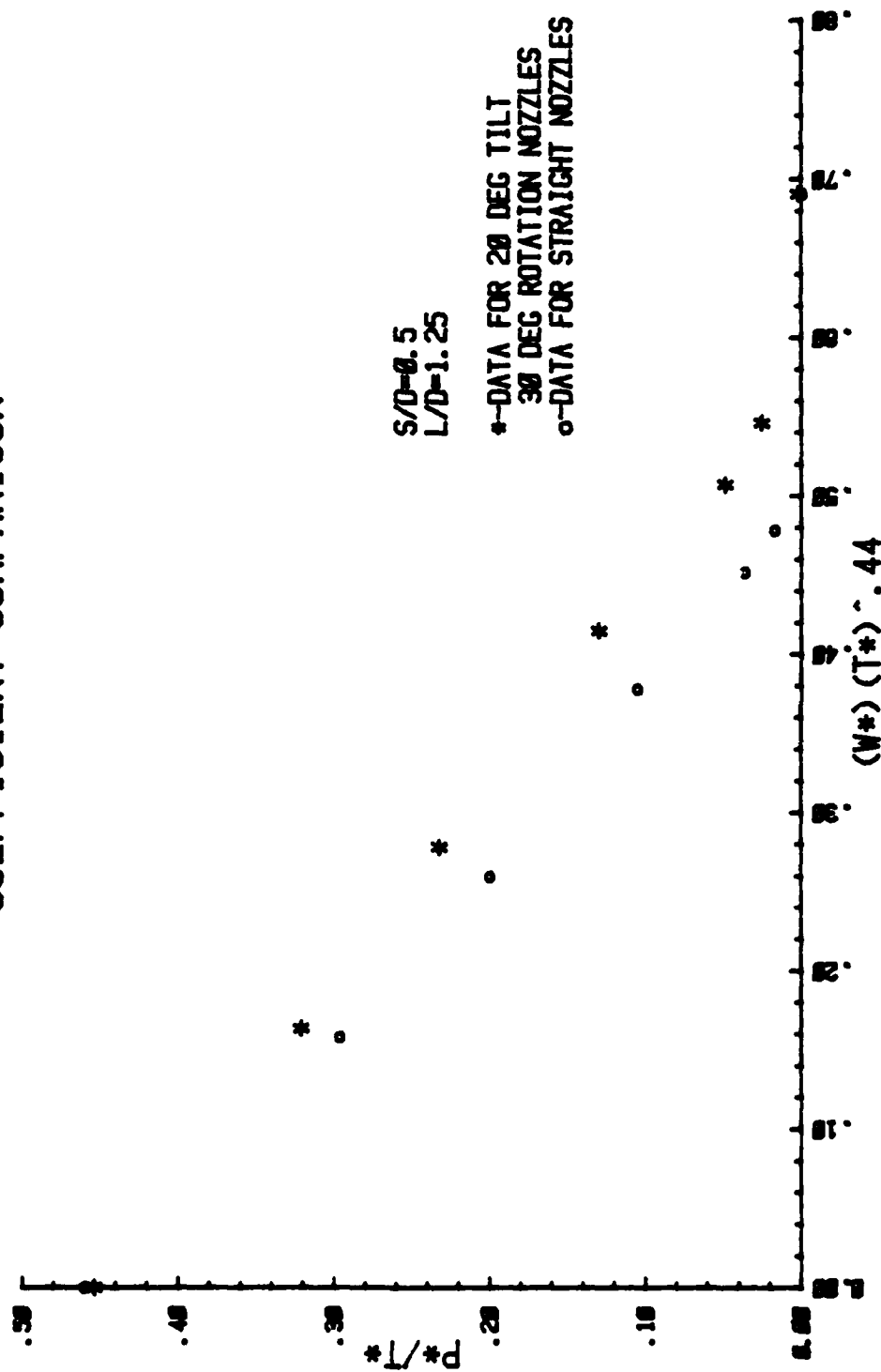


FIGURE 72

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

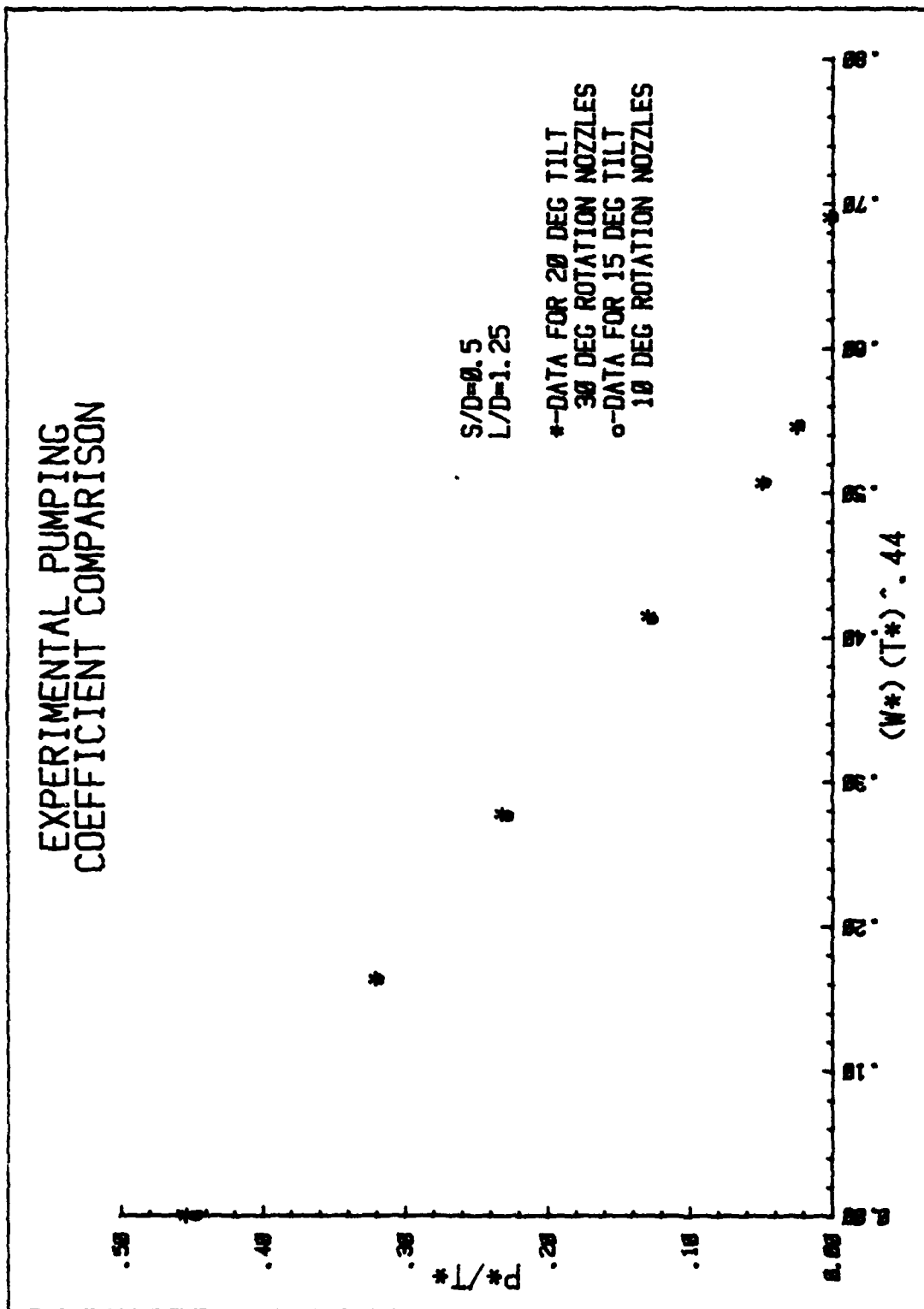


FIGURE 72.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

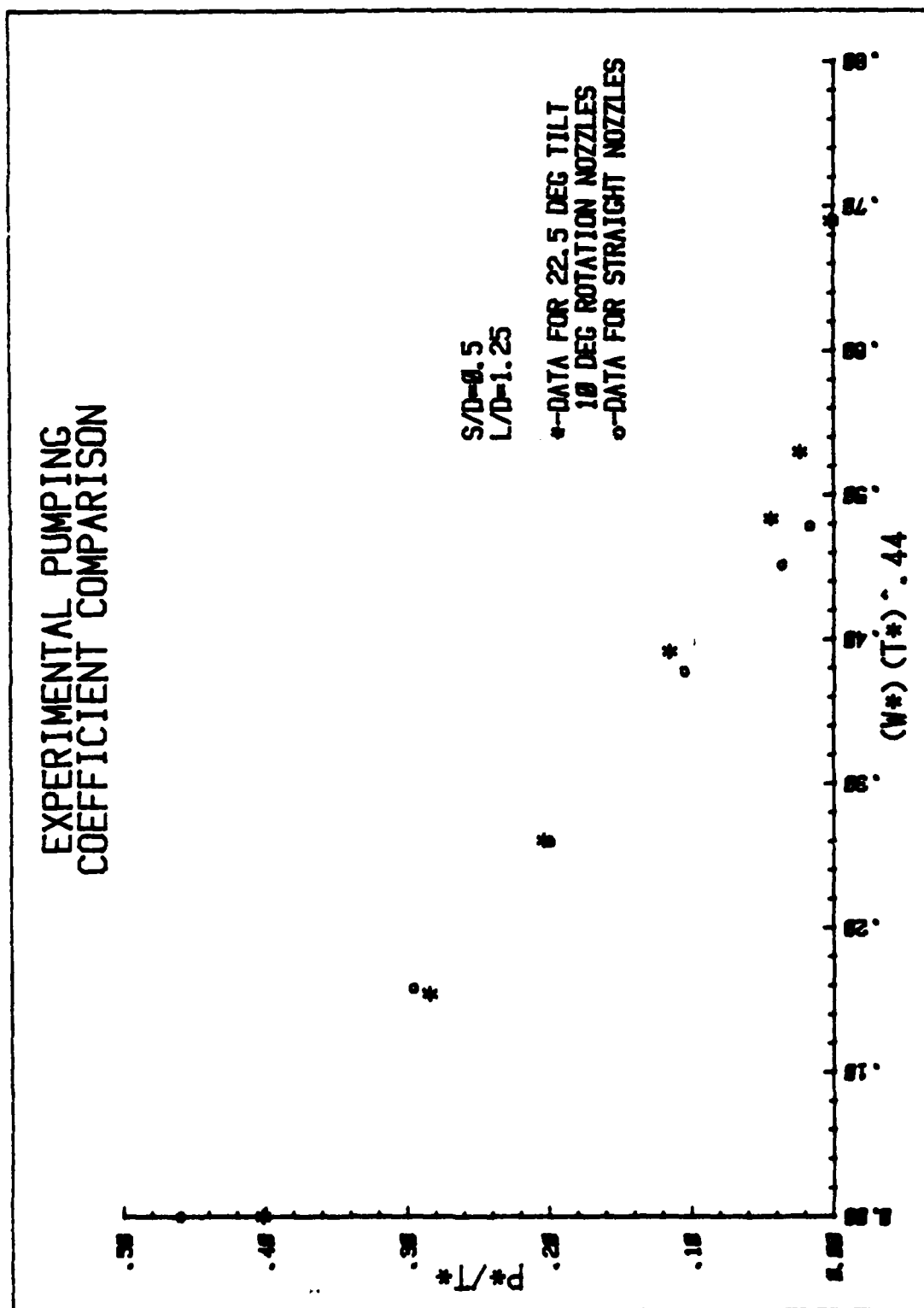


FIGURE 73

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

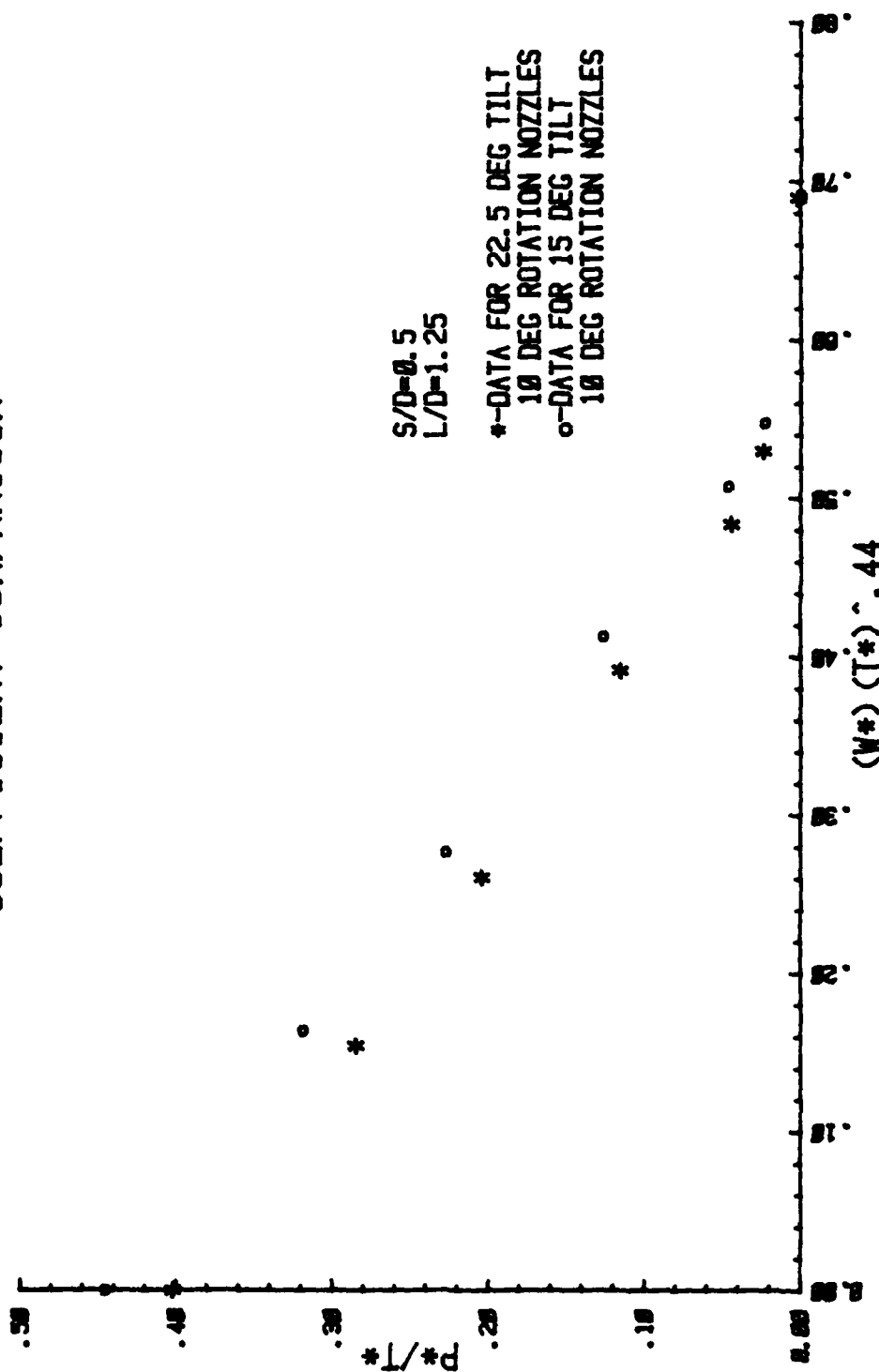


FIGURE 73.1

# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON

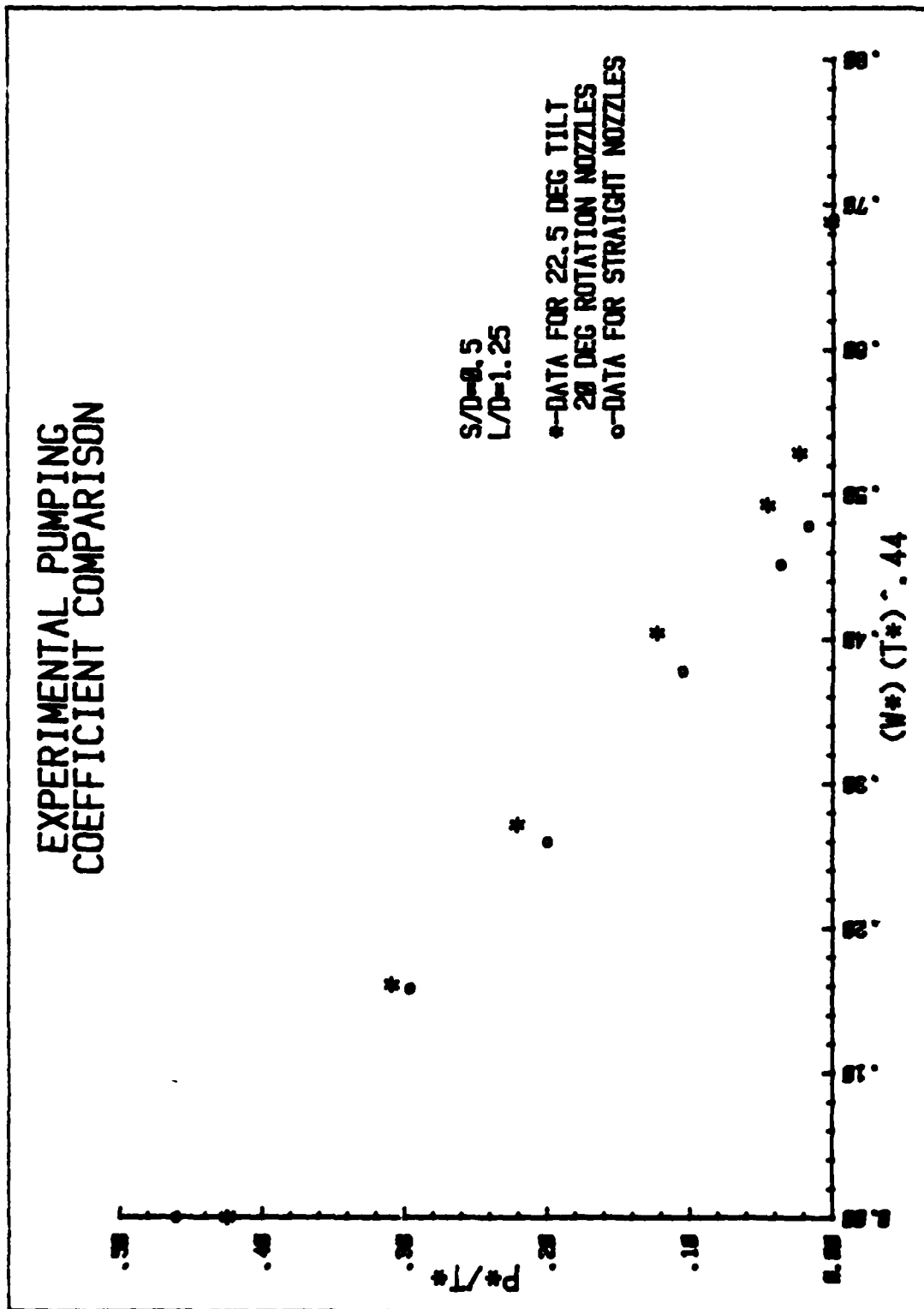
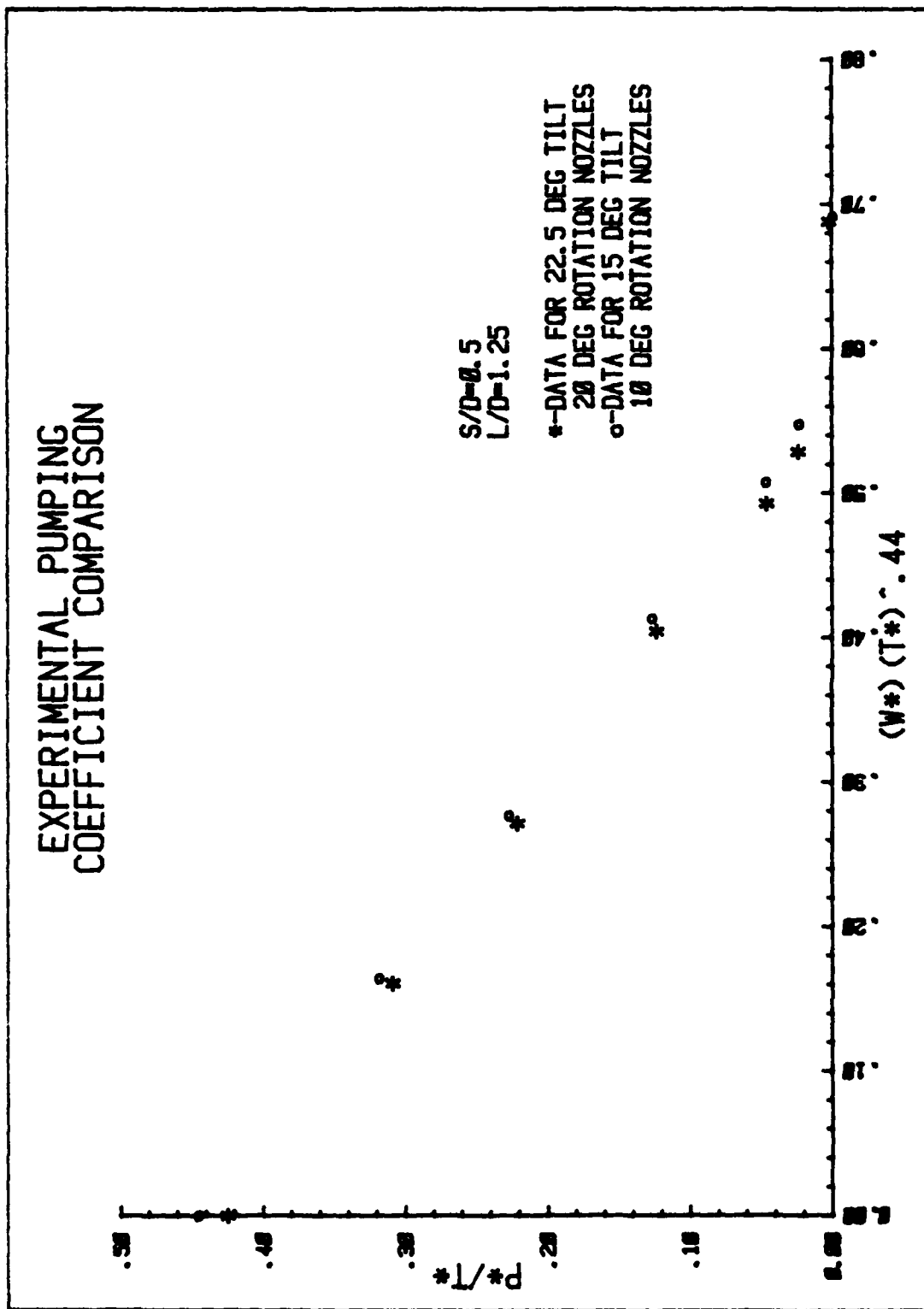


FIGURE 74



# EXPERIMENTAL PUMPING COEFFICIENT COMPARISON



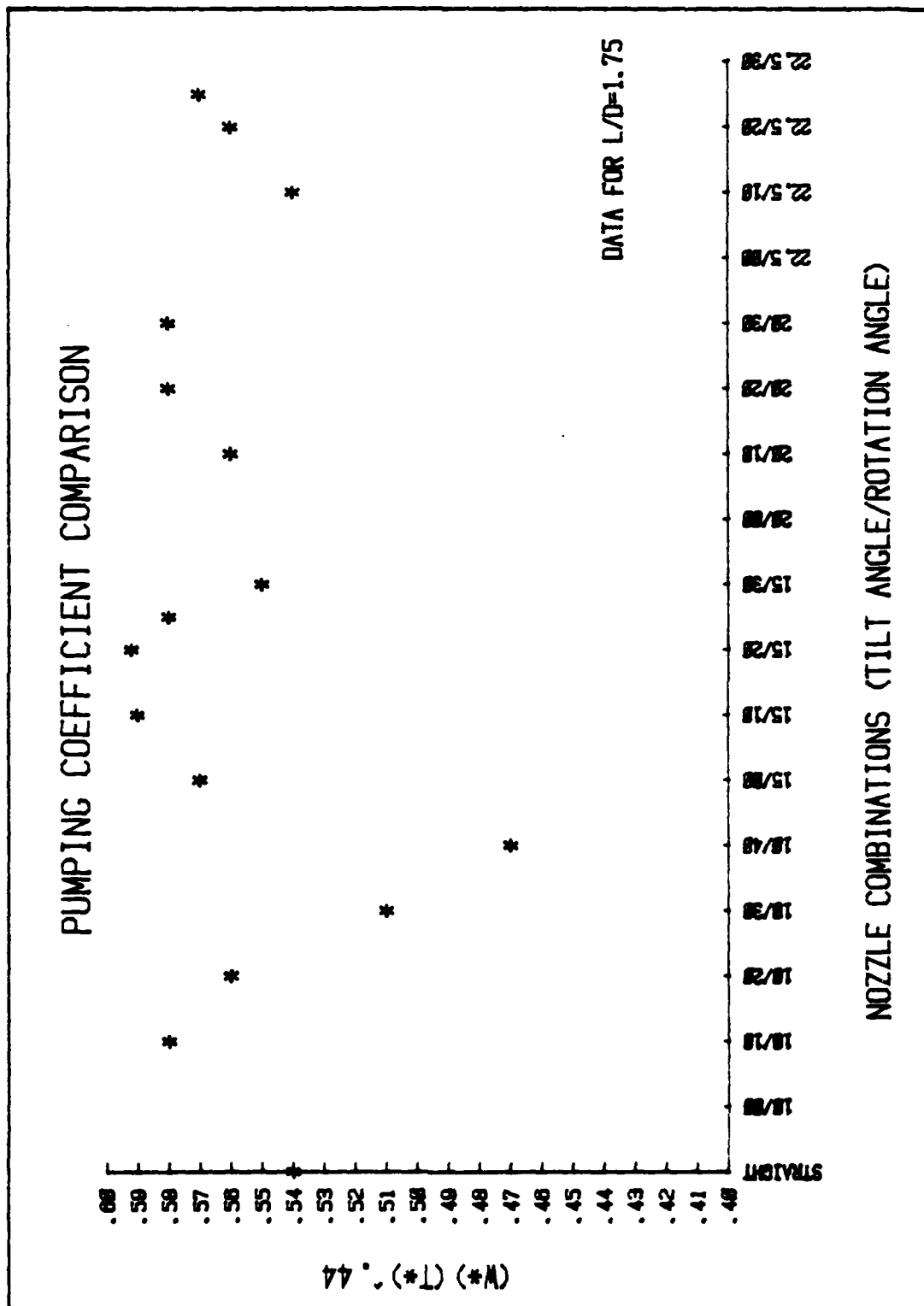


FIGURE 75

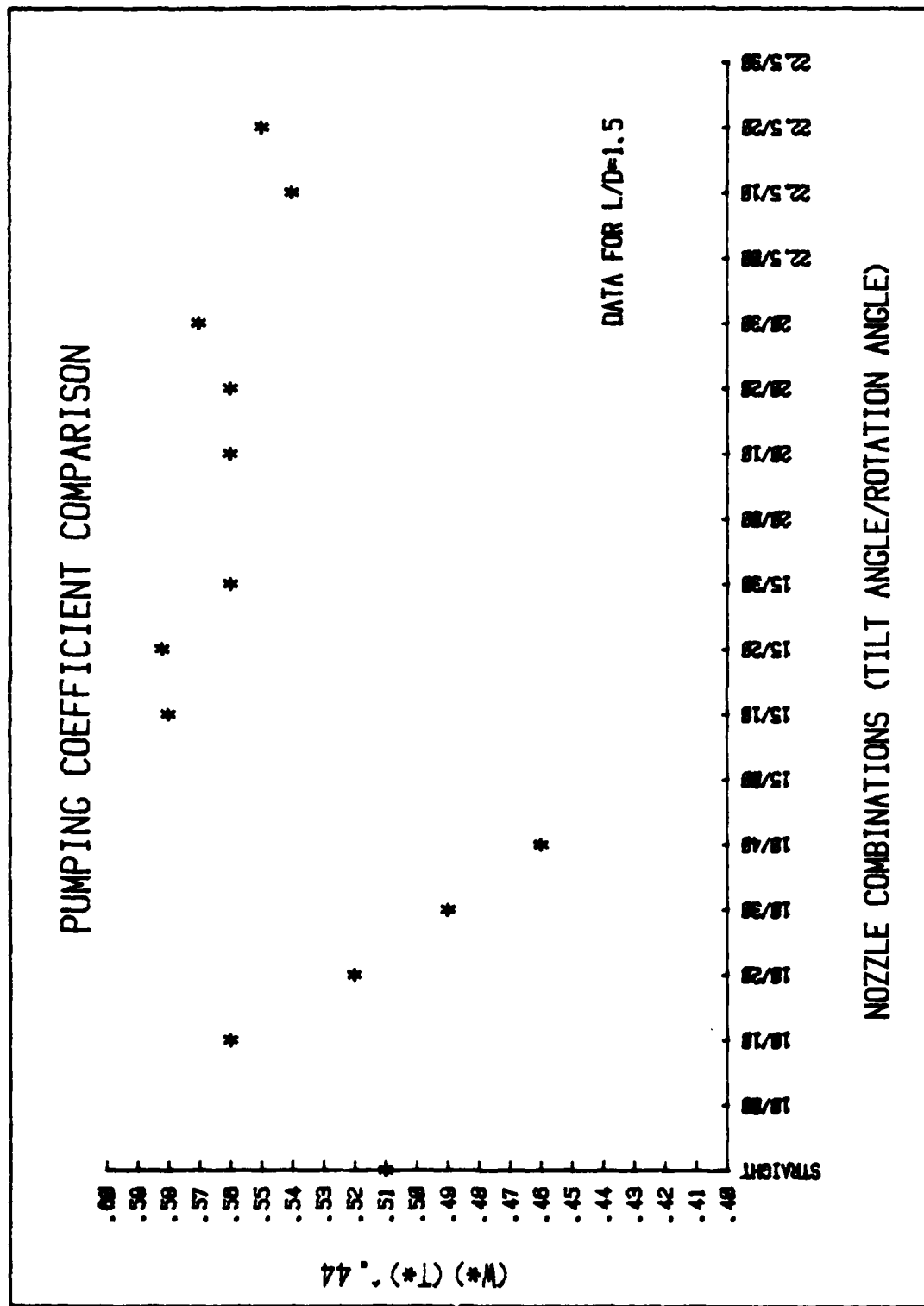


FIGURE 78

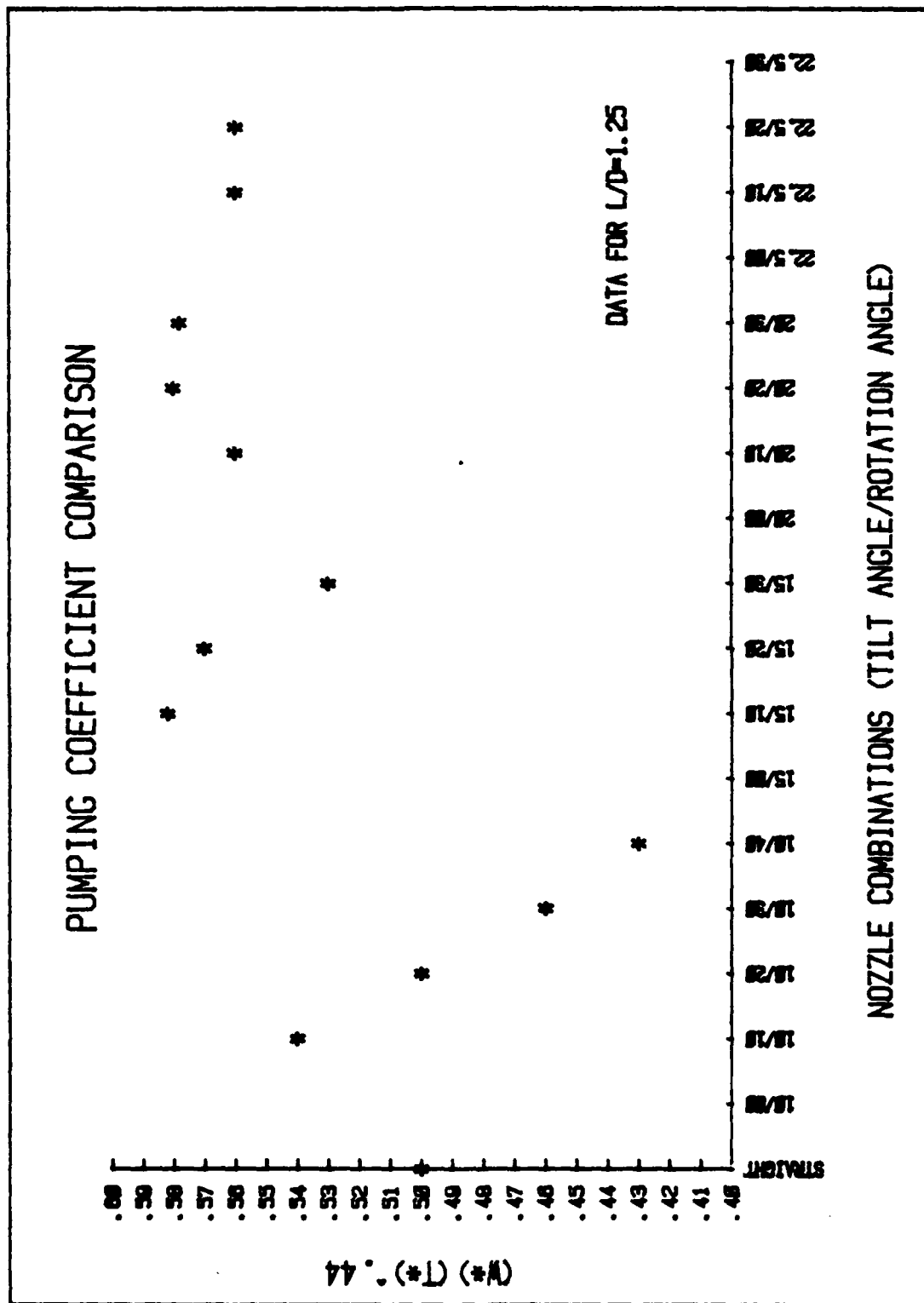


FIGURE 77

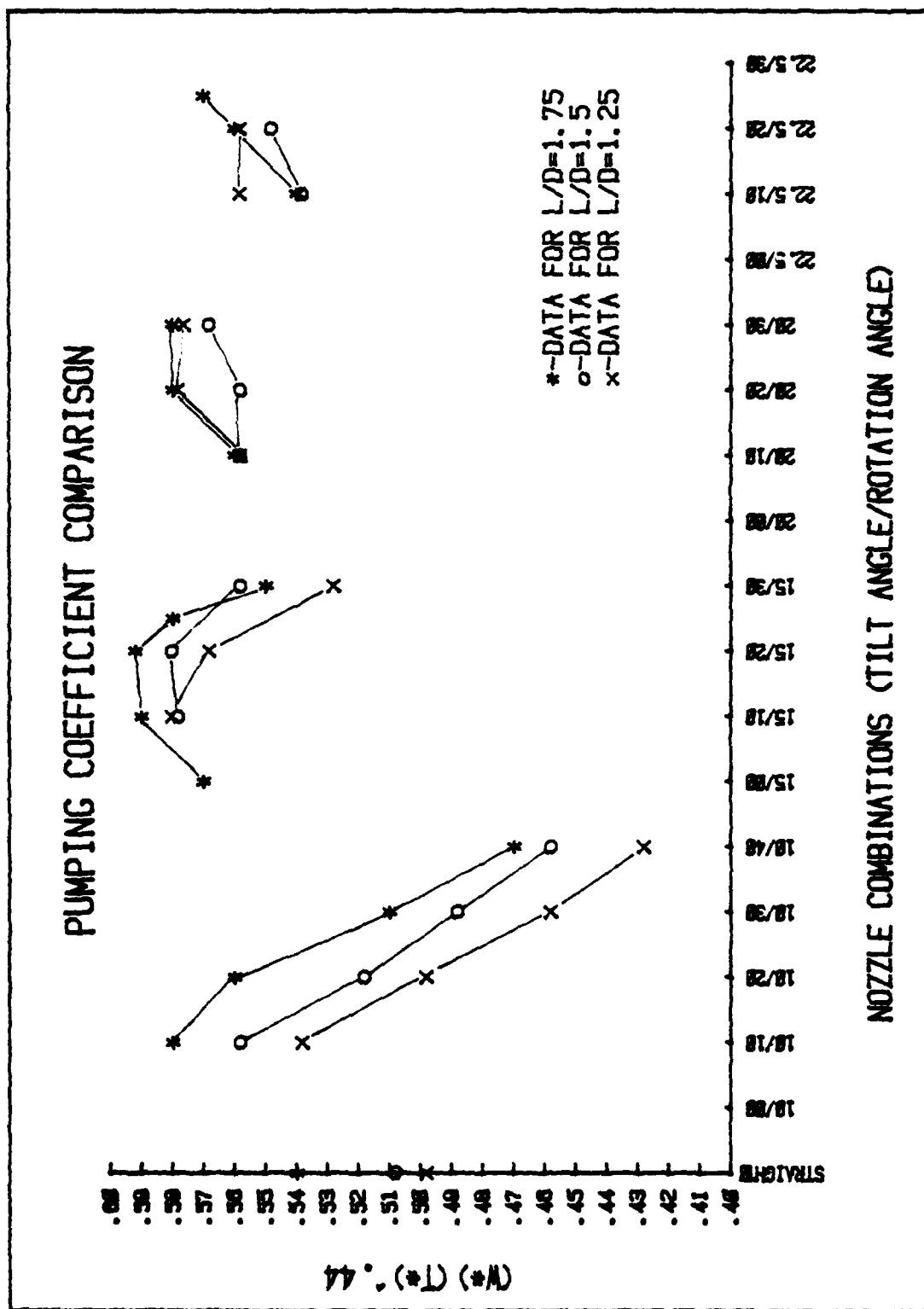


FIGURE 78

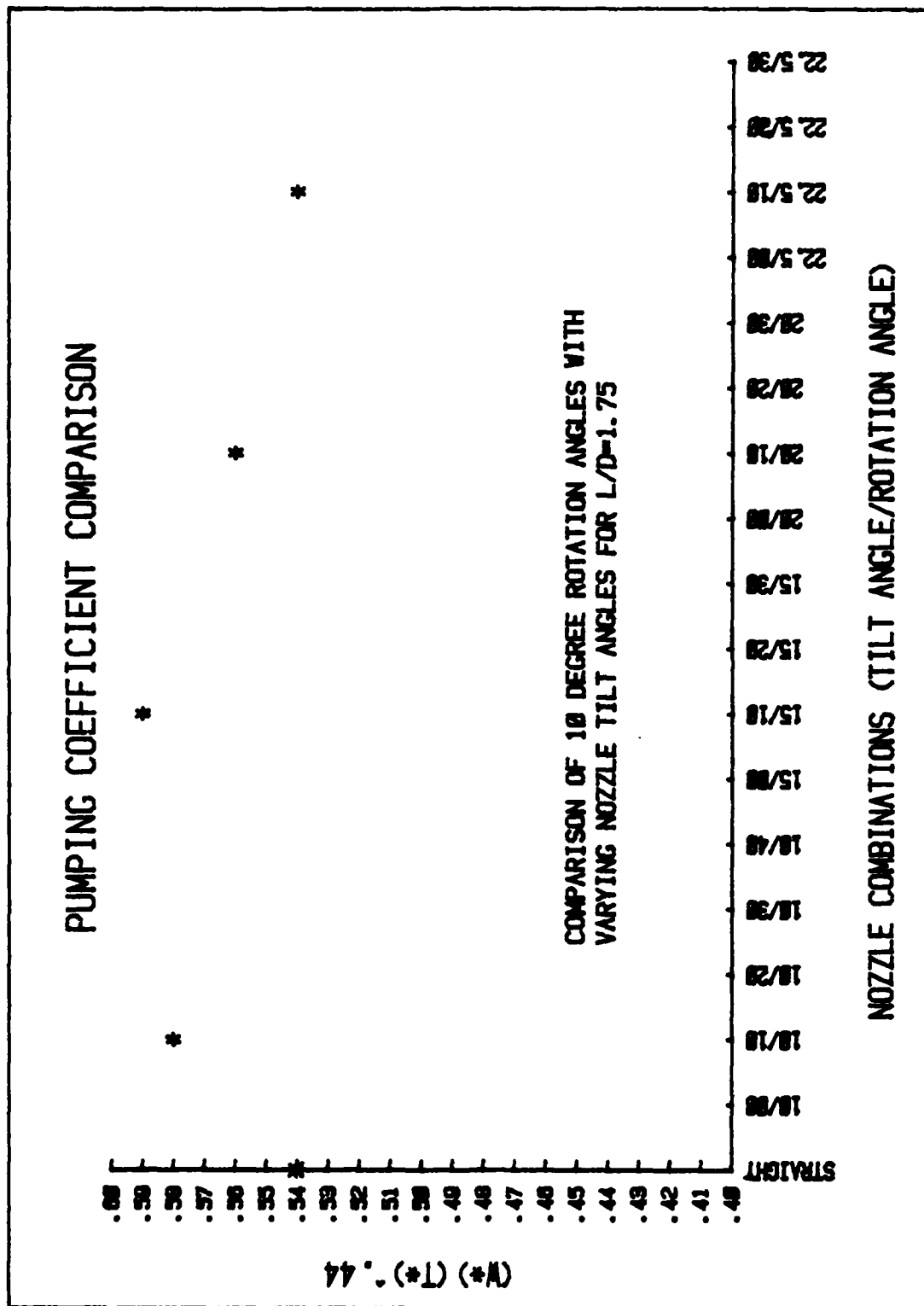


FIGURE 79

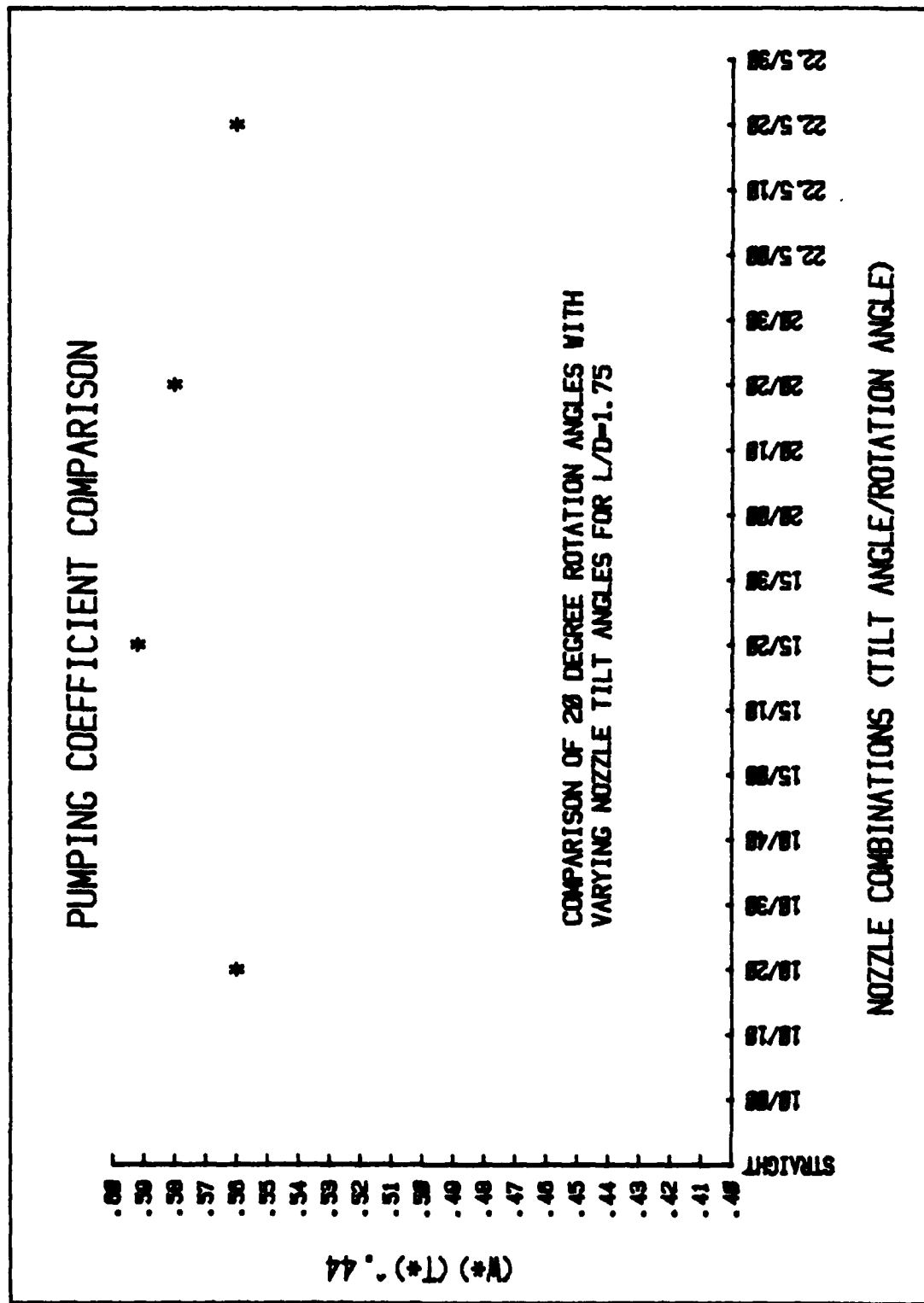


FIGURE 79.1

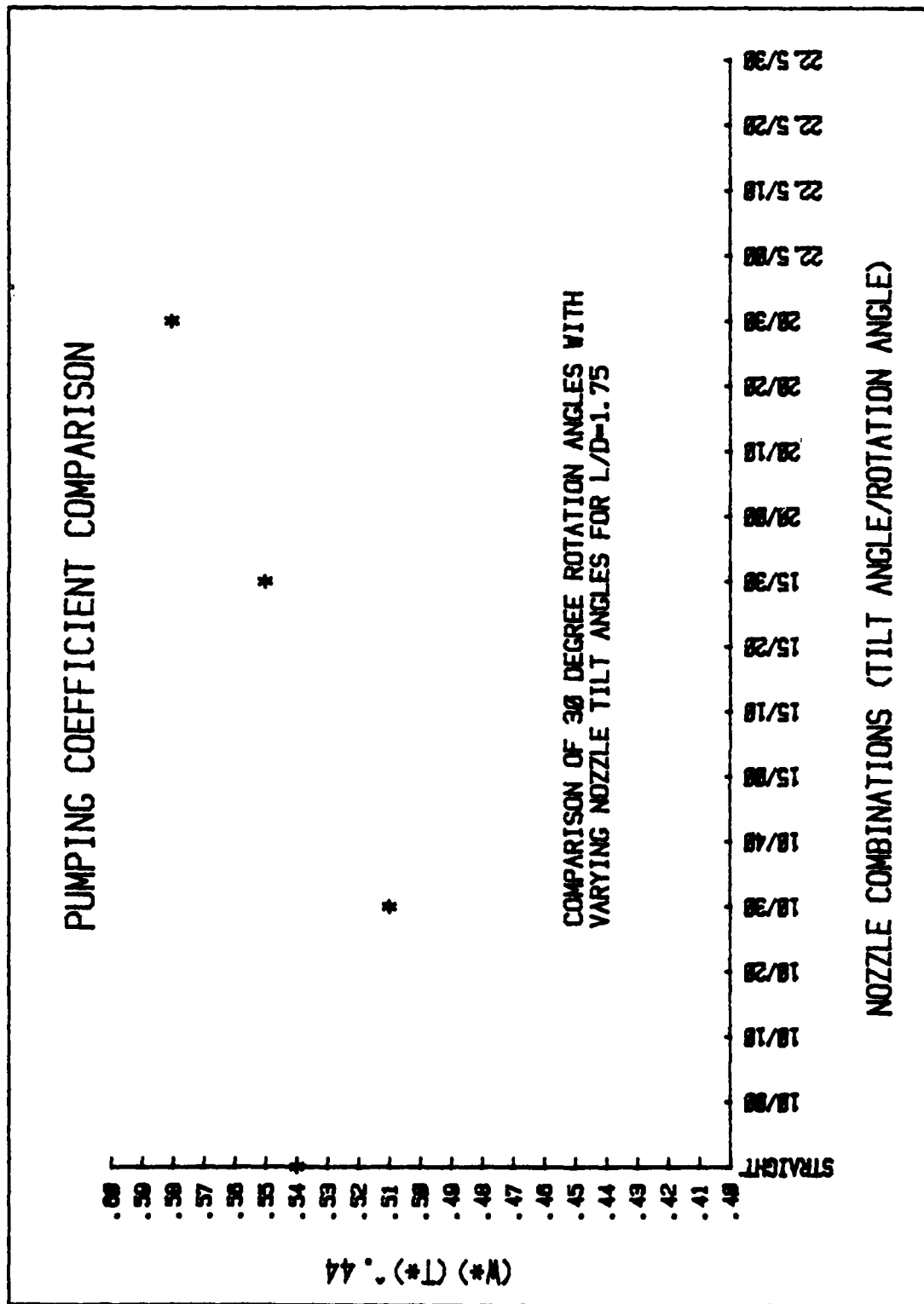


FIGURE 79.2



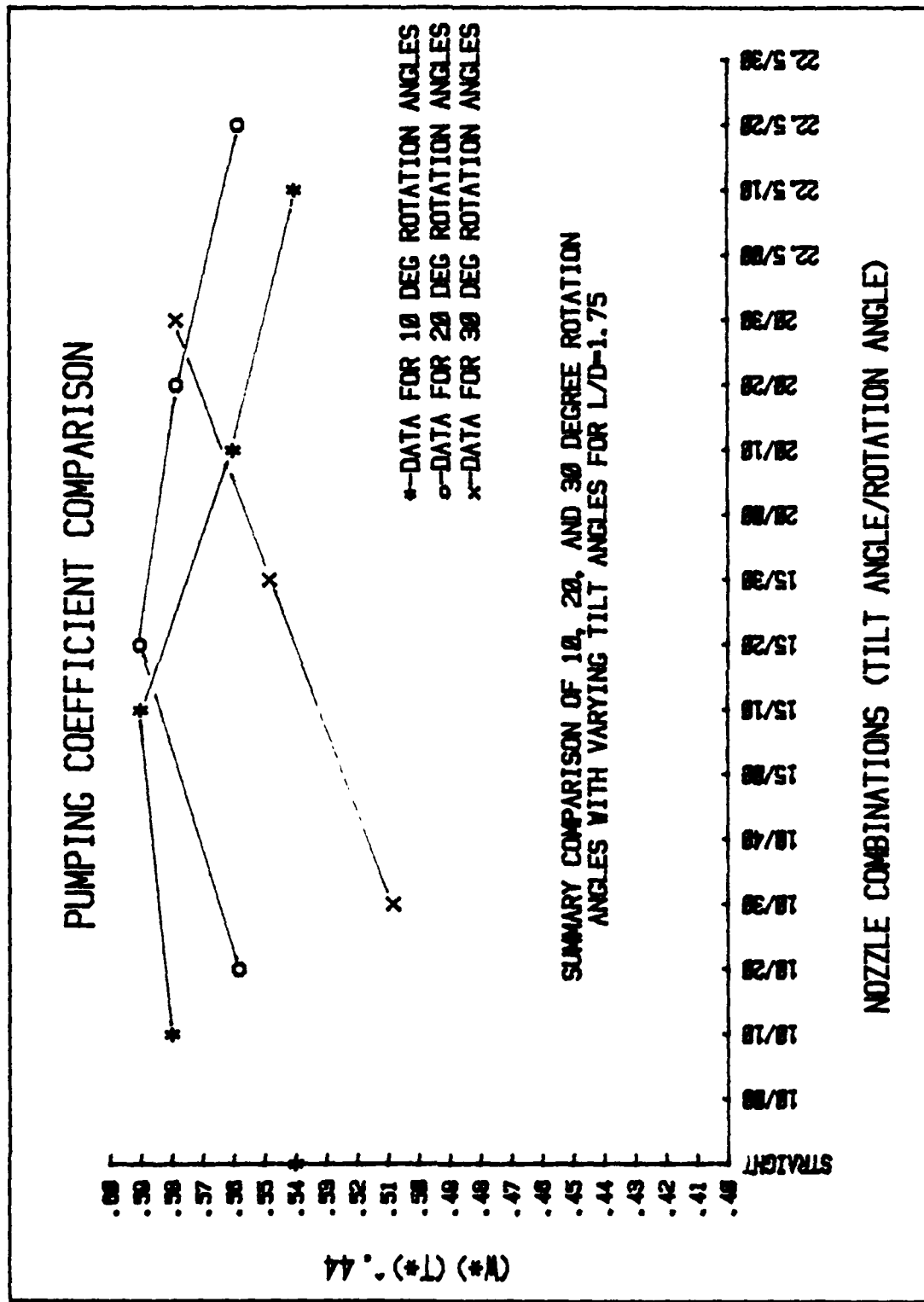


FIGURE 78.3

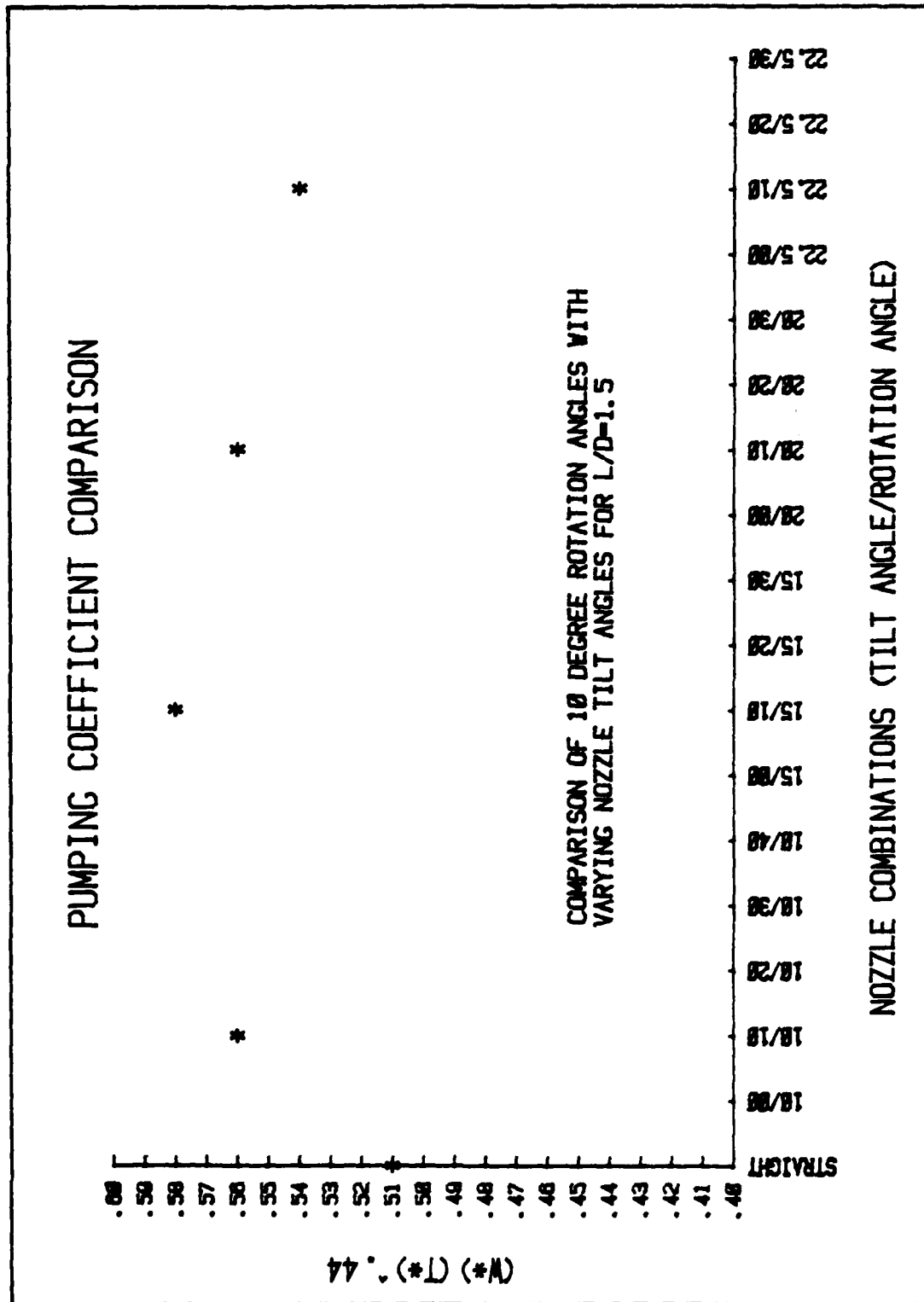


FIGURE 80

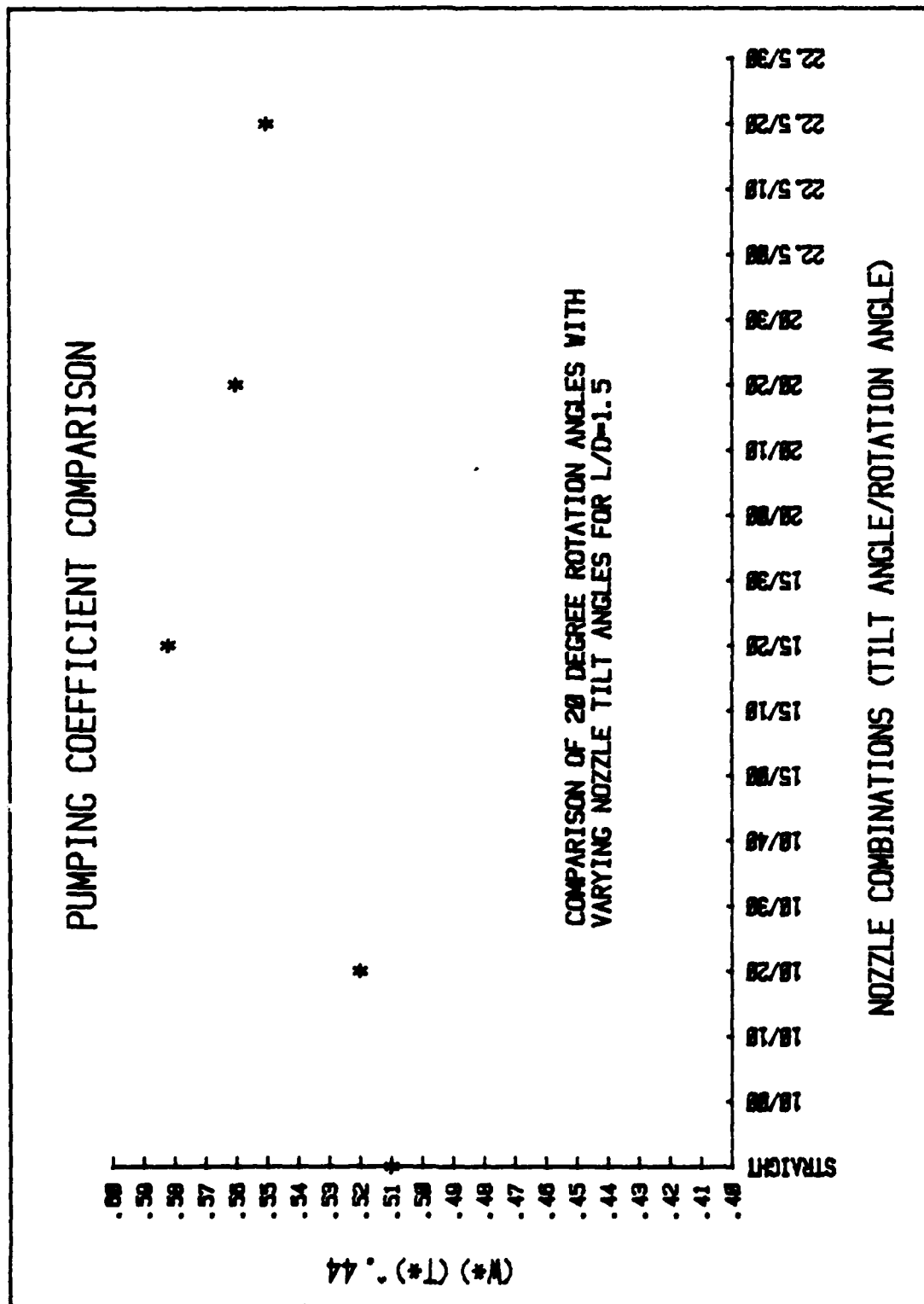


FIGURE 80.1

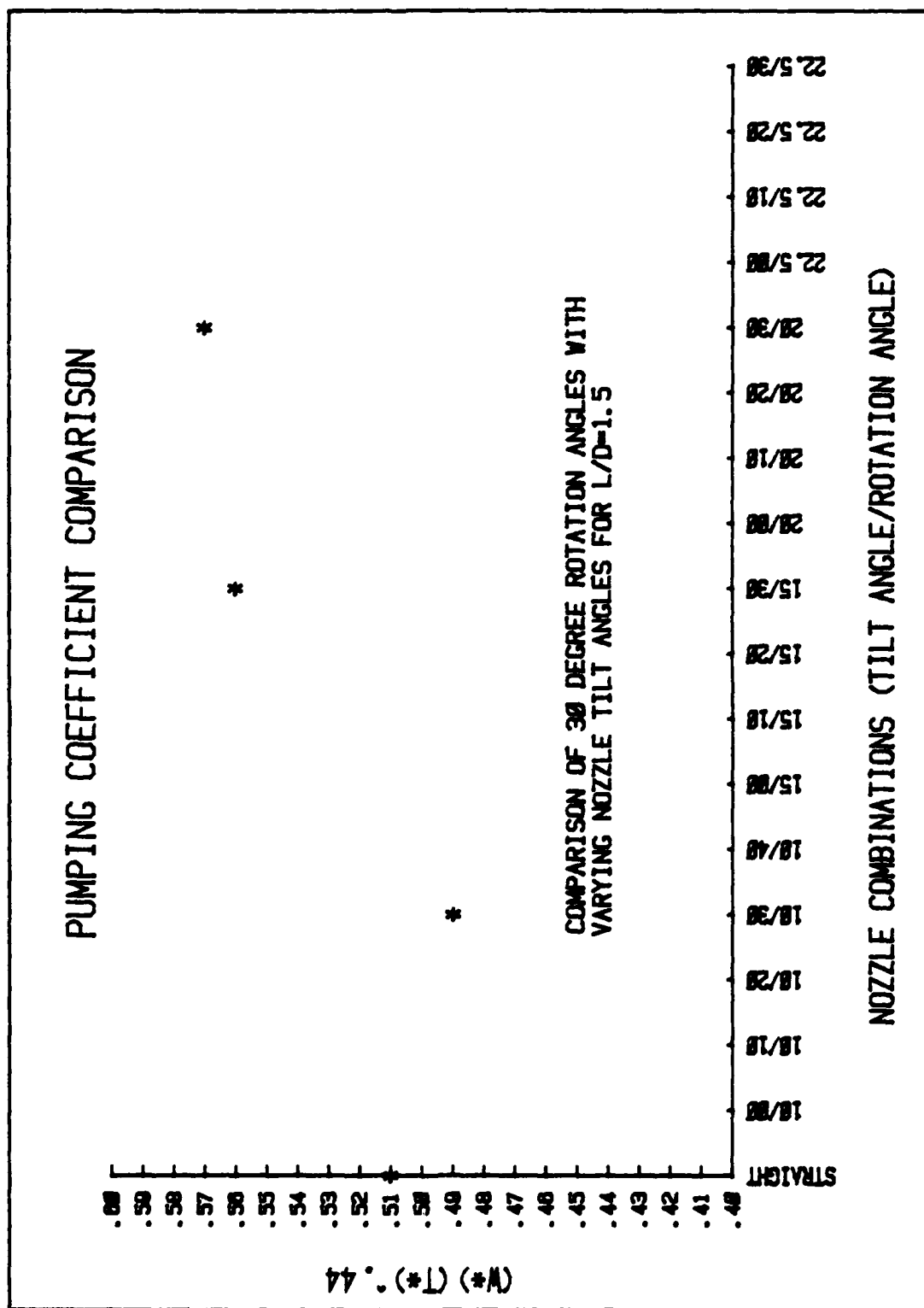
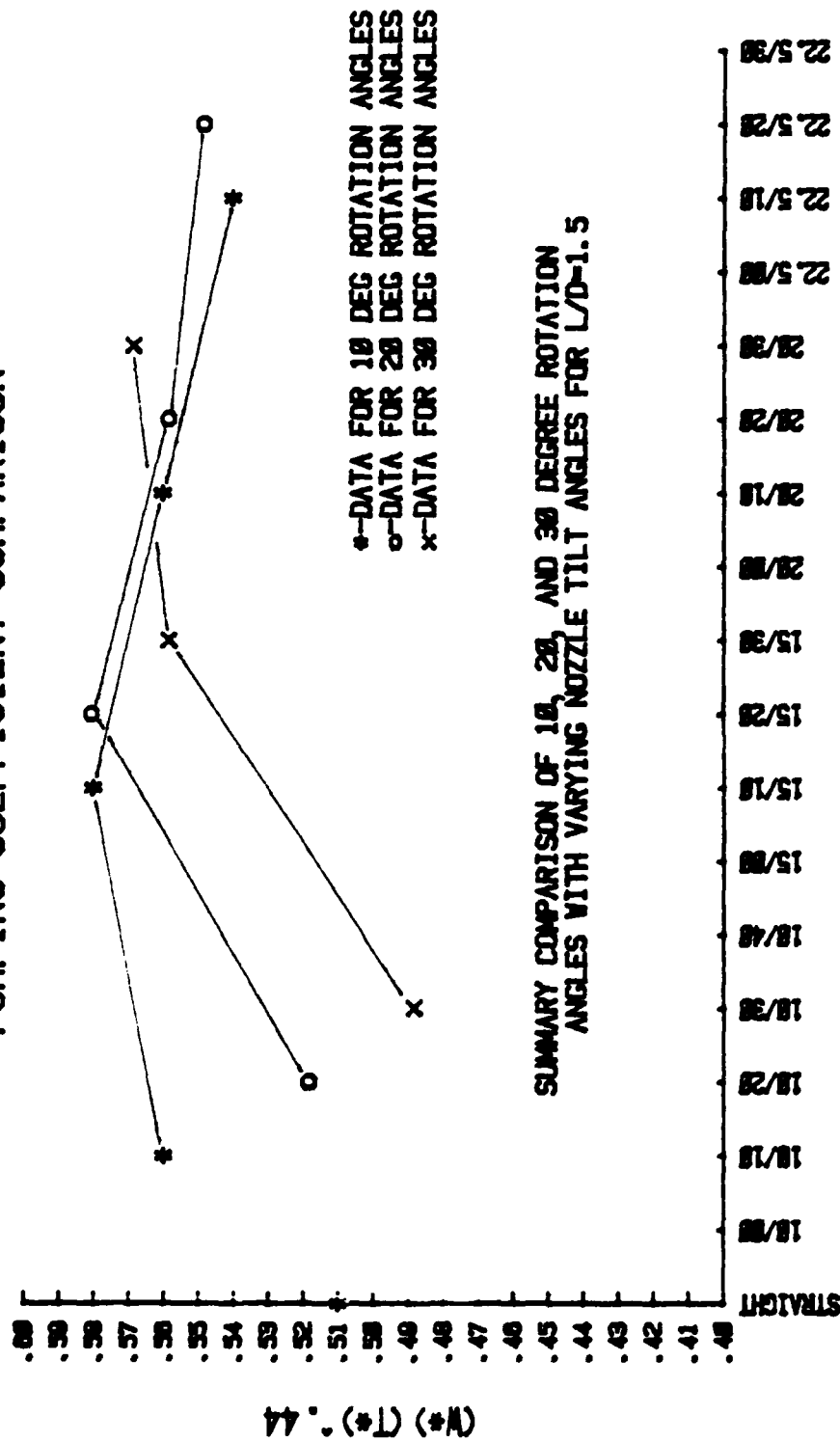


FIGURE 80.2

# PUMPING COEFFICIENT COMPARISON



SUMMARY COMPARISON OF 10, 20, AND 30 DEGREE ROTATION ANGLES WITH VARYING NOZZLE TILT ANGLES FOR L/D=1.5

NOZZLE COMBINATIONS (TILT ANGLE/ROTATION ANGLE)

FIGURE 80.3

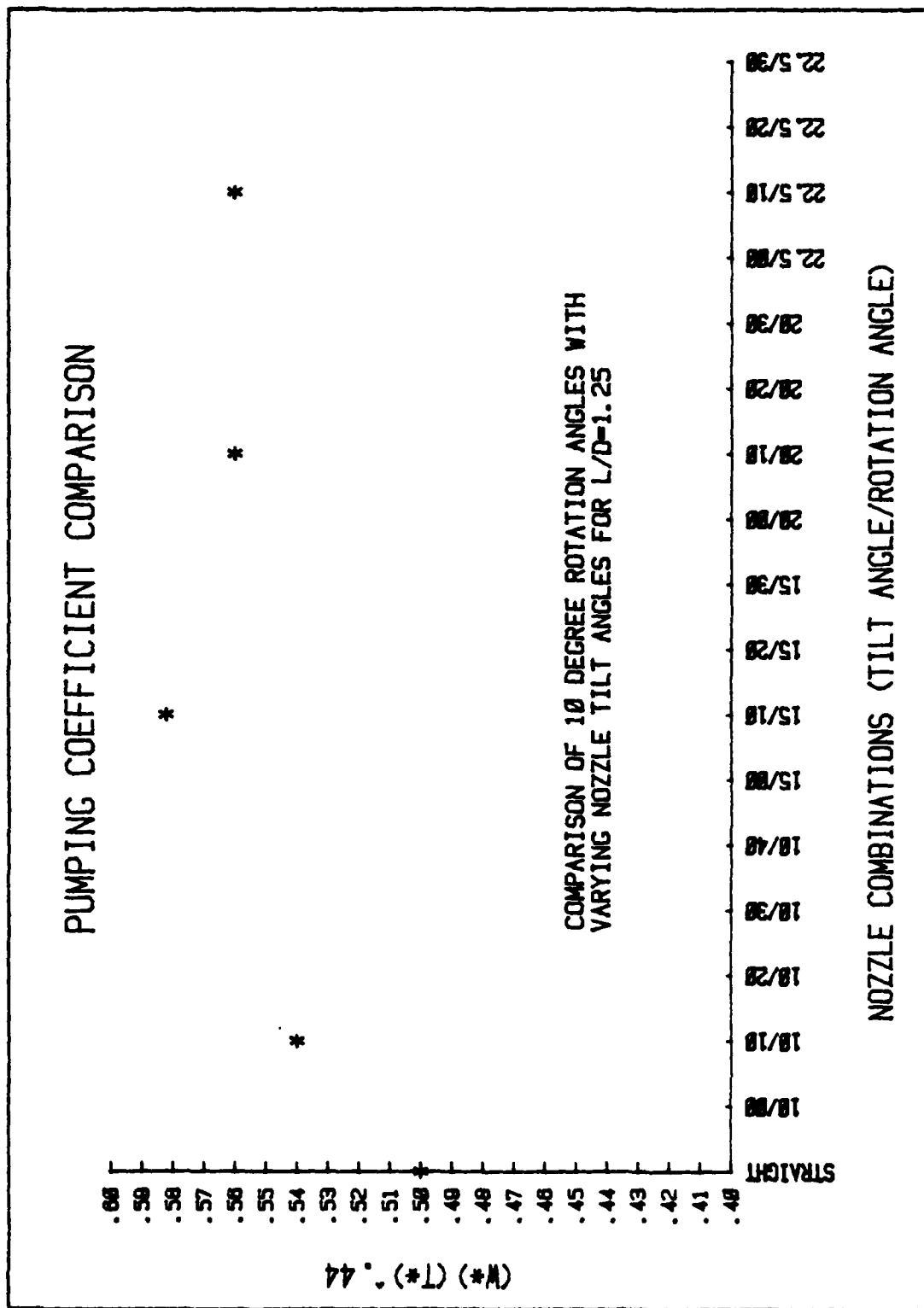


FIGURE 81

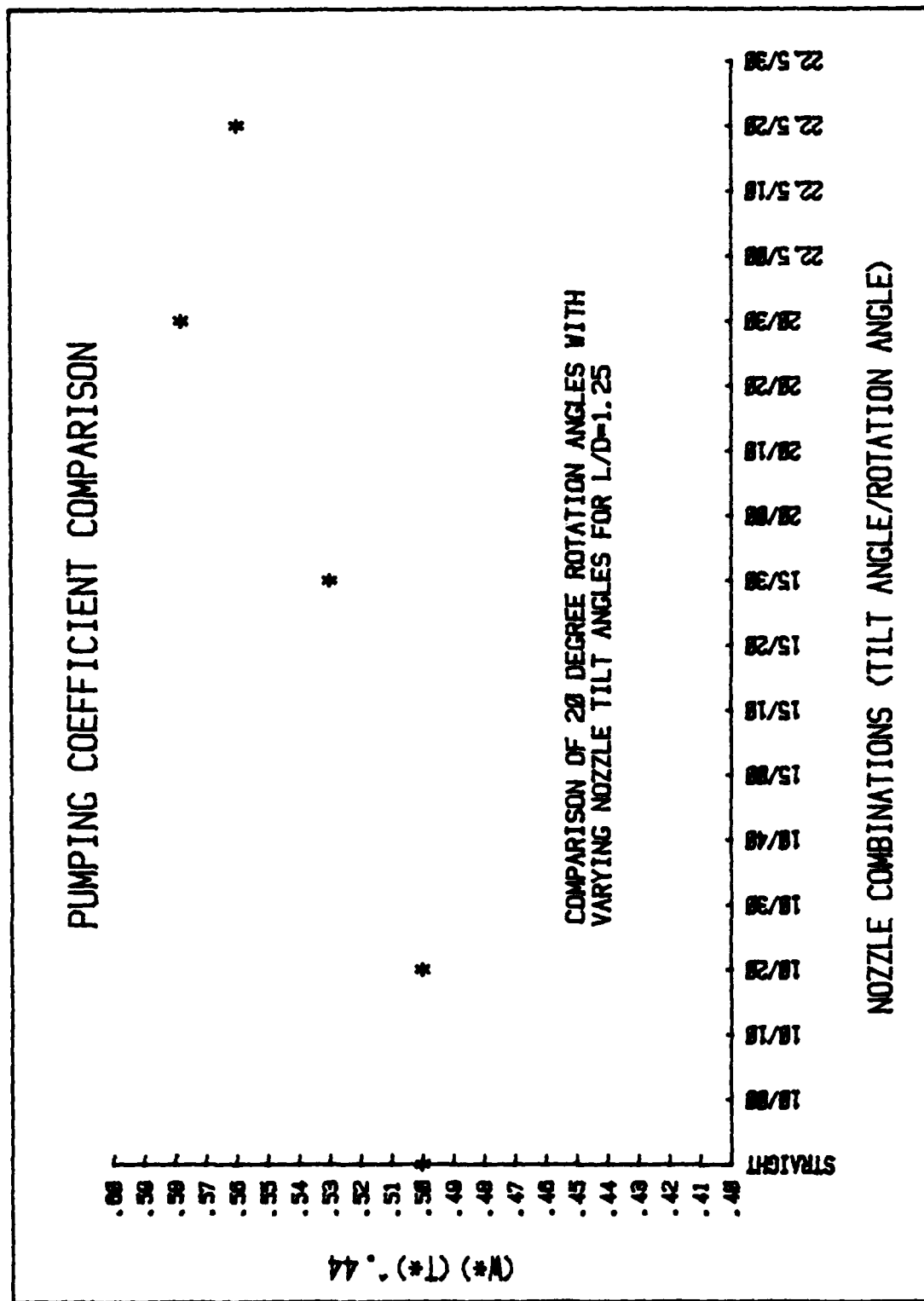


FIGURE 81.1

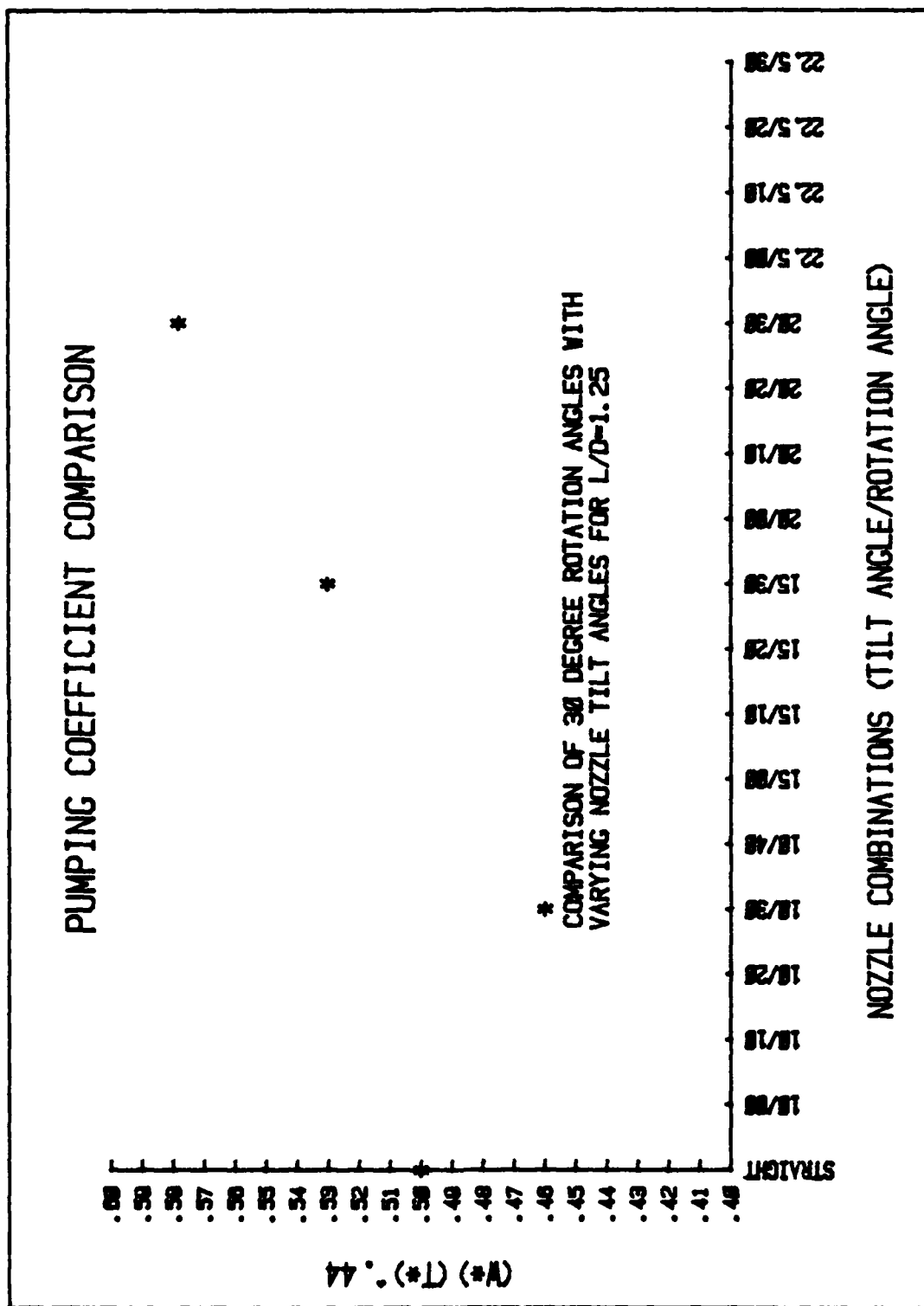


FIGURE 81.2



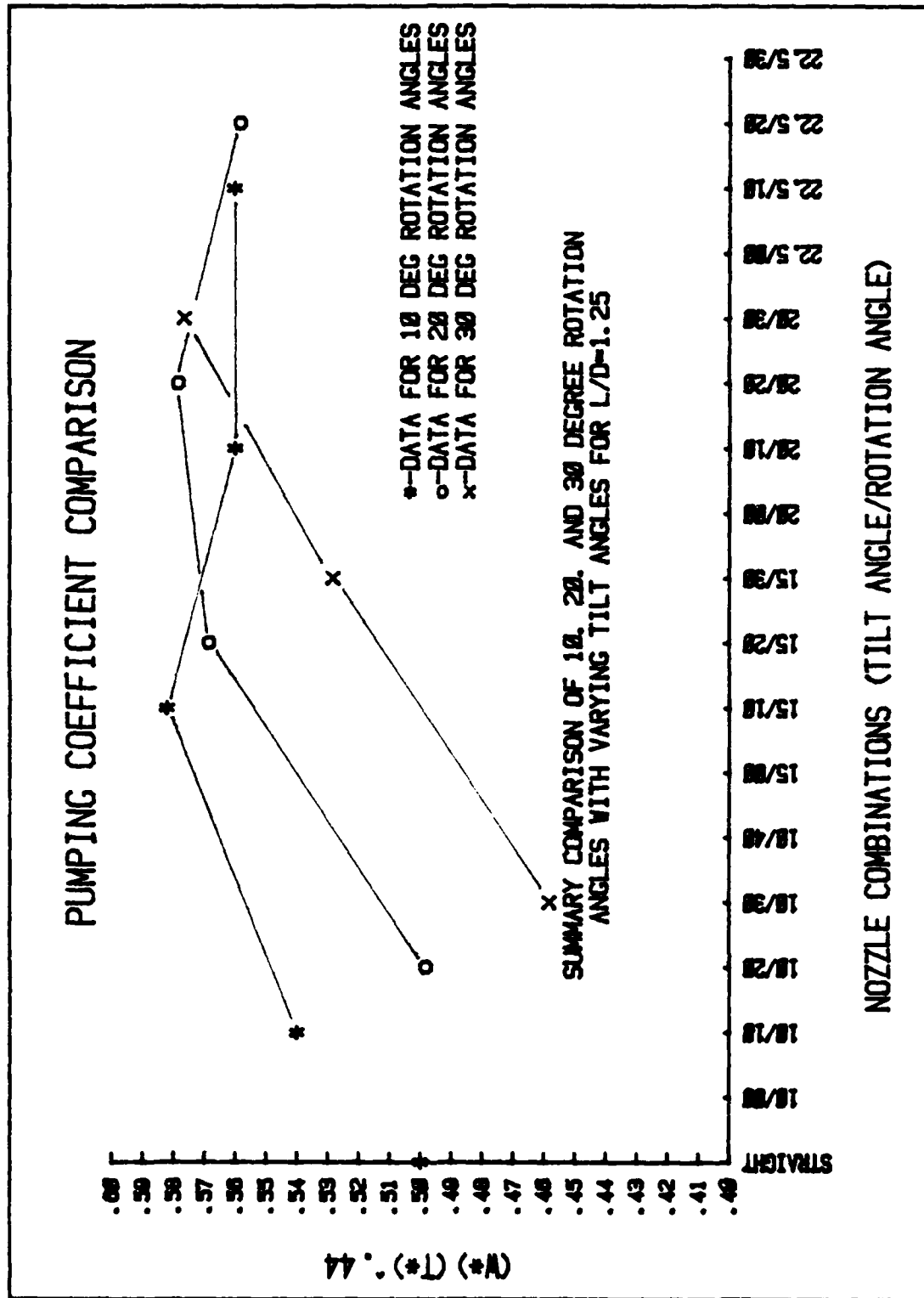


FIGURE 81.3

SUMMARY OF TABULATED DATA

L/D RATIO	S/D RATIO	NOZZLE		(U/P) (T°) .44	ACCURACY	DATA			DTG/RUN	COMMENTS
		TILT	ROTATION			PCD	HSD	VTL		
1.75	0.5	00	00	.54	±.005	X	X	X	0208011	Calibration run. Data compared extremely well with LEMKE-STAEHLI data.
	0.5	10	10	.58	±.005	X			1908014	Better than straight but below the 15/20 nozzles.
		10	20	.56	±.005	X			1908013	Better than straight but below the 15/20 nozzles.
		10	30	.51	±.005	X			1908012	Worse than both the straight and the 15/20 nozzles.
		10	40	.47	±.005	X			1908011	Much worse than the straight and the 15/20 nozzles.
	0.5	15	00	.57	±.005	X	X	X	0308011	Better than the straight but below the 15/20 nozzles. One positive MSD point.
		15	00	NA	NA	X	X		0508011	HSD and rotation angle comparison run with the base plate fixed at zero.
		15	00	NA	NA	X	X		0508012	HSD and rotation angle comparison run with the base plate fixed at the peak position 'A' value.
		15	00	NA	NA	X	X		0508013	HSD and rotation angle comparison run with the base plate rotated for peak position 'A' pressure values.
		15	10	.59	±.005	X	X	X	1008011	Better than straight nozzles but slightly below 15/20 nozzles. VTD edge effects.
		15	20	.59+	±.005	X	X	X	1008012	Best nozzle combination based on PCD, VTD adequate. MSD had one positive point.
	0.5	15	25	.58	±.0025	X	X	X	1208011	S/D comparison run. Better than straight but below 15/20 nozzles. Positive MSD pressure point.
	0.4	15	25	.585	±.0025	X	X	X	1208012	S/D comparison. Slightly better than with S/D=0.5 and positive MSD point was intermittent.
	0.25	15	25	.55	±.0025	X	X	X	1308011	S/D comparison run. Better than straight nozzles but below other S/D comparison data.
	0.5	15	30	.55	±.0025	X	X	X	1108011	Intermittent positive MSD point. Better than straight but below 15/20 nozzles.
	0.5	20	10	.56	±.0025	X	X	X	1708011	One slightly positive MSD point. Better than straight but below 15/20 nozzles. Generally poor MSD and VTD profiles.
		20	20	.58	±.01	X	X	X	1808011	Better than straight but slightly below 15/20 nozzles. One positive MSD pre-aure point but fairly flat VTD profile.

TABLE 1.1 SUMMARY OF TABULATED DATA

SUMMARY OF TABULATED DATA (CONTINUED)

L/D RATIO	S/D RATIO	NOZZLE ROTATION		(H°) (T°) .44	ACCURACY	DATA		DTG/RUN	COMMENTS
		TILT	ROTATION			PCD	MSD		
1.75	0.5	20	30	.58	±.0025	X		1908018	Better than straight nozzles but just below 15/20 nozzles.
	0.5	22.5	10	.54	±.0025	X		1908017	Slightly better than straight nozzles but well below 15/20 nozzles.
		22.5	20	.56	±.005	X		1908016	Better than straight nozzles but below 15/20 nozzles.
		22.5	25	.57	±.0025	X		1908015	Better than straight nozzles but below 15/20 nozzles.
1.5	0.5	00	00	.51	±.01	X	X	2008011	Straight nozzle calibration run. PCD worse than L/D=1.75 straight nozzles but MSD and VTD profiles were essentially the same for both mixing stacks.
	0.5	10	10	.56	±.0025	X		2108011	Better than straight nozzles but below 15/20 nozzles.
		10	20	.52	±.005	X		2308012	Slightly better than straight nozzles but well below 15/20 nozzles.
		10	30	.49	±.0025	X		2308013	Worse than the straight or the 15/20 nozzle combinations.
0.5		10	40	.46	±.01	X		2308014	Worst nozzle combination for the L/D=1.5 mixing stack.
	0.5	15	10	.50	±.0025	X		2308015	Better than the straight nozzles but just below the 15/20 nozzles.
		15	20	.58	±.0025	X		2308016	PCD data run only. Best nozzle combination as verified by the full data run.
		15	20	.58+	±.0025	X	X	2408011	Essentially the same pumping coefficient as the L/D=1.75 stack. Good MSD and rotation profile, but more pronounced peaks and troughs in the VTD profile compared to the L/D=1.75 stack and 15/20 nozzles.
0.5		15	30	.56	±.0025	X		2308017	Better than straight but below 15/20 nozzles.
	0.5	20	10	.56	±.005	X		2408012	Better than straight but below the 15/20 nozzles.
		20	20	.56	±.0025	X		2408013	Better than straight but below the 15/20 nozzles.
		20	30	.57	±.005	X		2408014	Better than straight but below the 15/20 nozzles.
0.5	0.5	22.5	10	.54	±.0025	X		2408015	Better than straight but below the 15/20 nozzles.
		22.5	20	.55	±.01	X		2408016	Better than straight but below the 15/20 nozzles.

TABLE 1.2 SUMMARY OF TABULATED DATA (CONT)

SUMMARY OF TABULATED DATA (CONTINUED)

L/D RATIO	S/D RATIO	NOZZLE ROTATION		(W*) (T*) .44	ACCURACY	DATA		DTG/RUN	COMMENTS
		TILT	ROTATION			PCD	MSD		
1.25	0.5	00	00	.50	±.005	X	X	2508811	PCD below L/D=1.5 and L/D=1.75 straight nozzles. MSD profile is good, but still remains below the longer mixing stacks. VTD profile has more pronounced peaks and troughs than the longer stacks.
		10	10	.54	±.0025	X		2608811	Better than the straight but below the 15/10 nozzles.
		10	20	.50	±.0025	X		2608812	Just slightly better than the straight nozzles and well below the 15/10 nozzles.
		10	30	.46	±.005	X		2608813	Well below the straight or the 15/10 nozzles.
		10	40	.43	±.01	X		2608814	Worst nozzle combination for any of the mixing stacks tested.
	0.5	15	10	.58+	±.0025	X		2508815	PCD data only, but should be the best combination for this mixing stack.
		15	20	.57	±.005	X		2608816	This combination should have been the best combination for the L/D=1.25 stack based on past data, but it fell off for unexplained reasons.
		15	20	.56	±.0025	X	X	2708812	More accurate data. Confirms drop in pumping coefficient. MSD and VTD profile are above average, and no positive pressure points. VTD profile does show more pronounced peaks and troughs.
		15	30	.53	±.01	X		2608817	Slightly better than straight nozzles but worse than 15/10 nozzles.
		20	10	.56	±.005	X		2608818	Better than the straight nozzles but below the 15/10 nozzles.
	0.5	20	20	.58	±.0025	X		2608819	PCD shows a strong contender for best nozzle combination selection.
		20	20	.58	±.0025	X	X	2708813	Good PCD, but MSD profile is markedly poor and has two positive pressure points. Some misalignment on VTD profile, but in general, horizontal profile is better and diagonal profile is worse than 15/20 combination.
		20	30	.58	±.0025	X		2708811	PCD just below 20/20 and 15/10 nozzles. All are very close.
		22.5	10	.56	±.005	X		2708814	Better than the straight nozzles but below the 15/10 nozzles.
		22.5	20	.56	±.005	X		2708815	Better than the straight nozzles but below the 15/10 nozzles.

TABLE 1.3 SUMMARY OF TABULATED DATA (CONT)

DATA TAKEN ON: 2 AUG 61  
 DATA TAKEN BY: C. C. DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 20.48 IN  
 DIAMETER: 11.78 IN  
 L/D RATIO: 1.75  
 S/D RATIO: 0.59

NOZZLE AN/AP AREA RATIO: 2.58

COMMENTS:  
 STRAIGHT NOZZLES-CAL RUN

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 5.902 IN  
 ORIFICE AREA: 0.497  
 UPTAKE AREA: 107.510 IN<sup>2</sup>  
 ATM PRESSURE: 30.09 INHG

N	FOR	DPOR	TOR	TUPT	TAMB	PUPY	PSEC	PIER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F					IN OF H2O		SQUARE INCHES	SQUARE INCHES
1	0.70	21.9	56.4	108.8	67.3	3.20	3.21	0.00	0.000	111111
2	0.69	21.8	56.4	109.2	67.3	4.10	2.12	0.00	12.566	111111
3	0.69	21.7	56.6	109.4	67.3	4.65	1.44	0.00	25.133	111111
4	0.70	22.1	56.6	109.6	67.3	5.45	0.61	0.00	50.265	111111
5	0.70	22.0	56.4	109.6	67.3	5.95	0.30	0.00	100.531	111111
6	0.69	22.0	56.6	109.8	67.3	6.05	0.14	0.00	150.796	111111
7	0.70	22.0	56.4	109.8	67.3	6.10	0.10	0.00	201.062	111111
8	0.70	22.0	56.6	109.8	67.3	6.15	0.06	0.00	245.044	111111
9	0.70	22.0	56.2	109.8	67.3	6.20	0.01	0.00	288.888	111111

SECONDARY BOX

N	MR	P2	T2	PR/TS	WAT-44	HP	WS	UP	UH	UUPY	UPT	WACH
RUN						LBH/SEC	LBH/SEC	FT/SEC	FT/SEC	FT/SEC		
1	0.000	0.4365	0.9270	0.4708	0.0000	3.7501	0.0000	180.31	72.13	72.13	0.062	
2	0.1675	0.2907	0.9263	0.3138	0.1620	3.7416	0.6268	179.55	82.91	71.83	0.061	
3	0.2769	0.1990	0.9260	0.2149	0.2676	3.7323	1.0333	178.07	89.83	71.55	0.061	
4	0.4115	0.1102	0.9257	0.1190	0.3977	3.7665	1.5499	180.29	99.54	72.12	0.062	
5	0.5019	0.0411	0.9257	0.0444	0.4851	3.7587	1.8865	179.69	105.25	71.88	0.061	
6	0.5144	0.0192	0.9254	0.0207	0.4971	3.7580	1.9330	179.65	106.06	71.87	0.061	
7	0.5735	0.0137	0.9254	0.0140	0.5601	3.7587	2.1783	179.67	110.41	71.87	0.061	
8	0.5472	0.0082	0.9254	0.0099	0.5209	3.7579	2.0564	179.61	108.23	71.85	0.061	
9	0.5888	0.0007	0.9254	0.0007	0.5888	3.7594	1.9017	179.66	108.23	71.87	0.061	

TABLE 2 - PCD DATA FOR STRAIGHT NOZZLES WITH L/D=1.75 STACK.

TERTIARY BOX

N	WTS	PTA	ITS	PT6/ITS	WTS77-44	MM	UT	UE
LBN/SEC LBN/SEC FT/SEC								
RUN								
1	0.0000	0.0000	0.9270	0.0000	0.0000	3.750	0.0000	0.0000
2	0.0000	0.0000	0.9263	0.0000	0.0000	4.360	0.0000	0.0000
3	0.0000	0.0000	0.9260	0.0000	0.0000	4.766	0.0000	0.0000
4	0.0000	0.0000	0.9257	0.0000	0.0000	5.316	0.0000	0.0000
5	0.0000	0.0000	0.9257	0.0000	0.0000	5.645	0.0000	0.0000
6	0.0000	0.0000	0.9254	0.0000	0.0000	5.691	0.0000	0.0000
7	0.0000	0.0000	0.9254	0.0000	0.0000	5.937	0.0000	0.0000
8	0.0000	0.0000	0.9254	0.0000	0.0000	5.814	0.0000	0.0000
9	0.0000	0.0000	0.9254	0.0000	0.0000	0.0000	0.0000	0.0000

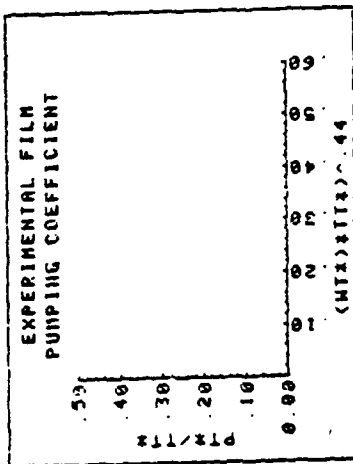
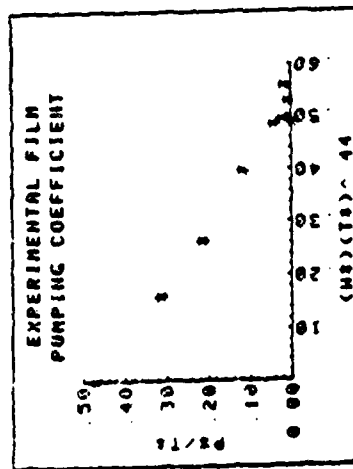


TABLE 2.1 - PCD DATA (CONT) FOR STRAIGHT NOZZLES WITH L/D=1.75 STACK

MIXING STACK DATA FOR RUN 9

TOP (POSITION 'A') DATA				DIAGONAL (POSITION 'B') DATA			
X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PHSE	X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PHSE
0.00	-1.950	0	-0.273	0.00	-1.450	0	-0.199
0.25	-0.920	0	-0.126	0.25	-0.930	0	-0.127
0.50	-0.720	0	-0.059	0.50	-0.710	0	-0.097
0.75	-0.610	0	-0.084	0.75	-0.600	0	-0.082
1.00	-0.450	0	-0.066	1.00	-0.480	0	-0.066
1.25	-0.310	0	-0.042	1.25	-0.310	0	-0.042
1.50	-0.200	0	-0.027	1.50	-0.190	0	-0.026

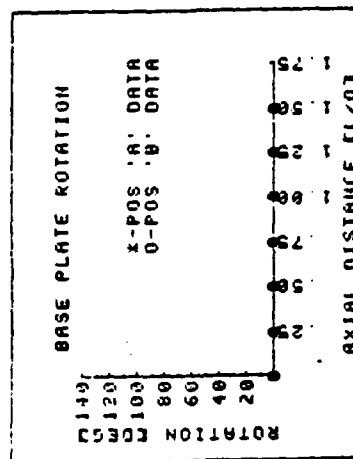
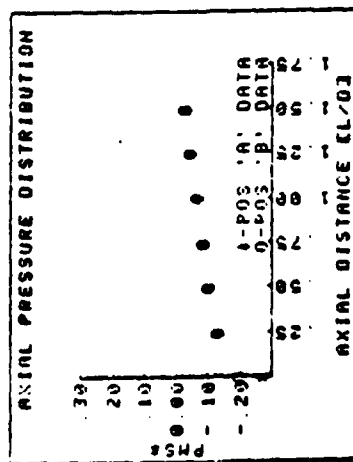
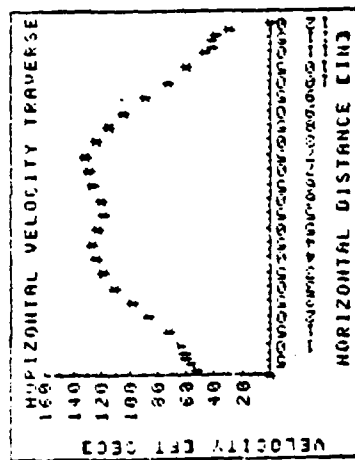


TABLE 2.2 - MSD DATA FOR STRAIGHT NOZZLES WITH L/D=1.75 STACK

HORIZONTAL VELOCITY TRAVERSE AT		BASE POSITION OF 90 DEGREES	
POSITION	0.00	0.20	0.40
FEIN H203	0.00	0.60	0.80
VEFT-SEC3	0.00	0.70	0.85
POSITION	0.00	51.50	55.63
FEIN H203	2.00	2.50	3.00
VEFT-SEC3	1.70	2.30	2.80
POSITION	86.92	98.62	111.26
FEIN H203	5.50	6.00	6.50
VEFT-SEC3	3.20	3.30	3.60
POSITION	118.94	120.78	126.15
FEIN H203	9.00	9.50	10.00
VEFT-SEC3	2.50	1.80	1.20
POSITION	105.13	89.20	72.84
FEIN H203	11.60	11.80	12.00
VEFT-SEC3	0.35	0.20	0.00



DIAGONAL VELOCITY TRAVERSE FOR		BASE POSITION OF 90 DEGREES	
POSITION	0.00	0.20	0.40
FEIN H203	0.00	0.50	1.10
VEFT-SEC3	0.00	47.01	69.73
POSITION	2.00	2.50	3.00
FEIN H203	5.10	6.00	6.10
VEFT-SEC3	150.15	162.86	164.22
POSITION	5.50	6.00	6.50
FEIN H203	3.20	3.10	3.30
VEFT-SEC3	118.94	117.07	120.78
POSITION	9.00	9.50	10.00
FEIN H203	6.10	5.90	5.00
VEFT-SEC3	164.22	161.50	148.67
POSITION	11.60	11.80	12.00
FEIN H203	1.50	1.20	0.00

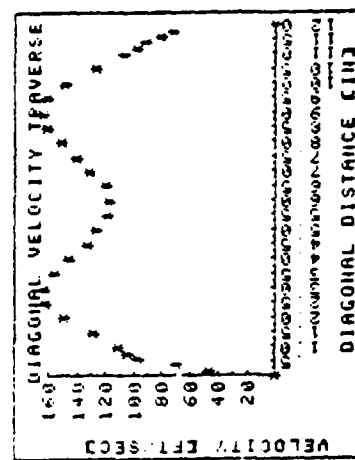


TABLE 2.3 - VTD DATA FOR STRAIGHT NOZZLES WITH L/D=1.75 STACK



DATA TAKEN ON: 19 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 20.48 [IN]  
 DIAMETER: 11.70 [IN]  
 L/D RATIO: 1.75  
 S/D RATIO: 0.50

NOZZLE AN/AP AREA RATIO: 2.50

COMMENTS:  
 10 TILT/10 POTATION/PCD

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 10 [DEG]  
 ROTATION ANGLE: 10 [DEG]  
 AREA PER NOZZLE: 10.752 [IN2]  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.982 [IN]  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 [IN2]  
 ATM. PRESSURE: 30.12 [INHG]

N	POR	DPOR	TOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.70	22.0	50.0	112.6	71.2	3.25	3.10	0.00	0.000	*****
2	0.69	21.9	50.0	112.4	71.2	4.15	2.23	0.00	12.566	*****
3	0.69	22.1	50.6	112.2	71.2	4.75	1.61	0.00	25.133	*****
4	0.69	22.0	50.0	112.2	71.4	5.40	0.88	0.00	50.265	*****
5	0.69	21.9	59.2	112.4	71.4	5.90	0.34	0.00	100.531	*****
6	0.69	21.9	59.4	112.0	71.6	6.05	0.19	0.00	150.796	*****
7	0.69	21.0	50.2	112.6	71.0	6.15	0.01	0.00	*****	*****

# SECONDARY BOX

N	WS	PS	TS	PS/TS	WRT^44	WP	WS	UP	UM	UUP	UPT	MACH
RUN							LBN/SEC	LBN/SEC	FT/SEC	FT/SEC	FT/SEC	
1	0.0000	0.4239	0.9277	0.4634	0.0000	3.7510	0.0000	101.41	72.57	72.57	0.062	
2	0.1711	0.3040	0.9280	0.3276	0.1655	3.7462	0.6400	100.65	83.67	72.27	0.062	
3	0.2096	0.2106	0.9203	0.2355	0.2802	3.7611	1.0891	101.03	91.81	72.42	0.062	
4	0.4200	0.1203	0.9287	0.1296	0.4151	3.7548	1.6100	100.40	100.84	72.17	0.062	
5	0.5309	0.0462	0.9203	0.0498	0.5139	3.7419	1.9868	179.61	107.23	71.85	0.061	
6	0.5030	0.0240	0.9200	0.0260	0.5649	3.7412	2.1041	179.63	110.77	71.06	0.061	
7	0.0000	0.0007	0.9207	0.0007	0.0000	3.7370	1.0946	179.29	0.0000	71.72	0.061	

TABLE 3 -- PCD DATA FOR 10/10 NOZZLES WITH L/D=1.75 STACK

TERTIARY BOX

N	WT	PT	TT	PT/TT	WT/TT	WT	UE
RUN					LBN/SEC	LBN/SEC	FT/SEC
1	0.0000	0.0000	0.9277	0.0000	3.752	3.752	0.0000
2	0.0000	0.0000	0.9280	0.0000	4.387	4.387	0.0000
3	0.0000	0.0000	0.9283	0.0000	4.850	4.850	0.0000
4	0.0000	0.0000	0.9287	0.0000	5.365	5.365	0.0000
5	0.0000	0.0000	0.9283	0.0000	5.729	5.729	0.0000
6	0.0000	0.0000	0.9280	0.0000	5.925	5.925	0.0000
7	0.0000	0.0000	0.9287	0.0000	5.925	5.925	0.0000

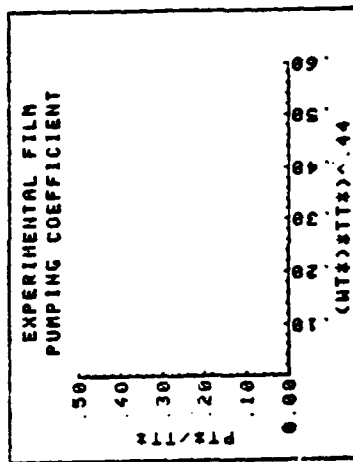
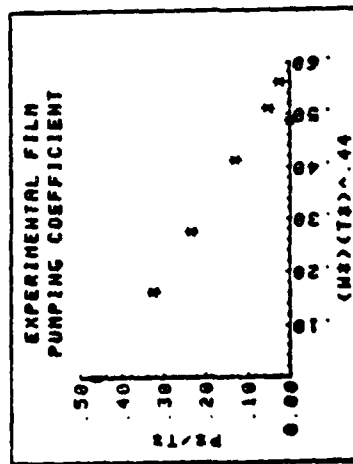


TABLE 3.1 - PCD DATA (CONT) FOR 10/10 NOZZLES WITH L/D=1.75 STACK

DATA TAKEN ON: 19 AUG 81  
 DATA TAKEN BY: C. C. DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 20.48 INJ  
 DIAMETER: 11.70 INJ  
 L/D RATIO: 1.75  
 S/D RATIO: 0.30

NOZZLE AN-AP AREA RATIO: 2.50  
 10 TILT: 20 ROTATION/PCD

COMMENTS:  
 10 TILT: 20 ROTATION/PCD

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.982 INJ  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.519 INJ  
 ATM. PRESSURE: 30.12 INHG

N	POR	OPOR	TOR	TUPT	TANB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F					IN OF H2O		SQUARE INCHES	SQUARE INCHES
1	0.70	22.1	59.2	112.6	71.4	3.25	3.15	0.00	0.000	0.000
2	0.69	21.9	59.0	112.0	71.4	4.15	2.18	0.00	12.566	0.000
3	0.70	22.1	58.6	112.6	71.0	4.80	1.56	0.00	25.133	0.000
4	0.70	22.0	59.2	112.6	71.0	5.45	0.85	0.00	50.265	0.000
5	0.70	22.1	59.0	112.0	71.0	6.00	0.31	0.00	100.531	0.000
6	0.70	22.0	59.2	112.0	71.0	6.10	0.16	0.00	150.796	0.000
7	0.70	22.0	58.6	112.6	72.0	6.25	0.01	0.00	0.000	0.000

# SECONDARY BOX

N	NP	PA	TS	PT/TS	MTA	44	HP	MS	UP	UM	UUPY	UPT	MACM
RUN								LBH/SEC	LBH/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC
1	0.0000	0.4245	0.9280	0.4374	0.0000	3.7589	0.0000	131.74	72.70	72.70	0.062	0.062	0.062
2	0.1693	0.2975	0.9277	0.3207	0.1638	3.7426	0.6335	180.58	83.52	72.24	0.062	0.062	0.062
3	0.2849	0.2118	0.9287	0.2260	0.2758	3.7611	1.0714	181.13	91.55	72.46	0.062	0.062	0.062
4	0.4218	0.1165	0.9287	0.1254	0.4082	3.7504	1.5817	180.30	100.32	72.13	0.062	0.062	0.062
5	0.5082	0.0423	0.9284	0.0456	0.4918	3.7596	1.9105	180.57	106.28	72.24	0.062	0.062	0.062
6	0.5489	0.0229	0.9284	0.0237	0.5313	3.7504	2.0508	180.06	106.72	72.03	0.061	0.061	0.061
7	0.5888	0.0007	0.9291	0.0007	0.5888	3.7526	1.0942	180.04	0.000	72.02	0.061	0.061	0.061

TABLE 4 - PCD DATA FOR 10/20 NOZZLES WITH L/D=1.75 STACK

TERTIARY BOX

N	MT	PT	TIA	PIA/TIA	MT/TIA	44	MM	MT	UE
LBM/SEC LBM/SEC FT/SEC									
RUN									
1	0.0000	0.0000	0.9280	0.0000	1.1111	3.759	1.1111	1.1111	1.1111
2	0.0000	0.0000	0.9277	0.0000	1.1111	4.376	1.1111	1.1111	1.1111
3	0.0000	0.0000	0.9287	0.0000	1.1111	4.833	1.1111	1.1111	1.1111
4	0.0000	0.0000	0.9287	0.0000	1.1111	5.332	1.1111	1.1111	1.1111
5	0.0000	0.0000	0.9224	0.0000	1.1111	5.670	1.1111	1.1111	1.1111
6	0.0000	0.0000	0.9284	0.0000	1.1111	5.809	1.1111	1.1111	1.1111
7	0.0000	0.0000	0.9291	0.0000	1.1111	1.1111	1.1111	1.1111	1.1111

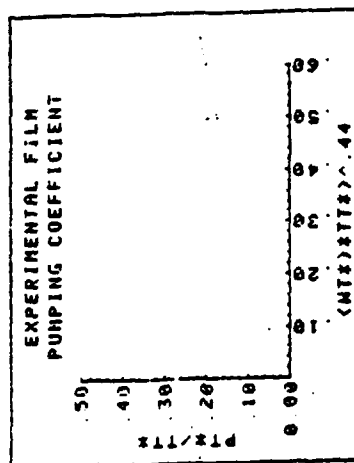
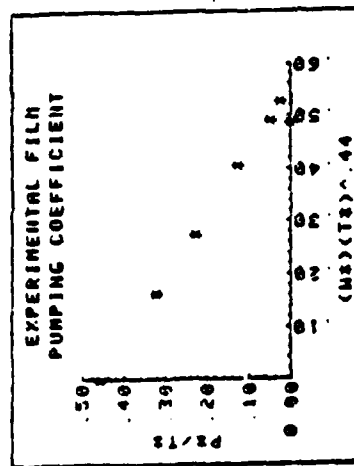


TABLE 4.1 - PCD DATA (CONT) FOR 10/20 NOZZLES WITH L/D=1.75 STACK

DATA TAKEN ON: 19 AUG 81  
 DATA TAKEN BY: C.C. GAVIS

MIXING STACK INFORMATION:  
 LENGTH: 20.40 CINS  
 DIAMETER: 11.70 CINS  
 L/D RATIO: 1.75  
 S/D RATIO: 0.50

NOZZLE AN-AP AREA RATIO: 2.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 10 DEGS  
 ROTATION ANGLE: 30 DEGS  
 AREA PER NOZZLE: 10.752 CINH2  
 NUMBER OF NOZZLES: 4

COMMENTS:  
 10 TILL 30 POTATION/PCD

MISCELLANEOUS INFORMATION:  
 ORIFACE DIAMETER: 6.902 CINH  
 ORIFACE BETA: 0.497 CINH  
 UPTAKE AREA: 107.510 CINH2  
 ATM. PRESSURE: 30.12 CINH2

N	POP	DPOP	TOP	TUPT	TAMB	PUFT	PSEC	PTER	SECONDARY AREA SQUARE INCHES	TERTIARY AREA SQUARE INCHES
RUN	IN OF H2O	DEGREES F					IN OF H2O			
1	0.71	22.1	58.2	112.0	71.6	3.40	3.00	0.00	0.000	1111111
2	0.70	22.0	58.2	112.0	71.6	4.30	2.00	0.00	12.566	1111111
3	0.70	21.9	58.0	111.0	71.6	4.90	1.44	0.00	25.133	1111111
4	0.70	22.0	58.6	112.0	71.6	5.55	0.77	0.00	50.265	1111111
5	0.70	21.9	58.2	112.0	71.8	6.00	0.27	0.00	100.531	1111111
6	0.70	22.0	58.4	112.0	71.8	6.15	0.14	0.00	150.796	1111111
7	0.70	22.0	57.0	111.0	71.8	6.30	0.01	0.00	1111111	1111111

SECONDARY BOX

N	WS	PS	TS	PS/TS	WAT	44	NP	WS	UP	UM	UPT	UPT WACH
RUN								LBH/SEC	LBH/SEC	FT/SEC	FT/SEC	
1	0.9000	0.4154	0.9293	0.4470	0.0000	3.7625	0.0000	181.69	72.63	72.68	0.062	
2	0.1646	0.2832	0.9293	0.3047	0.1596	3.7540	0.6187	180.83	83.35	72.34	0.062	
3	0.2740	0.1976	0.9297	0.2126	0.2662	3.7462	1.0296	180.11	90.39	72.05	0.061	
4	0.4000	0.1049	0.9293	0.1129	0.3073	3.7526	1.5008	180.18	98.82	72.00	0.062	
5	0.4760	0.0373	0.9297	0.0401	0.4610	3.7455	1.7830	179.62	103.63	71.86	0.061	
6	0.7039	0.0106	0.9297	0.0200	0.4072	3.7533	1.8911	179.94	105.69	71.90	0.061	
7	0.0000	0.0007	0.9300	0.0007	0.0000	3.7555	1.8946	179.92	1111111	71.90	0.061	

TABLE 5 - PCD DATA FOR 10/30 NOZZLES WITH L/D=1.75 STACK

VEPTIARY BOX

N	WT	PT	IT	PT	IT	WT	UE
RUN							
1	3.762	0.0000	0.9293	0.0000	3.762	111111	111111
2	4.373	0.0000	0.9293	0.0000	4.373	111111	111111
3	4.776	0.0000	0.9297	0.0000	4.776	111111	111111
4	5.253	0.0000	0.9293	0.0000	5.253	111111	111111
5	5.528	0.0000	0.9297	0.0000	5.528	111111	111111
6	5.644	0.0000	0.9297	0.0000	5.644	111111	111111
7	5.644	0.0000	0.9300	0.0000	5.644	111111	111111

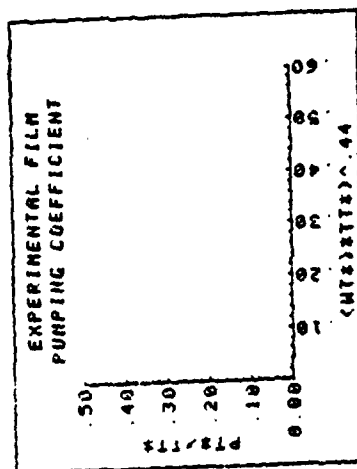
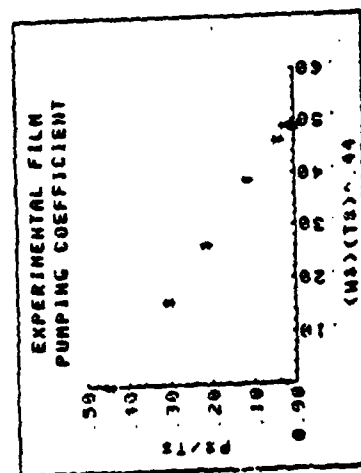


TABLE 5.1 - PCD DATA (CONT) FOR 10/30 NOZZLES WITH L/D=1.75 STACK

DATA TAKEN ON: 19 AUG 81  
 DATA TAKEN BY: C. C. DAVIS  
 NOZZLE AIR HP AREA RATIO: 2.50  
 COMMENTS:  
 10 TILT-40 POSITION EMAN3/PCD  
 MIXING STAGE INFORMATION:  
 LENGTH: 20.48 CINH  
 DIAMETER: 11.70 CINH  
 L/D RATIO: 1.75  
 S/D RATIO: 0.50  
 PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 10 DECG  
 ROTATION ANGLE: 40 DECG  
 AREA PER NOZZLE: 10.752 CINH2  
 NUMBER OF NOZZLES: 4  
 MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINH  
 ORIFICE BETA: 0.437  
 UPTAKE AREA: 107.310 CINH2  
 ATM PRESSURE: 30.12 CINHG3

N	POP	OPOR	TOR	TUPT	TAMB	PUP	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SOURCE INCHES
1	0.70	22.1	57.2	111.6	71.0	3.55	2.95	0.00	0.000	1111111
2	0.70	22.0	57.0	111.6	71.6	4.45	1.92	0.00	12.566	1111111
3	0.70	22.0	57.0	111.0	71.0	5.10	1.31	0.00	25.173	1111111
4	0.70	22.1	57.0	111.6	71.0	5.70	0.67	0.00	50.265	1111111
5	0.70	22.0	57.4	111.6	71.0	6.10	0.24	0.00	100.531	1111111
6	0.70	22.0	57.2	111.6	71.0	6.20	0.12	0.00	150.756	1111111
7	0.70	22.0	57.2	111.6	71.0	6.30	0.01	0.00	444444	1111111

# SECONDARY BOX

N	M2	P2	T2	P2/T2	MAT	44	HP	HS	UP	UN	UUP	UPT	MACH
RUN							LBH/SEC	LBH/SEC	FT/SEC	FT/SEC	FT/SEC		
1	0.0000	0.3374	0.9303	0.4272	0.0000	0.0000	3.7562	0.0000	181.68	72.68	72.68	0.062	
2	0.1531	0.2611	0.9300	0.2908	0.1531	0.5936	3.7555	0.5936	180.70	82.96	72.29	0.062	
3	0.2614	0.1791	0.9300	0.1922	0.2532	0.9818	3.7554	0.9818	180.50	89.70	72.21	0.062	
4	0.3717	0.0909	0.9303	0.0977	0.3601	1.3991	3.7640	1.3991	180.56	97.16	72.23	0.062	
5	0.4428	0.0123	0.9303	0.0347	0.4289	1.6674	3.7569	1.6674	180.03	101.66	72.02	0.061	
6	0.4643	0.0150	0.9303	0.0170	0.4500	1.7454	3.7576	1.7454	180.01	103.12	72.01	0.061	
7	0.0000	0.0007	0.9303	0.0007	0.0000	1.8946	3.7576	1.8946	179.97	103.88	71.99	0.061	

TABLE 6 - PCD DATA FOR 10/40 NOZZLES WITH L/D=1.75 STACK

# TERTIARY BOX

IN	OUT	PT	IT	PT	MT	44	IN	HT	DE
LBN/SEC LBN SEC FT/SEC									
RUN									
1	00000	0.0000	0.9303	0.0000	00000	00000	3.765	00000	00000
2	00000	0.0000	0.9303	0.0000	00000	00000	4.349	00000	00000
3	00000	0.0000	0.9303	0.0000	00000	00000	4.737	00000	00000
4	00000	0.0000	0.9303	0.0000	00000	00000	5.163	00000	00000
5	00000	0.0000	0.9303	0.0000	00000	00000	5.420	00000	00000
6	00000	0.0000	0.9303	0.0000	00000	00000	5.503	00000	00000
7	00000	0.0000	0.9303	0.0000	00000	00000	00000	00000	00000

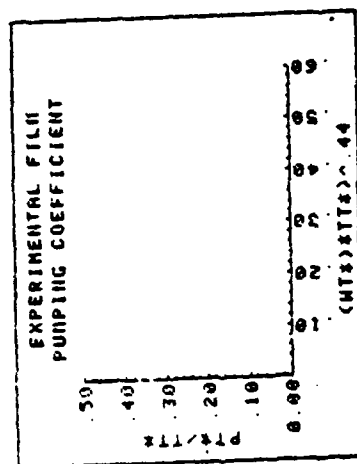
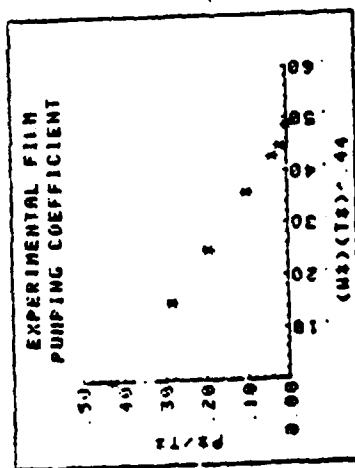


TABLE 6.1 - PCD DATA (CONT) FOR 10/40 NOZZLES WITH L/D=1.75 STACK



DATA TAKEN ON: 3 AUG 81  
 DATA TAKEN BY: C C DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 20.48 [IN]  
 DIAMETER: 11.78 [IN]  
 L/D RATIO: 1.75  
 S/D RATIO: 0.50

NOZZLE ANGLE: 15 DEGS  
 ROTATION ANGLE: 0 DEGS  
 AREA PER NOZZLE: 10.752 [IN<sup>2</sup>]  
 NUMBER OF NOZZLES: 4

NOZZLE ANGLE RATIO: 2.50

15 TILT/00 ROTATION CAL-FUN

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 [IN]  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 [IN<sup>2</sup>]  
 ATM PRESSURE: 30.06 [INHG]

W	POR	GFOR	TOR	TUPT	TANB	FUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
IN OF H2O	IN OF H2O	DEGREES F	IN OF H2O	IN OF H2O	IN OF H2O	IN OF H2O	IN OF H2O	IN OF H2O	SQUARE INCHES	SQUARE INCHES
1	0.69	22.0	55.6	107.6	67.0	3.75	3.14	0.00	0.000	111111
2	0.69	22.1	55.9	107.8	67.0	4.40	2.12	0.00	12.566	111111
3	0.69	22.0	55.8	108.2	67.0	4.95	1.48	0.00	25.133	111111
4	0.69	21.9	55.6	108.8	67.0	5.50	0.84	0.00	50.265	111111
5	0.69	22.1	55.6	108.8	67.0	6.05	0.33	0.00	100.531	111111
6	0.69	22.1	55.8	108.8	67.0	6.15	0.19	0.00	150.796	111111
7	0.69	22.0	56.0	109.2	67.0	6.20	0.11	0.00	201.062	111111
8	0.69	22.0	55.8	109.2	67.0	6.25	0.08	0.00	245.044	111111
9	0.69	22.0	56.4	109.4	67.0	6.30	0.01	0.00	111111	111111

# SECONDARY BOX

N	HS	PS	TV	PA/TI	NAT	44	UP	HS	UP	UM	UUPI	UPT	UACH
LBH/SEC	LBH/SEC	LBH/SEC	LBH/SEC	LBH/SEC	LBH/SEC	LBH/SEC	LBH/SEC	LBH/SEC	LBH/SEC	LBH/SEC	LBH/SEC	LBH/SEC	LBH/SEC
1	0.0000	0.4250	0.9284	0.4539	0.0000	3.7597	0.0000	180.55	72.22	72.23	0.062	0.062	0.062
2	0.1453	0.2827	0.9281	0.3100	0.1610	3.7675	0.5267	180.53	87.71	72.22	0.062	0.062	0.062
3	0.2786	0.2031	0.9274	0.2179	0.2695	3.7590	1.0473	179.97	91.11	71.99	0.062	0.062	0.062
4	0.4207	0.1193	0.9265	0.1245	0.4068	3.7512	1.5780	179.50	99.73	71.81	0.061	0.061	0.061
5	0.5243	0.0450	0.9265	0.0486	0.5076	3.7683	1.9781	180.09	107.05	72.04	0.062	0.062	0.062
6	0.5976	0.0259	0.9265	0.0280	0.5778	3.7675	2.2514	180.00	111.05	72.00	0.062	0.062	0.062
7	0.6070	0.0151	0.9258	0.0163	0.5875	3.7563	2.2841	179.64	112.29	71.86	0.061	0.061	0.061
8	0.6316	0.0110	0.9258	0.0110	0.6105	3.7590	2.3740	179.67	113.89	71.87	0.061	0.061	0.061
9	0.6888	0.0014	0.9255	0.0015	0.6888	3.7560	2.6880	179.59	113.88	71.84	0.061	0.061	0.061

TABLE 7 - PCD DATA FOR 15/00 NOZZLES WITH L/D=1.75 STACK

TEPTIARY BOX

RUN	N	WT	PTS	ITS	PTS/ITS	WT/ITS	44	WM	NT	UE
1	111111	0.0000	0.0000	0.9281	0.0000	111111	3.750	111111	111111	111111
2	111111	0.0000	0.0000	0.9281	0.0000	111111	4.394	111111	111111	111111
3	111111	0.0000	0.0000	0.9274	0.0000	111111	4.806	111111	111111	111111
4	111111	0.0000	0.0000	0.9265	0.0000	111111	5.329	111111	111111	111111
5	111111	0.0000	0.0000	0.9265	0.0000	111111	5.746	111111	111111	111111
6	111111	0.0000	0.0000	0.9265	0.0000	111111	6.019	111111	111111	111111
7	111111	0.0000	0.0000	0.9258	0.0000	111111	6.042	111111	111111	111111
8	111111	0.0000	0.0000	0.9258	0.0000	111111	6.133	111111	111111	111111
9	111111	0.0000	0.0000	0.9255	0.0000	111111	6.111	111111	111111	111111

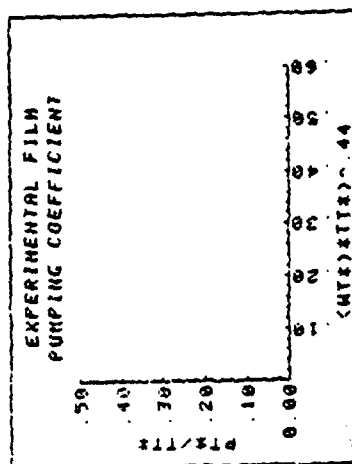
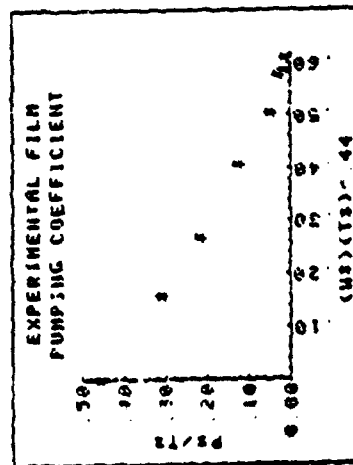


TABLE 7.1 - PCD DATA (CONT) FOR 15/00 NOZZLES WITH L/D=1.75 STACK

# MIXING STACK DATA FOR RUN 9

## TOP (POSITION 'A') DATA

X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PM51
0.20	-2.320	104	-0.328
0.25	-1.060	38	-0.145
0.50	-0.680	32	-0.093
0.75	-0.320	26	-0.053
1.00	-0.205	22	-0.028
1.25	-0.290	26	-0.040
1.50	0.090	33	0.012

## DIAGONAL (POSITION 'B') DATA

X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PM51
0.00	-1.590	104	-0.218
0.25	-0.870	38	-0.119
0.50	-0.330	32	-0.045
0.75	-0.260	26	-0.036
1.00	-0.165	22	-0.023
1.25	-0.250	26	-0.034
1.50	-0.065	33	-0.009

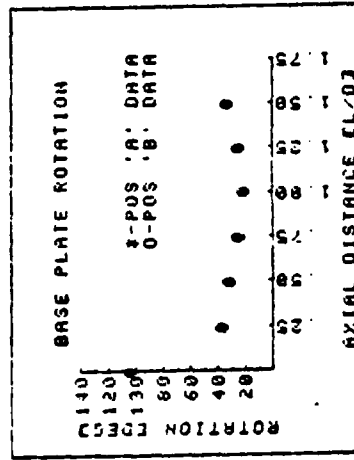
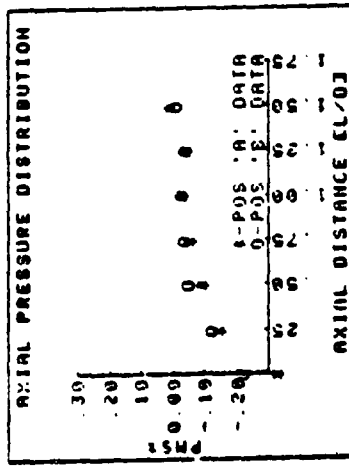
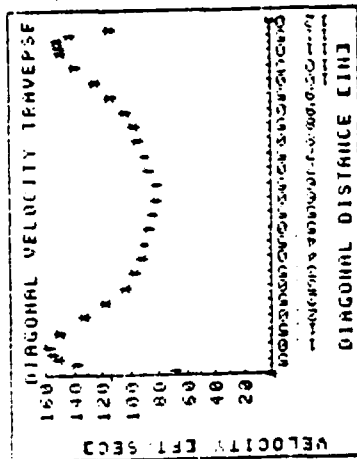


TABLE 7.2 - MSD DATA FOR 15/00 NOZZLES WITH L/D=1.75 STACK

HORIZONTAL VELOCITY TRAVERSE AT		BASE POSITION OF 0° DEGREE	
POSITION	0.00	0.20	0.40
FEIN H203	0.00	1.50	1.90
VEFT-SEC3	0.00	81.45	91.67
POSITION	2.00	2.50	3.00
FEIN H203	1.50	1.50	1.50
VEFT-SEC3	91.67	91.67	91.67
POSITION	5.50	6.00	6.50
FEIN H203	1.50	1.50	1.50
VEFT-SEC3	84.12	81.45	81.45
POSITION	9.00	9.50	10.00
FEIN H203	2.30	2.20	2.20
VEFT-SEC3	100.86	96.64	96.64
POSITION	11.60	11.80	12.00
FEIN H203	2.20	1.80	0.20



DIAGONAL VELOCITY TRAVERSE FOR		BASE POSITION OF 0° DEGREE	
POSITION	0.00	0.20	0.40
FEIN H203	0.00	1.05	4.30
VEFT-SEC3	0.00	68.15	137.90
POSITION	2.00	2.50	3.00
FEIN H203	4.00	3.10	2.40
VEFT-SEC3	133.01	117.09	103.03
POSITION	5.50	6.00	6.50
FEIN H203	1.60	1.50	1.50
VEFT-SEC3	84.12	81.45	81.45
POSITION	9.00	9.50	10.00
FEIN H203	2.40	2.90	3.50
VEFT-SEC3	103.03	113.25	124.42
POSITION	11.60	11.80	12.00
FEIN H203	4.60	2.00	0.00

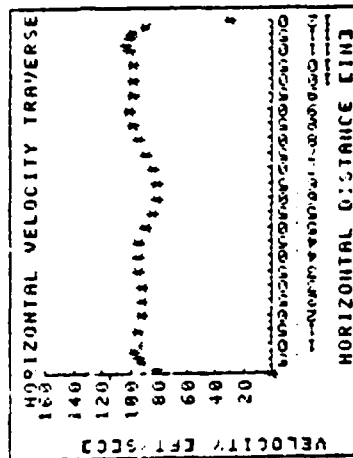


TABLE 7.3 - VTD DATA FOR 15/00 NOZZLES WITH L/D=1.75 STACK

DATA TAKEN ON: 5 AUG 81  
 DATA TAKEN BY: C. C. DAVIS  
 NOZZLE AN/AP AREA RATIO: 2.50  
 COMMENTS: COMPARISON OF ROTATION ANGLES  
 MIXING STACK INFORMATION:  
 LENGTH: 20.48 [IN]  
 DIAMETER: 11.70 [IN]  
 L/D RATIO: 1.75  
 S/D RATIO: 0.50  
 PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 15 [DEG]  
 ROTATION ANGLE: 0 [DEG]  
 AREA PER NOZZLE: 10.752 [IN2]  
 NUMBER OF NOZZLES: 4  
 MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 [IN]  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 [IN2]  
 ATM. PRESSURE: 30.00 [INHG]

M	FOR	DPOR	TOR	TUPT	TAMB	PUPY	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF M20	DEGREES F				IN OF M20			SQUARE INCHES	SQUARE INCHES
1	0.69	22.0	33.2	107.2	67.2	6.25	0.01	0.00	*****	*****

SECONDARY BOX

M	MS	PS	TS	PT8	MT8	44	MP	MS	UP	UM	UUPY	UPT	MACH
RUN													
1	*****	0.0007	0.9294	0.0007	*****	3.7650	1.9016	179.39	*****	71.76	0.061		

TERTIARY BOX

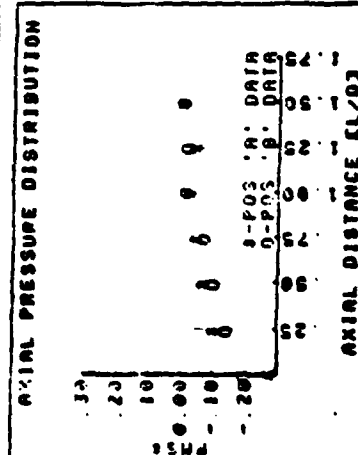
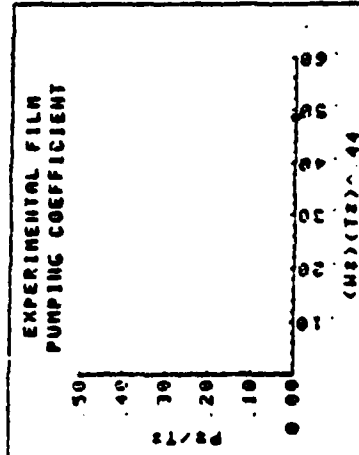
M	MT8	PT8	TT8	PT8/TT8	MT8/TT8	44	MM	MT	UE
RUN									
1	*****	0.0000	0.9294	0.0000	*****	*****	*****	*****	*****

TABLE 8 - PCD DATA FOR 15/00 NOZZLES WITH L/D=1.75 MSD COMPARISON  
 BASE PLATE FIXED AT 000 ROTATION

# MIXING STACK DATA FOR PUN 1

## TOP (POSITION 'A') DATA

X/D	PRESSURE CIN H2O3	ROTATION CDEG3	PHS4
0.00	-1.995	0	-0.274
0.25	-0.735	0	-0.101
0.50	-0.485	0	-0.067
0.75	-0.395	0	-0.042
1.00	-0.195	0	-0.027
1.25	-0.305	0	-0.042
1.50	0.015	0	0.002



## DIAGONAL (POSITION 'B') DATA

X/D	PRESSURE CIN H2O3	ROTATION CDEG3	PHS4
0.00	-1.415	0	-0.194
0.25	-0.995	0	-0.137
0.50	-0.705	0	-0.097
0.75	-0.470	0	-0.065
1.00	-0.115	0	-0.016
1.25	-0.100	0	-0.014
1.50	-0.095	0	-0.001

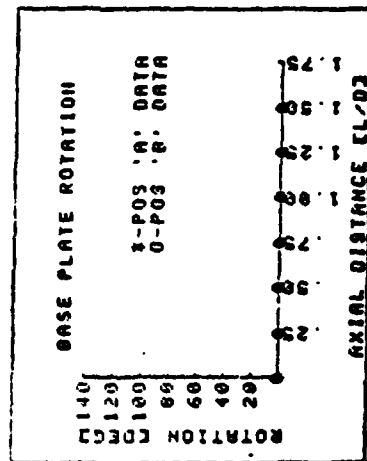
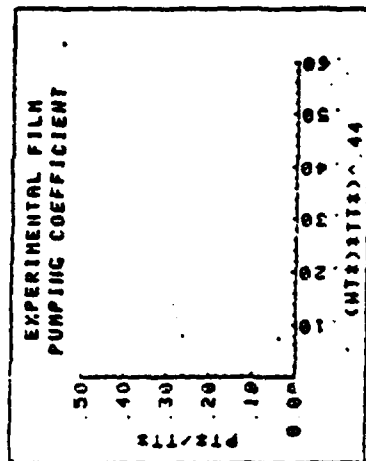


TABLE 8.1 - MSD DATA FOR 15/00 NOZZLES WITH L/D=1.75 MSD COMPARISON  
BASE PLATE FIXED AT 00 ROTATION

DATA TAKEN ON: 5 AUG 81  
 DATA TAKEN BY: C C DAVIS

NOZZLE AN/AP AREA RATIO: 2.50

COMMENTS:  
 COMPARISON OF ROTATION ANGLES

MIXING STACK INFORMATION:  
 LENGTH: 20.48 INCH  
 DIAMETER: 11.70 INCH  
 L/D RATIO: 1.75

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 15 DEGREE  
 ROTATION ANGLE: 0 DEGREE  
 AREA PER NOZZLE: 10.752 INCH2  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 INCH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 INCH2  
 ATM. PRESSURE: 30.00 INHG

N	POR	DPOR	TOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF W20	DEGREES F			IN OF W20				SQUARE INCHES	SQUARE INCHES
1	0.69	22.0	53.1	107.3	67.4	6.25	0.01	0.00	*****	*****

#### SECONDARY BOX

N	MS	PS	TS	PS/TS	WST	MP	MS	UP	UN	UOPT	UPT MACH
RUN											
1	*****	0.0007	0.9296	0.0007	*****	3.7702	1.9012	179.44	*****	71.70	0.062

#### TERTIARY BOX

N	MS	PT3	TT3	PT3/TT3	WST	MM	WT	UE
RUN								
1	*****	0.0000	0.9296	0.0000	*****	*****	*****	*****

TABLE 9 - PCD DATA FOR 15/00 NOZZLES WITH L/D=1.75 MSD COMPARISON  
 BASE PLATE ROTATED TO FIRST PEAK ONLY

# MIXING STAGE DATA FOR RUN 1

## TOP (POSITION 'A') DATA

X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PHS
0.00	-2.339	13	-0.327
0.25	-0.995	13	-0.137
0.50	-0.615	13	-9.084
0.75	-0.425	13	-0.058
1.00	-0.235	13	-0.032
1.25	-0.145	13	-0.020
1.50	0.015	13	0.002

## DIAGONAL (POSITION 'B') DATA

X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PHS
0.00	-1.650	13	-0.227
0.25	-0.870	13	-0.120
0.50	-0.605	13	-0.083
0.75	-0.295	13	-0.041
1.00	-0.075	13	-0.010
1.25	-0.100	13	-0.025
1.50	-0.065	13	-0.009

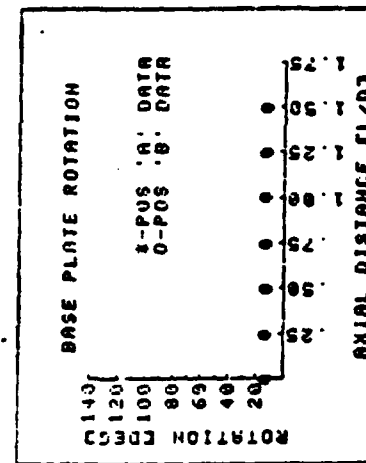
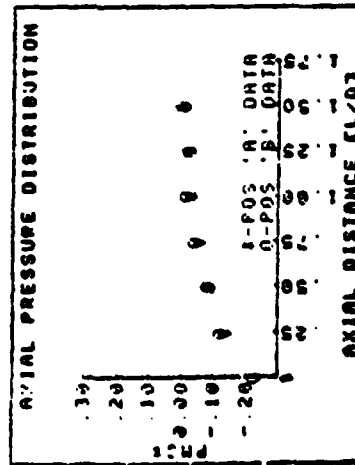
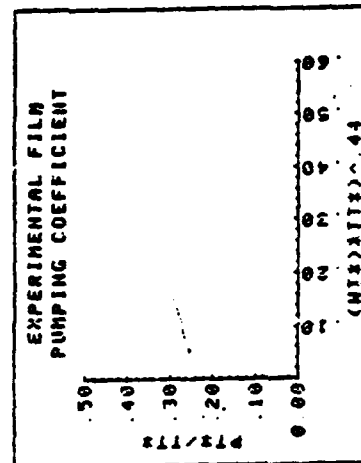
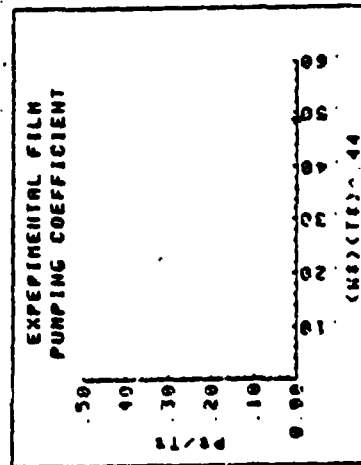


TABLE 9.1 - MSD DATA FOR 15/10 NOZZLES WITH L/D=1.75 MSD COMPARISON  
BASE PLATE ROTATED TO FIRST PEAK ONLY



DATA TAKEN ON: 5 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 20.46 CINH  
 DIAMETER: 11.70 CINH  
 L/D RATIO: 1.75  
 S/D RATIO: 0.50

NOZZLE AN AP AREA RATIO: 2.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 15 DEEG3  
 ROTATION ANGLE: 0 DEEG3  
 AREA PER NOZZLE: 10.752 CINH2  
 NUMBER OF NOZZLES: 4

COMMENTS:  
 COMPARISON OF POTATION ANGLES

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINH2  
 ATM PRESSURE: 30.00 CINHG3

N	FOR	UPOR	TOR	TUPT	TANG	PUP	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
IN OF H2O	DEGREES F				IN OF H2O				SQUARE INCHES	SQUARE INCHES
1	0.69	22.0	53.0	107.4	67.6	6.25	0.01	0.00	1111111	1111111

SECONDARY BOX

N	H2	P3	T3	P3/T3	WAT	44	WP	US	UP	UN	UOPT	UPT	MACH
								LBM/SEC	LBM/SEC	FT/SEC	FT/SEC		
1	1111111	0.0007	0.9290	0.0007	1111111	3.7705	1.3000	179.49	1111111	71.00	0.062		

TERTIARY BOX

N	MT3	PT3	IT3	PT3/IT3	WAT	44	WN	WT	UE	
								LBM/SEC	LBM/SEC	FT/SEC
1	1111111	0.0000	0.9290	0.0000	1111111	1111111	1111111	1111111	1111111	1111111

TABLE 10 - PCD DATA FOR 15/00 NOZZLES WITH L/D=1.75 MSD COMPARISON  
 BASE PLATE ROTATED FOR PEAKS AT EACH X/D POSITION

# MIXING STAGE DATA FOR RUN 1

TOP 'POSITION 'A' DATA:

X/D	PRESSURE CIN M203	ROTATION [DEG]	PHS*
0.50	-2.360	183	-0.327
0.75	-1.145	36	-0.157
0.50	-0.595	32	-0.094
0.75	-0.395	25	-0.054
1.00	-0.195	22	-0.027
1.25	-0.200	24	-0.030
1.50	0.155	32	0.021

DIAGONAL (POSITION 'B') DATA:

X/D	PRESSURE CIN M203	ROTATION [DEG]	PHS*
0.50	-1.595	183	-0.219
0.75	-0.605	36	-0.033
0.50	-0.355	32	-0.049
0.75	-0.215	25	-0.030
1.00	-0.095	22	-0.013
1.25	-0.250	24	-0.034
1.50	-0.070	32	-0.010

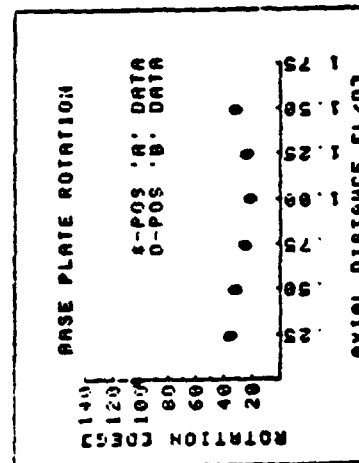
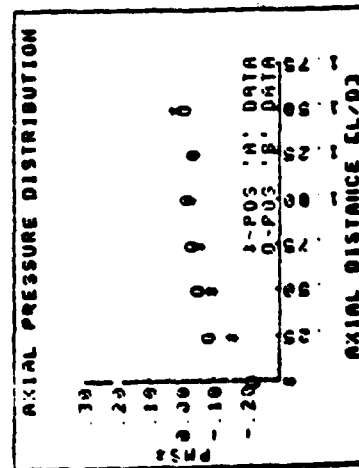
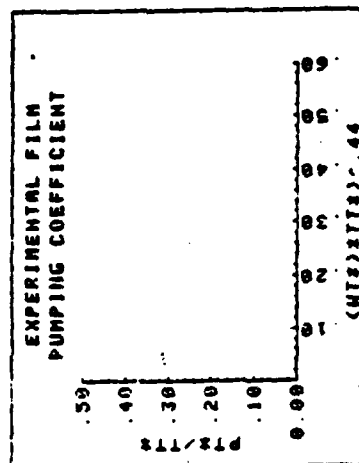
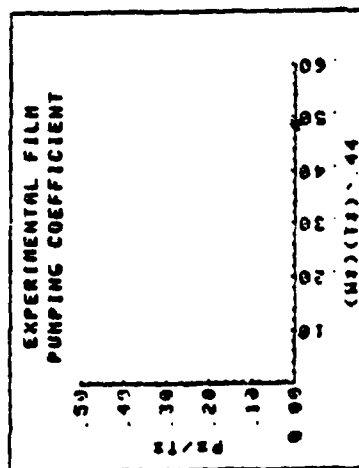


TABLE 10.1 - MSD DATA FOR 15/00 NOZZLES WITH L/D=1.75 MSD COMPARISON  
BASE PLATED ROTATED FOR PEAKS AT EACH X/D POSITION

DATA TAKEN ON: 10 AUG 81  
 DATA TAKEN BY: C. C. DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 20.48 CINH  
 DIAMETER: 11.78 CINH  
 L/D RATIO: 1.75  
 S/D RATIO: 0.50

NOZZLE AN/AP AREA RATIO: 2.50

COMMENTS:  
 15 TILT/10 ROTATION NOZZLES

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 15 IDEGJ  
 ROTATION ANGLE: 10 IDEGJ  
 AREA PER NOZZLE: 10.752 CINH2  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINH2  
 ATM. PRESSURE: 30.12 CINHGJ

M	POR	DFOP	TOP	TUFT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.70	22.2	57.0	111.0	71.4	3.45	3.10	0.00	0.000	1111111
2	0.70	22.1	57.2	111.0	71.4	4.25	2.21	0.00	12.566	1111111
3	0.70	22.0	56.4	110.0	71.6	4.80	1.57	0.00	25.133	1111111
4	0.70	22.1	56.4	110.4	71.6	5.45	0.88	0.00	50.265	1111111
5	0.70	22.0	56.0	110.2	71.0	5.95	0.35	0.00	100.531	1111111
6	0.70	22.0	56.0	110.2	71.0	6.05	0.19	0.00	150.796	1111111
7	0.70	22.0	56.2	110.2	72.2	6.15	0.11	0.00	201.062	1111111
8	0.70	22.0	56.2	110.2	72.2	5.20	0.07	0.00	245.044	1111111
9	0.70	22.0	56.0	110.4	72.4	6.25	0.00	0.00	3333333	1111111

SECONDARY BOX

M	H3	P3	T3	P3/T3	W3/T3	HP	HS	UP	UN	UUPT	UPT MACH
RUN						LBN/SEC	LBN/SEC	FT/SEC	FT/SEC	FT/SEC	
1	0.000	0.4153	0.9306	0.4476	0.0000	3.7754	0.0000	192.00	72.81	72.81	0.062
2	0.1634	0.2997	0.9206	0.3221	0.1611	3.7662	0.6379	181.16	83.63	72.47	0.052
3	0.2659	0.2145	0.9213	0.2303	0.2771	3.7605	1.0751	180.54	91.38	72.22	0.062
4	0.4271	0.1202	0.9319	0.1290	0.4140	3.7691	1.6097	180.52	100.89	72.21	0.062
5	0.5357	0.0473	0.9326	0.0509	0.5125	3.7620	2.0154	179.88	107.68	71.96	0.061
6	0.5964	0.0262	0.9326	0.0291	0.5703	3.7620	2.2435	179.81	111.92	71.93	0.061
7	0.5049	0.0152	0.9333	0.0163	0.5860	3.7613	2.2752	179.74	112.48	71.90	0.061
8	0.5081	0.0097	0.9333	0.0103	0.5705	3.7613	2.2120	179.73	111.35	71.90	0.061
9	0.0000	0.0001	0.9333	0.0001	0.0000	3.7591	0.0460	179.66	3333333	71.07	0.061

TABLE 11 - PCD DATA FOR 15/10 NOZZLES WITH L/D=1.75 STACK

TEMPERATURE BOX

RUN	M	HT	PT	IT	PI	IT	HT	UE
1	00000	0	0000	0	9306	0	0000	
2	00000	0	0000	0	9306	0	0000	
3	00000	0	0000	0	9313	0	0000	
4	00000	0	0000	0	9319	0	0000	
5	00000	0	0000	0	9326	0	0000	
6	00000	0	0000	0	9326	0	0000	
7	00000	0	0000	0	9333	0	0000	
8	00000	0	0000	0	9333	0	0000	
9	00000	0	0000	0	9333	0	0000	

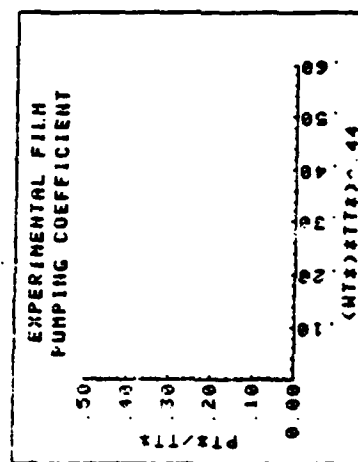
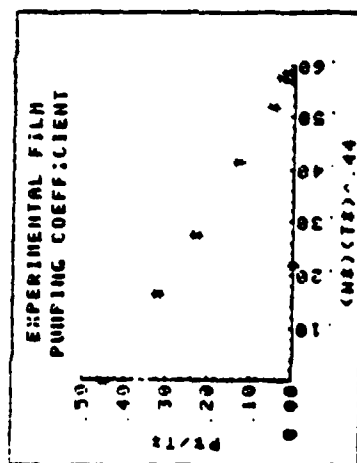


TABLE 11.1 - PCD DATA (CONT) FOR 15/10 NOZZLES WITH L/D=1.75

# MIXING STAGE DATA FOR RUN 9

## TOP (POSITION 'A') DATA

X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PHSA	X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PHSA
0.00	-2.160	96	-0.298	0.00	-1.595	96	-0.220
0.25	-1.040	34	-0.144	0.25	-0.845	34	-0.117
0.50	-0.835	29	-0.115	0.50	-0.585	29	-0.041
0.75	-0.655	27	-0.090	0.75	-0.445	27	-0.061
1.00	-0.385	32	-0.053	1.00	-0.225	32	-0.031
1.25	-0.315	36	-0.044	1.25	-0.235	36	-0.032
1.50	0.145	38	0.020	1.50	-0.100	38	-0.014

## DIAGONAL (POSITION 'B') DATA

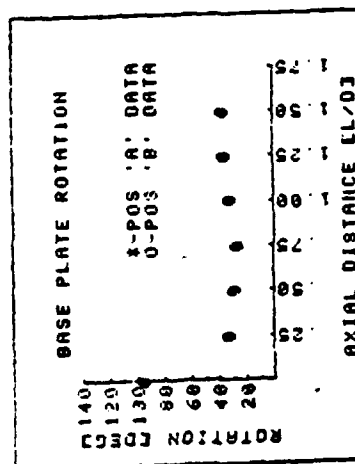
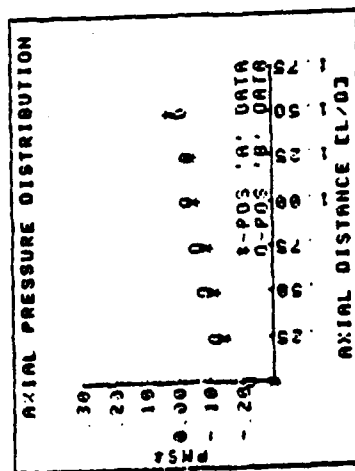
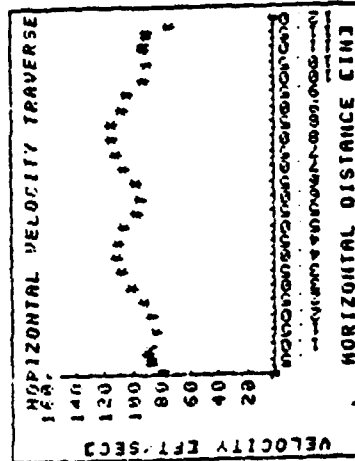
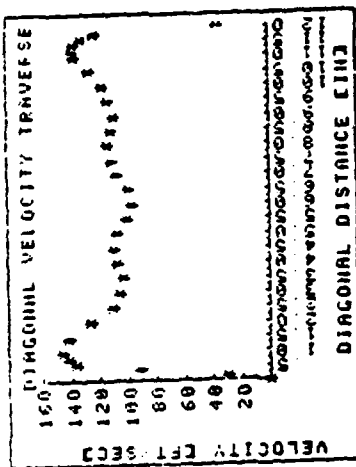


TABLE 11.2 - MSD DATA FOR 15/10 NOZZLES WITH L/D=1.75



WIND TUNNEL VELOCITY TRAVERSE HT	BASE POSITION OF 07 DEGREES	BASE POSITION OF 07 DEGREES
POSITIVE INJ: 0.00	0.20	0.40
PEIN M203: 0.00	1.40	1.70
VEFT/SEC3: 0.00	79.01	87.07
POSITIVE INJ: 2.00	2.50	3.00
PEIN M203: 1.70	1.90	2.30
VEFT/SEC3: 87.07	92.05	101.27
POSITIVE INJ: 5.50	6.00	6.50
PEIN M203: 2.10	2.00	2.10
VEFT/SEC3: 96.77	94.44	96.77
POSITIVE INJ: 9.00	9.50	10.00
PEIN M203: 2.60	2.40	1.90
VEFT/SEC3: 107.67	103.45	92.05
POSITIVE INJ: 11.60	11.80	12.00
PEIN M203: 1.60	1.20	0.60

DIAGONAL VELOCITY TRAVERSE FOR	BASE POSITION OF 07 DEGREES	BASE POSITION OF 07 DEGREES
POSITIVE INJ: 0.00	0.20	0.40
PEIN M203: 0.00	0.20	1.90
VEFT/SEC3: 0.00	23.86	92.05
POSITIVE INJ: 2.00	2.50	3.00
PEIN M203: 3.60	2.80	2.50
VEFT/SEC3: 126.79	111.74	105.58
POSITIVE INJ: 5.50	6.00	6.50
PEIN M203: 2.50	2.10	2.20
VEFT/SEC3: 101.27	96.77	99.05
POSITIVE INJ: 9.00	9.50	10.00
PEIN M203: 2.70	2.90	3.10
VEFT/SEC3: 109.73	113.72	117.57
POSITIVE INJ: 11.60	11.80	12.00
PEIN M203: 3.90	3.40	0.30

TABLE 11.3 - VTD DATA FOR 15/10 NOZZLES WITH L/D-1.75 STACK

DATA TAKEN ON: 10 AUG 51  
 DATA TAKEN BY: C. C. DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 20.48 INJ  
 DIAMETER: 11.70 INJ  
 L/D RATIO: 1.75  
 S/D RATIO: 0.50

NOZZLE AN/AP AREA RATIO: 2.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 15 IDEGJ  
 ROTATION ANGLE: 20 IDEGJ  
 AREA PER NOZZLE: 10.752 INH2J  
 NUMBER OF NOZZLES: 4

COMMENTS:  
 15 TILT/20 POTATION NOZZLES

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 INJ  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 INH2J  
 ATM. PRESSURE: 30.12 INHGJ

N	POP	DPOR	TOR	TUPT	TANG	PUP	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F					IN OF H2O		SQUARE INCHES	SQUARE INCHES
1	0.69	22.0	56.2	110.6	72.0	3.25	3.11	0.00	0.000	0.000
2	0.69	21.9	56.6	110.8	72.2	4.15	2.22	0.00	12.566	0.000
3	0.70	22.0	55.0	110.4	72.6	4.80	1.62	0.00	25.133	0.000
4	0.70	22.0	55.0	110.0	72.4	5.40	0.94	0.00	50.265	0.000
5	0.69	22.0	55.6	110.2	72.4	5.95	0.34	0.00	100.531	0.000
6	0.69	22.0	55.2	110.2	72.4	6.15	0.22	0.00	150.796	0.000
7	0.70	22.0	55.0	110.2	72.4	6.20	0.16	0.00	201.062	0.000
8	0.70	22.0	55.4	110.2	72.4	6.25	0.12	0.00	245.044	0.000
9	0.70	22.0	56.2	110.4	72.4	6.30	0.00	0.00	0.000	0.000

N	MR	PS	TS	FS/TS	MT/TS	HP	HS	UP	UH	UUP	UPT	MACH
RUN							LBH/SEC	LBH/SEC	FT/SEC	FT/SEC		
1	0.0030	0.4221	0.9323	0.4527	0.0390	3.7613	0.0000	181.20	72.48	72.49	0.062	
2	0.1703	0.3041	0.9333	0.3262	0.1651	3.7513	0.6338	180.39	83.55	72.16	0.062	
3	0.2997	0.2214	0.9337	0.2371	0.2811	3.7656	1.0910	180.68	91.75	72.28	0.062	
4	0.4403	0.1283	0.9340	0.1374	0.4273	3.7656	1.6580	180.25	101.69	72.11	0.062	
5	0.5313	0.0468	0.9337	0.0501	0.5155	3.7635	1.9996	179.95	107.67	71.99	0.062	
6	0.6408	0.0303	0.9337	0.0324	0.6210	3.7650	2.4128	179.97	115.04	71.99	0.062	
7	0.7171	0.0213	0.9337	0.0229	0.6957	3.7657	2.7003	179.97	120.10	72.00	0.062	
8	0.7531	0.0150	0.9337	0.0170	0.7307	3.7642	2.8347	179.89	122.54	71.96	0.061	
9	0.80028	0.0006	0.9333	0.0006	0.80028	3.7613	1.6936	179.76	0.000	0.000	0.061	

TABLE 12 - PCD DATA FOR 15/20 NOZZLES WITH L/D=1.75 STACK

TERTIARY BOX

N	WT	PT	IT	PT/IT	WT/IT	44	UM	WT	UE
RUN							LBM/SEC	LBM/SEC	FT/SEC
1	0.0000	0.0000	0.9323	0.0000	0.0000	0.0000	3.761	0.0000	0.0000
2	0.0000	0.0000	0.9323	0.0000	0.0000	0.0000	4.390	0.0000	0.0000
3	0.0000	0.0000	0.9337	0.0000	0.0000	0.0000	4.857	0.0000	0.0000
4	0.0000	0.0000	0.9349	0.0000	0.0000	0.0000	5.424	0.0000	0.0000
5	0.0000	0.0000	0.9337	0.0000	0.0000	0.0000	5.763	0.0000	0.0000
6	0.0000	0.0000	0.9337	0.0000	0.0000	0.0000	6.178	0.0000	0.0000
7	0.0000	0.0000	0.9337	0.0000	0.0000	0.0000	6.466	0.0000	0.0000
8	0.0000	0.0000	0.9337	0.0000	0.0000	0.0000	6.599	0.0000	0.0000
9	0.0000	0.0000	0.9333	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

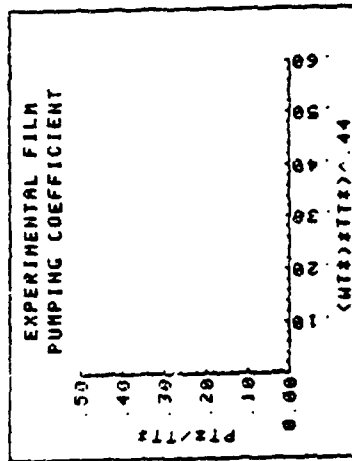
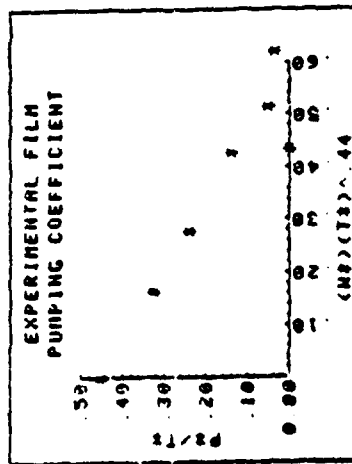


TABLE 12.1 - PCD DATA (CONT) FOR 15/20 NOZZLES WITH L/D=1.75 STACK



# MIXING STACK DATA FOR RUN 9

## TOP (POSITION 'A') DATA

X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PHSA	X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PHSA
0.00	-2.270	92	-0.313	0.00	-1.710	92	-0.236
0.25	-1.150	30	-0.159	0.25	-1.010	30	-0.139
0.50	-0.935	26	-0.129	0.50	-0.790	26	-0.109
0.75	-0.765	24	-0.106	0.75	-0.565	24	-0.078
1.00	-0.530	24	-0.073	1.00	-0.385	24	-0.053
1.25	-0.375	25	-0.052	1.25	-0.315	25	-0.043
1.50	-0.075	24	-0.010	1.50	-0.150	24	-0.021

## DIAGONAL (POSITION 'B') DATA

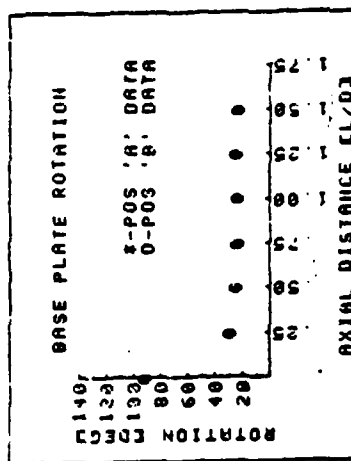
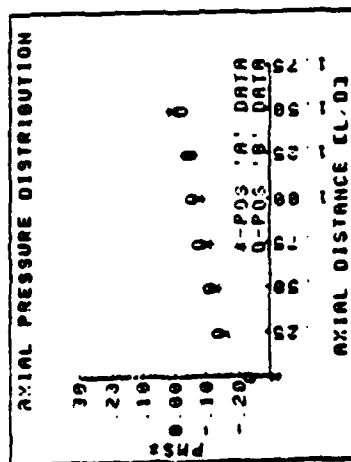
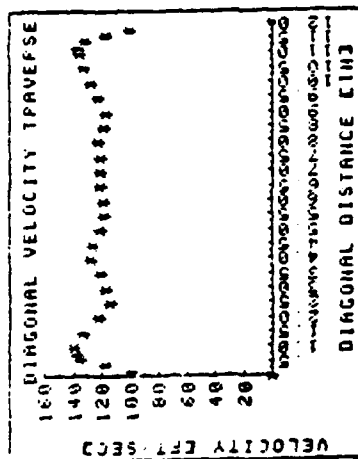


TABLE 12.2 - MSD DATA FOR 15/20 NOZZLES WITH L/D=1.75 STACK

HORIZONTAL VELOCITY TRAVERSE AT BASE ROTATION OF 05 DEGREES

POSITION	0 00	0 20	0 40	0 60	0 80	1 00	1 50
FLIN H203	0 00	0 30	1 10	1 20	1 30	1 20	1 30
VEFT/SEC3	0 00	59 73	70 04	73 15	76 14	73 15	76 14
POSITION	2 00	2 50	3 00	3 50	4 00	4 50	5 00
FLIN H203	1 50	2 20	3 00	3 50	3 80	3 70	3 30
VEFT/SEC3	91 72	99 05	115 66	124 33	130 17	128 15	121 31
POSITION	5 50	6 00	6 50	7 00	7 50	8 00	8 50
FLIN H203	3 10	3 60	3 10	3 30	3 40	3 30	2 70
VEFT/SEC3	117 57	115 66	117 57	121 31	123 13	121 31	119 73
POSITION	9 00	9 50	10 00	10 50	11 00	11 20	11 40
FLIN H203	2 10	1 60	1 60	1 50	1 60	1 50	1 50
VEFT/SEC3	96 77	89 59	84 47	81 78	84 47	81 78	81 78
POSITION	11 60	11 80	12 00				
FLIN H203	1 30	0 30	0 00				



DIAGONAL VELOCITY TRAVERSE FOR BASE ROTATION OF 05 DEGREES

POSITION	0 00	0 20	0 40	0 60	0 80	1 00	1 50
FLIN H203	0 00	2 20	3 10	4 10	4 30	4 40	4 00
VEFT/SEC3	0 00	99 05	117 57	135 21	139 47	140 07	133 55
POSITION	2 00	2 50	3 00	3 50	4 00	4 50	5 00
FLIN H203	3 40	3 00	3 10	3 30	3 70	3 60	3 30
VEFT/SEC3	123 17	115 66	117 57	121 31	128 45	126 70	121 31
POSITION	5 50	6 00	6 50	7 00	7 50	8 00	8 50
FLIN H203	3 20	3 20	3 30	3 30	3 30	3 40	3 20
VEFT/SEC3	119 45	119 45	121 31	121 31	121 31	123 13	119 45
POSITION	9 00	9 50	10 00	10 50	11 00	11 20	11 40
FLIN H203	3 10	3 40	3 70	4 00	4 10	4 20	3 90
VEFT/SEC3	117 57	123 13	128 45	133 55	135 21	136 85	131 87
POSITION	11 60	11 80	12 00				
FLIN H203	3 10	2 30	0 00				

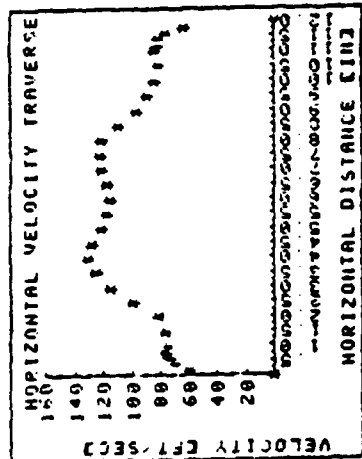


TABLE 12.3 - VTD DATA FOR 15/20 NOZZLES WITH L/D=1.75 STACK

DATA WHEN ON: 12 AUG 81  
 DATA WHEN BY: C C. DAVIS  
 NOZZLE AN/AP AREA RATIO: 2.50  
 15 TILT 25 ROTATION/ 5 S/D RATIO  
 COMMENTS:  
 MIXING STACK INFORMATION:  
 LENGTH: 20.48 CINH  
 DIAMETER: 11.70 CINH  
 L/D RATIO: 1.75  
 S/D RATIO: 0.50  
 PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 15 CDEG  
 ROTATION ANGLE: 25 CDEG  
 AREA PER NOZZLE: 10.752 CINH2  
 NUMBER OF NOZZLES: 4  
 MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINH2  
 ATM PRESSURE: 29.92 CINHG

N	POP	LPOR	TOR	TUPT	TANB	PUPT	PSEC	PTER	SECONDARY AREA SQUARE INCHES	TERTIARY AREA SQUARE INCHES
RUN	IN OF H2O	DEGREES F	IN OF H2O	IN OF H2O	IN OF H2O	IN OF H2O	IN OF H2O	IN OF H2O	IN OF H2O	IN OF H2O
1	0.70	22.1	57.2	110.6	69.6	3.25	3.10	0.00	0.000	0.000
2	0.70	22.0	57.2	110.6	63.6	4.15	2.21	0.00	12.566	0.000
3	0.69	22.0	57.8	110.6	69.2	4.70	1.59	0.00	25.133	0.000
4	0.70	22.1	57.2	110.6	70.2	5.45	0.89	0.00	50.265	0.000
5	0.70	22.1	58.6	111.2	70.6	5.95	0.34	0.00	100.531	0.000
6	0.70	22.0	56.6	111.4	70.6	6.10	0.19	0.00	150.796	0.000
7	0.70	22.0	58.0	111.2	70.6	6.15	0.13	0.00	201.062	0.000
8	0.70	22.0	58.2	111.4	70.6	6.25	0.07	0.00	245.044	0.000
9	0.70	22.0	50.0	111.2	70.0	6.30	0.03	0.00	0.000	0.000

# SECONDARY BOX

N	HP	Tt	Pt	Wt	Wt	Wt	Wt	Wt	Wt	Wt
RUN	Wt	Wt	Wt	Wt	Wt	Wt	Wt	Wt	Wt	Wt
1	0.0000	0.4169	0.9264	0.4501	0.0000	3.7536	0.0000	102.04	72.82	72.82
2	0.1702	0.2939	0.9264	0.3237	0.1646	3.7451	0.6374	181.23	83.86	72.50
3	0.2687	0.2169	0.9274	0.2339	0.2793	3.7430	1.0807	180.85	91.64	72.35
4	0.4304	0.1214	0.9292	0.1306	0.4167	3.7536	1.6156	181.05	101.33	72.43
5	0.5326	0.0466	0.9289	0.0501	0.5156	3.7482	1.9964	180.75	108.04	72.31
6	0.5295	0.0261	0.9286	0.0281	0.5793	3.7401	2.2386	180.34	112.22	72.14
7	0.6597	0.0179	0.9269	0.0192	0.6367	3.7422	2.4689	180.35	116.34	72.15
8	0.5901	0.0096	0.9286	0.0104	0.5712	3.7415	2.2000	180.36	111.67	72.15
9	0.0000	0.0001	0.9292	0.0044	0.0000	3.7422	4.6297	180.31	0.0000	72.15

TABLE 13 - PCD DATA FOR 15/25 NOZZLES WITH L/D=1.75 AND S/D=0.5 STACK

TERTIARY BOX

N	HT	PT	TT	PT	TT	HT	UE
RUN							
1	0.0000	0.0000	0.9264	0.0000	0.0000	3.754	0.0000
2	0.0000	0.0000	0.9264	0.0000	0.0000	4.383	0.0000
3	0.0000	0.0000	0.9274	0.0000	0.0000	4.824	0.0000
4	0.0000	0.0000	0.9292	0.0000	0.0000	5.369	0.0000
5	0.0000	0.0000	0.9289	0.0000	0.0000	5.745	0.0000
6	0.0000	0.0000	0.9286	0.0000	0.0000	5.979	0.0000
7	0.0000	0.0000	0.9289	0.0000	0.0000	6.211	0.0000
8	0.0000	0.0000	0.9286	0.0000	0.0000	5.949	0.0000
9	0.0000	0.0000	0.9292	0.0000	0.0000	6.211	0.0000

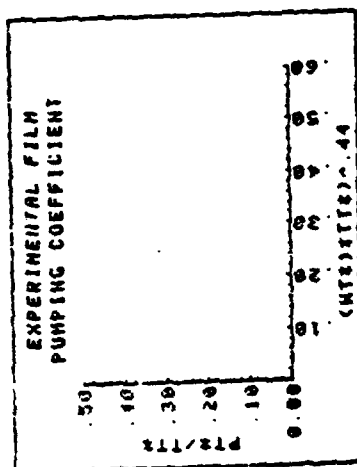
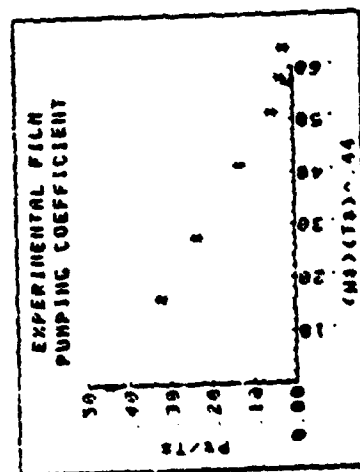


TABLE 13.1 - PCD DATA (CONT) FOR 15/25 NOZZLES WITH L/D=1.75 AND S/D=0.5 STACK

# MIXING STACK DATA FOR RUN 9

## TOP POSITION 'A' DATA

X/D	PRESSURE CIN H2O3	ROTATION CDEG	PHSE
0.29	-2.209	92	-0.303
0.25	-1.230	28	-0.169
0.50	-0.970	24	-0.134
0.75	-0.810	16	-0.112
1.00	-0.620	18	-0.085
1.25	-0.455	19	-0.063
1.50	-0.045	20	-0.006

## DIAGONAL (POSITION 'B') DATA

X/D	PRESSURE CIN H2O3	ROTATION CDEG	PHSE
0.00	-1.690	92	-0.233
0.25	-1.030	28	-0.142
0.50	-0.090	24	-0.121
0.75	-0.615	16	-0.085
1.00	-0.485	18	-0.056
1.25	-0.335	19	-0.046
1.50	-0.105	20	-0.025

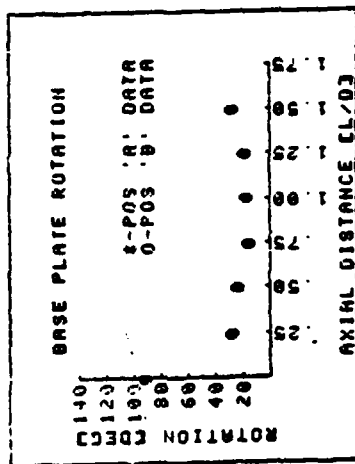
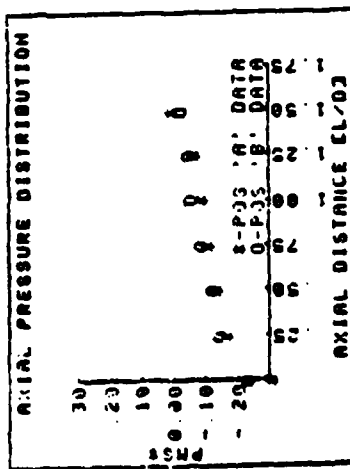
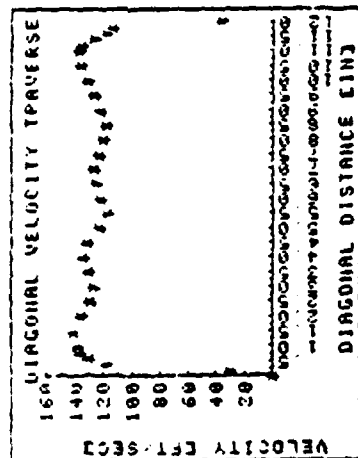


TABLE 13.2 - MSD DATA FOR 15/25 NOZZLES WITH L/D=1.75 AND S/D=0.5 STACK

NOZZLE: 15/25 VELOCITY TRAVERSE HT BASE ROTATION OF 84 DEGREES

POSITION	0.00	0.20	0.40	0.60	0.80	1.00	1.50
PEIN M203	0.00	1.00	1.30	1.40	1.40	1.50	1.30
VEFT/SEC3	0.00	66.90	76.28	79.16	79.16	81.93	76.23
POSITION	2.00	2.50	3.00	3.50	4.00	4.50	5.00
PEIN M203	1.40	1.70	2.00	2.50	4.10	4.00	3.70
VEFT/SEC3	79.15	87.23	107.87	125.16	135.46	133.89	128.68
POSITION	5.50	6.00	6.50	7.00	7.50	8.00	8.50
PEIN M203	3.10	3.20	3.50	3.80	3.70	3.60	2.80
VEFT/SEC3	117.79	119.67	125.16	130.41	128.63	126.93	111.94
POSITION	9.00	9.50	10.00	10.50	11.00	11.20	11.40
PEIN M203	2.20	1.60	1.50	1.50	1.60	1.70	1.70
VEFT/SEC3	99.23	84.62	81.93	81.93	84.62	87.23	87.23
POSITION	11.60	11.80	12.00				
PEIN M203	1.40	0.90	0.10				



NOZZLE: 15/25 VELOCITY TRAVERSE FOR BASE ROTATION OF 84 DEGREES

POSITION	0.00	0.20	0.40	0.60	0.80	1.00	1.50
PEIN M203	0.00	0.20	3.10	3.80	4.20	4.30	4.40
VEFT/SEC3	0.00	29.92	117.79	130.41	137.10	138.72	140.33
POSITION	2.00	2.50	3.00	3.50	4.00	4.50	5.00
PEIN M203	4.10	3.70	3.60	3.80	4.00	3.90	3.40
VEFT/SEC3	135.46	128.68	126.93	130.41	133.80	132.11	123.36
POSITION	5.50	6.00	6.50	7.00	7.50	8.00	8.50
PEIN M203	3.10	3.30	3.50	3.60	3.40	3.20	3.10
VEFT/SEC3	117.79	121.53	125.16	126.93	123.36	119.67	117.79
POSITION	9.00	9.50	10.00	10.50	11.00	11.20	11.40
PEIN M203	3.30	3.60	2.80	4.10	4.20	4.10	3.60
VEFT/SEC3	121.53	126.93	130.41	135.46	137.10	135.46	126.93
POSITION	11.60	11.80	12.00				
PEIN M203	3.10	2.90	0.30				

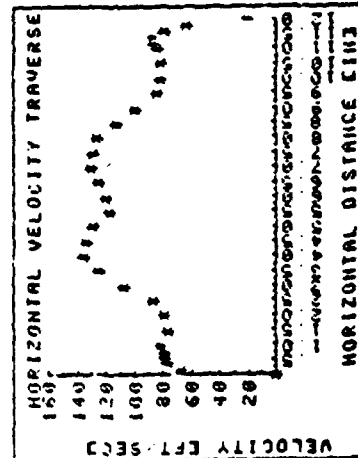


TABLE 13.3 - VTD DATA FOR 15/25 NOZZLES WITH L/D=1.75 AND S/D=0.5 STACK

DATA TAKEN ON: 12 AUG 91  
 DATA TAKEN BY: DAVIS/DPUCKER

NOZZLE AN/AP AREA RATIO: 2.50  
 COMMENTS:  
 15 TILT/25 ROTATE/ 4 S/D RATIO

MIXING STACK INFORMATION:  
 LENGTH: 20.40 EINH  
 DIAMETER: 11.70 EINH  
 L/D RATIO: 1.75  
 S/D RATIO: 0.40

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 15 DEEG  
 ROTATION ANGLE: 25 DEEG  
 AREA PER NOZZLE: 10.752 EINH  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 EINH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 EINH  
 ATM PRESSURE: 29.94 EINH

N	POR	DPOR	TOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F					IN OF H2O		SQUARE INCHES	SQUARE INCHES
1	0.70	22.1	56.2	110.0	60.0	3.25	3.13	0.00	0.000	0.000
2	0.70	22.0	56.2	110.0	60.2	4.10	2.23	0.00	12.566	0.000
3	0.70	22.0	56.4	110.0	69.0	4.75	1.61	0.00	25.133	0.000
4	0.70	22.1	56.0	110.2	69.4	5.40	0.90	0.00	50.265	0.000
5	0.69	22.0	57.0	110.4	69.4	5.90	0.34	0.00	100.531	0.000
6	0.70	22.0	56.4	110.4	69.6	6.05	0.19	0.00	150.796	0.000
7	0.70	22.0	56.8	110.4	70.0	6.10	0.12	0.00	201.062	0.000
8	0.70	22.0	56.8	110.4	70.0	6.15	0.08	0.00	245.044	0.000
9	0.70	22.0	56.6	110.4	70.0	6.20	0.02	0.00	0.000	0.000

# SECONDARY BOX

N	WE	PS	TS	P+TS	WAT	HP	WS	UP	UM	UPT	UPT	MACH
RUN							LBM/SEC	LBM/SEC	FT/SEC	FT/SEC	FT/SEC	
1	0.0000	0.4205	0.9263	0.4540	0.0000	3.7532	0.0000	181.99	72.80	72.80	0.062	
2	0.1090	0.3024	0.9266	0.7263	0.1652	3.7497	0.6307	181.18	83.89	72.48	0.062	
3	0.2902	0.2194	0.9280	0.2364	0.2808	3.7489	1.0380	180.87	91.76	72.35	0.062	
4	0.4330	0.1226	0.9284	0.1321	0.4191	3.7560	1.6263	180.95	101.42	72.39	0.062	
5	0.5336	0.0466	0.9281	0.0503	0.5163	3.7468	1.9991	180.32	107.82	72.14	0.062	
6	0.5976	0.0261	0.9284	0.0281	0.5786	3.7489	2.2412	180.36	112.18	72.15	0.062	
7	0.6335	0.0165	0.9291	0.0170	0.6133	3.7475	2.3740	180.26	114.54	72.11	0.062	
8	0.6304	0.0110	0.9291	0.0110	0.6103	3.7475	2.3624	180.24	114.32	72.10	0.062	
9	0.0000	0.0027	0.9291	0.0030	0.0000	3.7402	3.7039	180.25	0.0000	72.11	0.062	

TABLE 14 - PCD DATA FOR 15/25 NOZZLES WITH L/D=1.75 AND S/D=0.4 STACK

TERTIARY BOX

N	MT	PTS	ITS	PTS/ITS	MT/ITS	MT	UE
LBM/SEC LBM/SEC FT/SEC							
RUN							
1	00000	0.0000	0.9263	0.0000	0.0000	3.758	0.0000
2	00000	0.0000	0.9266	0.0000	0.0000	4.390	0.0000
3	00000	0.0000	0.9280	0.0000	0.0000	4.837	0.0000
4	00000	0.0000	0.9284	0.0000	0.0000	5.382	0.0000
5	00000	0.0000	0.9281	0.0000	0.0000	5.746	0.0000
6	00000	0.0000	0.9284	0.0000	0.0000	5.990	0.0000
7	00000	0.0000	0.9291	0.0000	0.0000	6.121	0.0000
8	00000	0.0000	0.9291	0.0000	0.0000	6.110	0.0000
9	00000	0.0000	0.9291	0.0000	0.0000	0.0000	0.0000

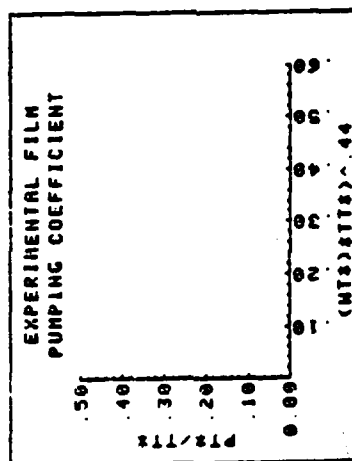
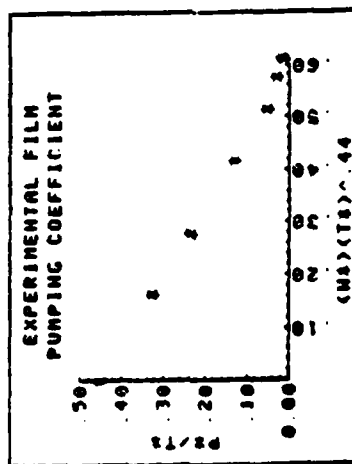


TABLE 14.1 - PCD DATA (CONT) FOR 15/25 NOZZLES WITH L/D=1.75 AND S/D=0.4 STACK



# MIXING STACK DATA FOR RUN 9

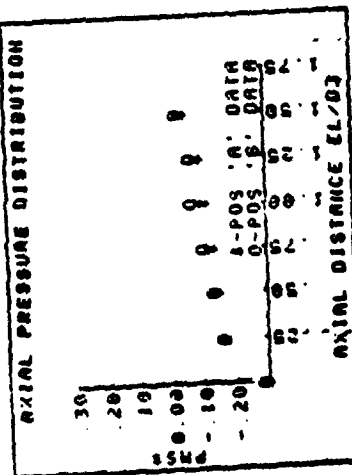
## TOP (POSITION 'A') DATA

X/D	PRESSURE LIN H2O3	ROTATION EDEC3	PHS4
0.00	-2.110	115	-0.290
0.25	-1.210	24	-0.166
0.50	-1.010	20	-0.139
0.75	-0.910	18	-0.125
1.00	-0.770	20	-0.106
1.25	-0.605	24	-0.083
1.50	-0.256	14	-0.034

## DIAGONAL (POSITION 'B') DATA

X/D	PRESSURE LIN H2O3	ROTATION EDEC3	PHS4
0.00	-2.062	115	-0.293
0.25	-1.150	24	-0.159
0.50	-0.930	20	-0.120
0.75	-0.705	18	-0.097
1.00	-0.465	20	-0.064
1.25	-0.415	24	-0.057
1.50	-0.145	14	-0.020

## AXIAL PRESSURE DISTRIBUTION



## BASE PLATE ROTATION

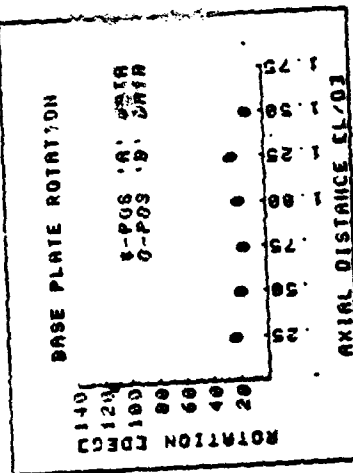
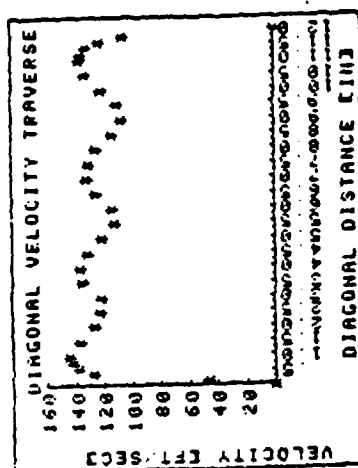
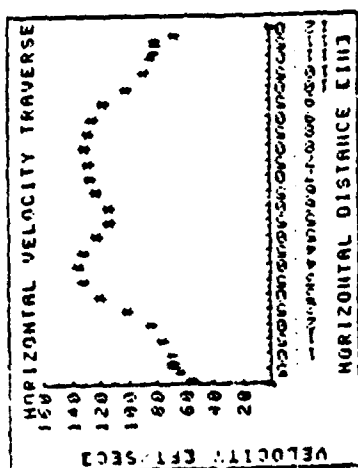


TABLE 14.2 - MSD DATA FOR 15/25 NOZZLES WITH L/D-1.75 AND S/D-0.4 STACK



HORIZONTAL VELOCITY TRAVERSE AT BASE ROTATION OF 90 DEGREES									
POSITION	0 00	0 20	0 40	0 60	0 80	1 00	1 20	1 40	1 50
PEIN H203	0 00	0 70	0 90	1 00	1 10	1 10	1 10	1 30	
VEFT/SEC	0 00	55 92	63 40	66 83	70 09	70 09	70 09	76 20	
POSITION	2 00	2 50	3 00	3 50	4 00	4 50	5 00	5 00	
PEIN H203	1 60	2 30	3 20	3 90	4 10	3 90	3 40	3 40	
VEFT/SEC	84 54	101 36	119 55	131 98	135 32	131 98	123 23	123 23	
POSITION	5 50	6 00	6 50	7 00	7 50	8 00	8 50	8 50	
PEIN H203	5 50	6 00	6 50	7 00	7 50	8 00	8 50	8 50	
VEFT/SEC	113 81	113 81	123 23	126 20	128 55	130 28	128 55	128 55	
POSITION	9 00	9 50	10 00	10 50	11 00	11 20	11 40	11 40	
PEIN H203	3 50	3 10	2 30	1 80	1 60	1 50	1 50	1 50	
VEFT/SEC	125 03	117 67	101 36	89 66	84 54	81 85	81 85	81 85	
POSITION	11 60	11 80	12 00						
PEIN H203	1 50	1 00	0 00						

DIAGONAL VELOCITY TRAVERSE FOR BASE ROTATION OF 98 DEGREES									
POSITION	0 00	0 20	0 40	0 60	0 80	1 00	1 20	1 40	1 50
PEIN H203	0 00	0 50	3 70	4 30	4 50	4 70	4 70	4 20	
VEFT/SEC	0 00	47 26	128 55	138 58	141 77	144 89	136 96	136 96	
POSITION	2 00	2 50	3 00	3 50	4 00	4 50	5 00	5 00	
PEIN H203	3 60	3 40	3 30	4 10	4 20	3 90	3 30	3 30	
VEFT/SEC	126 80	123 23	121 41	135 32	136 96	131 98	121 41	121 41	
POSITION	5 50	6 00	6 50	7 00	7 50	8 00	8 50	8 50	
PEIN H203	2 80	2 90	3 50	3 90	3 80	3 50	2 90	2 90	
VEFT/SEC	111 83	113 81	125 03	131 98	130 28	125 03	113 81	113 81	
POSITION	9 00	9 50	10 00	10 50	11 00	11 20	11 40	11 40	
PEIN H203	2 60	2 70	3 30	4 00	4 20	4 10	3 90	3 90	
VEFT/SEC	107 76	109 82	121 41	133 66	136 96	135 32	131 98	131 98	
POSITION	11 60	11 80	12 00						
PEIN H203	3 40	2 50	0 00						

TABLE 14.3 - VTD DATA FOR 15/25 NOZZLES WITH L/D=1.75 AND S/D=0.4 STACK

DATA TAKEN ON: 13 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

NOZZLE AN/AP AREA RATIO: 2.50  
 15 TILT/25 ROTATE/0.25 S/D RATIO

MIXING STACK INFORMATION:  
 LENGTH: 29.49 INJ  
 DIAMETER: 11.70 INJ  
 L/D RATIO: 1.75  
 S/D RATIO: 0.25

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 15 DEGS  
 ROTATION ANGLE: 25 DEGS  
 AREA PER NOZZLE: 10.752 INJ  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 OFFICE DIAMETER: 6.902 INJ  
 OFFICE BETA: 0.497  
 UPTAKE AREA: 107.510 INJ  
 ATM PRESSURE: 29.99 INJ

N	POP	DPOR	TOR	TUPT	TANG	TUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
SUM	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.71	22.0	57.2	110.0	69.0	3.25	3.11	0.00	0.000	8111111
2	0.71	22.0	57.6	111.0	68.0	4.10	2.21	0.00	12.566	8111111
3	0.70	22.0	57.0	111.0	69.2	4.65	1.57	0.00	25.133	8111111
4	0.70	22.0	58.0	111.4	69.4	5.35	0.03	0.00	50.265	8111111
5	0.70	22.1	58.2	111.0	69.4	5.05	0.29	0.00	100.531	8111111
6	0.70	22.2	58.2	112.0	70.0	5.95	0.16	0.00	150.796	8111111
7	0.70	22.2	58.2	111.0	70.2	6.10	0.02	0.00	8111111	8111111

# SECONDARY BOX

N	WS	P	T	P	14	WT	44	HP	WS	HP	UM	UUMT	UPT	NACH
SUM									LBH/SEC	LBH/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC
1	0.0000	0.4202	0.9267	0.4534	0.0000	3.7495	0.0000	181.48	72.60	72.60	0.062	0.062	0.062	0.062
2	0.1702	0.2993	0.9261	0.3239	0.1646	3.7480	0.6380	181.07	83.79	72.44	0.062	0.062	0.062	0.062
3	0.2069	0.2139	0.9268	0.2308	0.2775	3.7473	1.0752	180.79	91.46	72.31	0.062	0.062	0.062	0.062
4	0.4172	0.1134	0.9265	0.1224	0.4034	3.7466	1.5632	180.52	100.07	72.21	0.062	0.062	0.062	0.062
5	0.4322	0.0395	0.9258	0.0427	0.4756	3.7544	1.0480	180.70	105.25	72.32	0.062	0.062	0.062	0.062
6	0.5969	0.0217	0.9265	0.0235	0.5280	3.7629	2.0570	181.19	109.19	72.40	0.062	0.062	0.062	0.062
7	0.0000	0.0027	0.9272	0.0029	0.0000	3.7629	3.7067	181.07	8111111	72.43	0.062	0.062	0.062	0.062

TABLE 15 - PCD DATA FOR 15/25 NOZZLES WITH L/D=1.75 AND S/D=0.25 STACK

TEPTIARY BOX

N	WT	PTS	TIS	PIA/TIS	WSTIT	44	NM	MT	UE
LBM/SEC LBM/SEC FT/SEC									
1	100000	0.0000	0.9267	0.0000	100000	3.749	100000	100000	100000
2	100000	0.0000	0.9261	0.0003	100000	4.386	100000	100000	100000
3	100000	0.0000	0.9260	0.0000	100000	4.822	100000	100000	100000
4	100000	0.0000	0.9265	0.0000	100000	5.310	100000	100000	100000
5	100000	0.0000	0.9258	0.0000	100000	5.602	100000	100000	100000
6	100000	0.0000	0.9265	0.0000	100000	5.821	100000	100000	100000
7	100000	0.0000	0.9272	0.0000	100000	5.821	100000	100000	100000

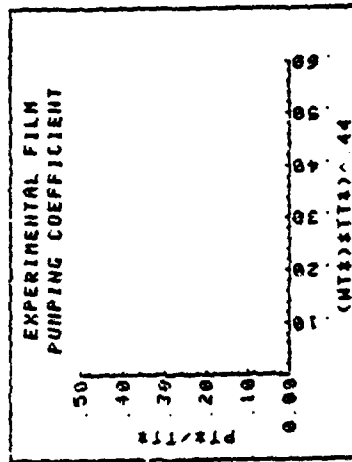
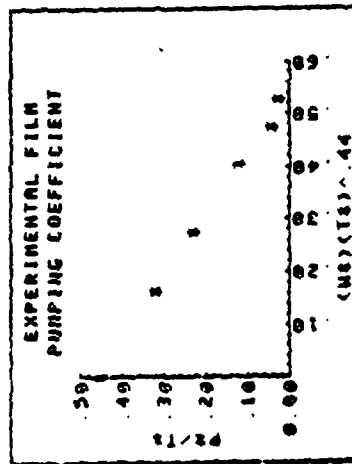


TABLE 15.1 - PCO DATA (CONT) FOR 15/25 NOZZLES WITH L/D=1.75 AND S/D=0.25 STACK

# MIXING STAGE DATA FOR RUN 7

TOP (POSITION 'A') DATA:				DIAGONAL (POSITION 'B') DATA:			
X-D	PRESSURE CIN H2O3	ROTATION COEG3	PM54	X-D	PRESSURE CIN H2O3	ROTATION COEG3	PM54
0.00	-2.220	92	-0.362	0.09	-1.970	92	-0.268
0.25	-1.200	28	-0.163	0.25	-1.120	28	-0.152
0.50	-1.040	14	-0.141	0.50	-0.950	14	-0.129
0.75	-0.910	26	-0.124	0.75	-0.815	26	-0.111
1.00	-0.790	32	-0.107	1.00	-0.705	32	-0.096
1.25	-0.675	34	-0.092	1.25	-0.520	34	-0.071
1.50	-0.595	20	-0.054	1.50	-0.170	20	-0.023

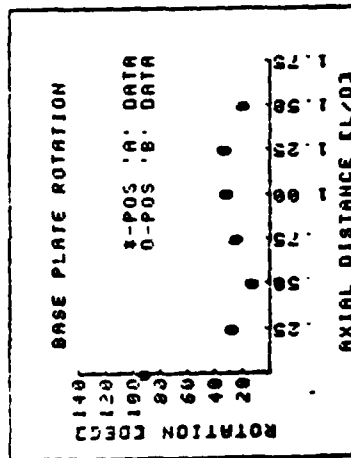
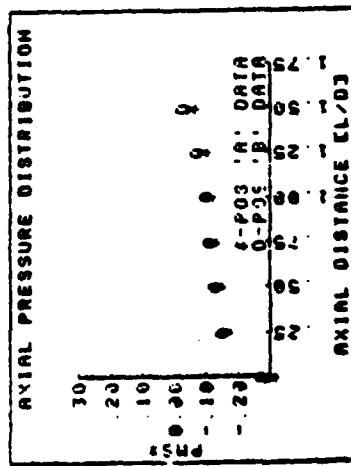
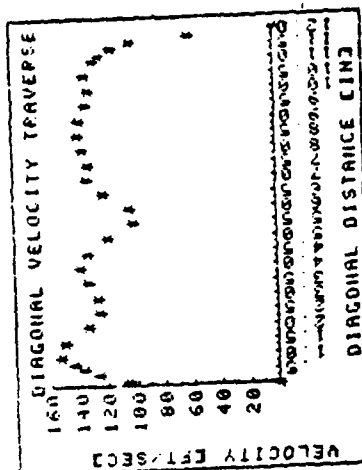
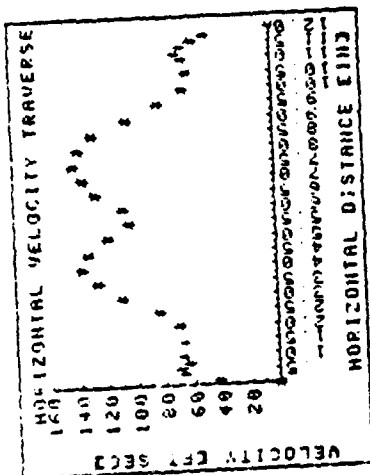


TABLE 15.2 - MSD DATA FOR 15/25 NOZZLES WITH L/D=1.75 AND S/D=0.25 STACK



HORIZONTAL VELOCITY TRAVERSE AT		BASE ROTATION OF 02 DEGREES	
POSITION	0.00	0.20	0.40
FEIN H203	0.00	1.00	1.00
VEFT SEC3	0.00	42.24	66.78
POSITION	2.00	2.50	3.00
FEIN H203	1.10	1.50	2.70
VEFT SEC3	79.64	84.47	109.74
POSITION	5.50	6.00	6.50
FEIN H203	2.48	2.60	3.60
VEFT SEC3	162.46	107.68	126.71
POSITION	9.00	9.50	10.00
FEIN H203	2.40	1.50	0.90
VEFT SEC3	103.46	21.79	63.36
POSITION	11.60	11.80	12.00
FEIN H203	6.70	0.50	0.00

DIAGONAL VELOCITY TRAVERSE FOR		BASE ROTATION OF 02 DEGREES	
POSITION	0.00	0.20	0.40
FEIN H203	0.00	2.50	3.60
VEFT SEC3	0.00	105.59	126.71
POSITION	2.00	2.50	3.00
FEIN H203	4.00	3.50	3.60
VEFT SEC3	137.57	124.94	126.71
POSITION	5.50	6.00	6.50
FEIN H203	2.30	2.40	3.30
VEFT SEC3	101.28	103.46	121.32
POSITION	9.00	9.50	10.00
FEIN H203	4.20	4.00	3.80
VEFT SEC3	136.86	133.57	130.18
POSITION	11.60	11.80	12.00
FEIN H203	2.30	0.80	0.00

TABLE 15.3 - VTD DATA FOR 15/25 NOZZLES WITH L/D=1.75 AND S/D=0.25 STACK

DATA INVEN ON: 11 AUG 81  
 DATA TAKEN BY: C C. DAVIS

NOZZLE AN/AP AREA RATIO: 2.50

COMMENTS:  
 15 TILT 30 POTATION (MAX 35)

MISCCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.982 EINH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 EINH<sup>2</sup>  
 ATM. PRESSURE: 30.06 EINH<sup>2</sup>

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 15 EDEGJ  
 ROTATION ANGLE: 30 EDEGJ  
 AREA PER NOZZLE: 10.752 EINH<sup>2</sup>  
 NUMBER OF NOZZLES: 4

MILLING STACK INFORMATION:  
 LENGTH: 20.48 EINH  
 DIAMETER: 11.70 EINH  
 L/D RATIO: 1.75  
 S/D RATIO: 0.50

N	POR	DPOR	FOR	TUPT	TAMB	PURT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.71	22.1	69.2	113.2	72.2	3.25	3.11	0.00	0.000	1111111
2	0.70	22.0	59.2	112.0	72.4	4.15	2.20	0.00	12.566	1111111
3	0.70	22.0	59.4	113.0	73.0	4.75	1.59	0.00	25.133	1111111
4	0.70	22.0	59.6	113.2	73.0	5.40	0.87	0.00	50.265	1111111
5	0.70	22.1	58.0	112.0	73.0	6.00	0.33	0.00	100.531	1111111
6	0.70	22.1	59.2	112.0	73.0	6.15	0.19	0.00	150.795	1111111
7	0.70	22.0	58.6	112.9	73.0	6.20	0.13	0.00	201.062	1111111
8	0.70	22.0	59.6	113.2	73.0	6.20	0.08	0.00	245.044	1111111
9	0.70	22.0	58.0	113.0	73.0	6.30	0.02	0.00	3333333	1111111

# SECONDARY BOX

N	US	P1	T1	PT-T1 HRT' 44	UP	NS	UP	UN	UUPT	UPT HACH
RUN					LBH/SEC	LBH/SEC	FT/SEC	FT/SEC	FT/SEC	
1	0.0000	0.4197	0.9284	0.4521	0.0000	3.7515	0.0000	181.92	72.77	0.062
2	0.1655	0.2326	0.9291	0.1223	0.1642	3.7466	0.6352	181.15	83.82	0.062
3	0.2832	0.2173	0.9302	0.2316	0.2791	3.7459	1.0794	180.90	91.69	0.062
4	0.4251	0.1186	0.9298	0.1376	0.4117	3.7452	1.5922	180.61	100.75	0.062
5	0.5236	0.0452	0.9305	0.0405	0.5073	3.7566	1.9669	180.80	107.53	0.062
6	0.5262	0.0260	0.9305	0.0280	0.5776	3.7551	2.2387	180.66	112.34	0.062
7	0.6506	0.0179	0.9305	0.0192	0.6301	3.7488	2.4691	180.33	116.33	0.062
8	0.6103	0.0103	0.9290	0.0111	0.5911	3.7452	2.2857	180.26	113.02	0.061
9	0.88888	0.0020	0.9302	0.0030	0.88888	3.7481	3.7811	180.31	3333333	0.061

TABLE 16 - PCO DATA FOR 15/30 NOZZLES WITH L/D=1.75 STACK

TERMINAL BOX

N	WT	PT	IT	PT/IT	WT/IT	44	NH	HT	UE
LBM/SEC LBM/SEC FT/SEC									
1	0.0000	0.0000	0.9294	0.0000	0.0000	0.0000	3.751	0.0000	0.0000
2	0.0000	0.0000	0.9294	0.0000	0.0000	0.0000	4.392	0.0000	0.0000
3	0.0000	0.0000	0.9302	0.0000	0.0000	0.0000	4.825	0.0000	0.0000
4	0.0000	0.0000	0.9298	0.0000	0.0000	0.0000	5.337	0.0000	0.0000
5	0.0000	0.0000	0.9305	0.0000	0.0000	0.0000	5.724	0.0000	0.0000
6	0.0000	0.0000	0.9305	0.0000	0.0000	0.0000	5.994	0.0000	0.0000
7	0.0000	0.0000	0.9305	0.0000	0.0000	0.0000	6.218	0.0000	0.0000
8	0.0000	0.0000	0.9298	0.0000	0.0000	0.0000	6.031	0.0000	0.0000
9	0.0000	0.0000	0.9302	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

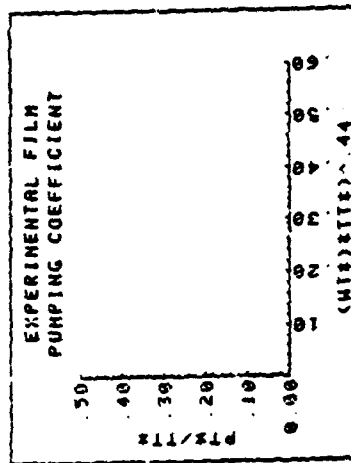
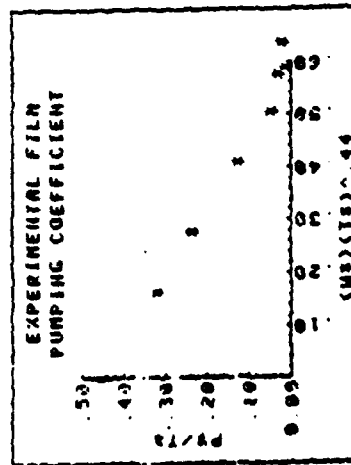


TABLE 16.1 - PCD DATA (CONT) FOR 15/30 NOZZLES WITH L/D=1.75 STACK



# MIXING STACK DATA FOR RUN 9

## TOP (POSITION 'A') DATA:

X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PMST
0.00	-2.140	96	-0.294
0.25	-1.150	10	-0.150
0.50	-0.955	14	-0.131
0.75	-0.840	24	-0.116
1.00	-0.695	10	-0.096
1.25	-0.510	22	-0.070
1.50	0.025	20	0.003

## DIAGONAL (POSITION 'B') DATA:

X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PMST
0.00	-1.030	96	-0.252
0.25	-0.905	10	-0.136
0.50	-0.905	13	-0.125
0.75	-0.675	24	-0.093
1.00	-0.475	10	-0.065
1.25	-0.395	22	-0.054
1.50	-0.205	20	-0.020

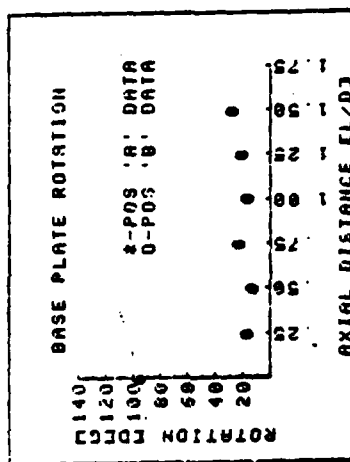
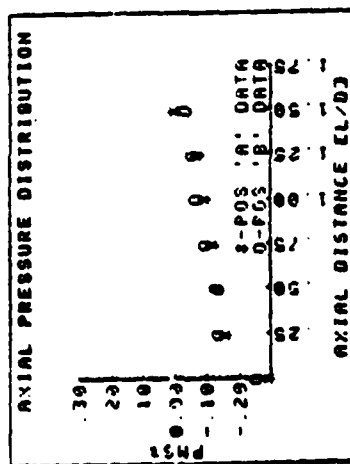
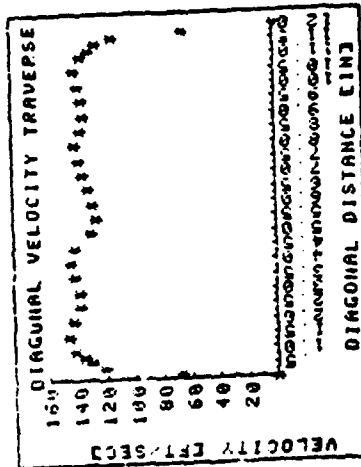
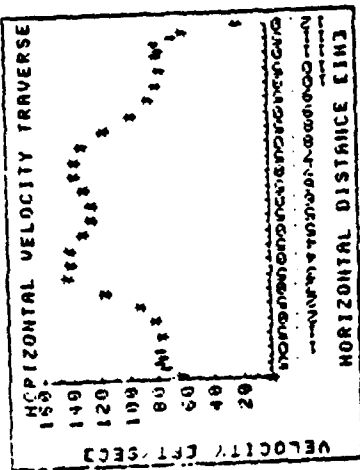


TABLE 16.2 - MSD DATA FOR 15/30 NOZZLES WITH L/D=1.75 STACK



HORIZONTAL VELOCITY TRAVERSE AT		BASE ROTATION OF 76 DEGREES	
POSITION	0.00	0.20	0.40
PEIN H203	0.00	0.30	1.20
VEFT/SEC	0.00	63.45	73.26
POSITION	2.00	2.50	3.00
PEIN H203	1.50	1.50	3.00
VEFT/SEC	61.91	92.19	115.84
POSITION	5.50	6.00	6.50
PEIN H203	3.50	3.50	3.00
VEFT/SEC	125.12	125.12	130.38
POSITION	9.00	9.50	10.00
PEIN H203	2.10	1.60	1.40
VEFT/SEC	96.92	84.60	79.13
POSITION	11.60	11.00	12.00
PEIN H203	1.00	0.60	0.10

DIAGONAL VELOCITY TRAVERSE FOR		BASE ROTATION OF 76 DEGREES	
POSITION	0.00	0.20	0.40
PEIN H203	0.00	1.00	3.30
VEFT/SEC	0.00	66.88	121.50
POSITION	2.00	2.50	3.00
PEIN H203	4.62	4.30	4.30
VEFT/SEC	143.44	139.69	138.69
POSITION	5.50	6.00	6.50
PEIN H203	3.69	3.70	3.90
VEFT/SEC	126.90	126.65	132.08
POSITION	9.00	9.50	10.00
PEIN H203	4.00	4.10	4.30
VEFT/SEC	133.72	135.42	138.69
POSITION	11.60	11.00	12.00
PEIN H203	2.90	0.90	0.00

TABLE 16.3 - VTD DATA FOR 15/30 NOZZLES WITH L/D=1.75 STACK

DATA TAKEN ON: 17 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

NOZZLE AN/AP AREA RATIO: 2.56  
 NOZZLE AN/AP AREA RATIO: 2.56  
 20 TILT/10 ROTATION: 0.5 S/D

MIXING STACK INFORMATION:  
 LENGTH: 20.48 EINH  
 DIAMETER: 11.70 EINH  
 L/D RATIO: 1.75  
 S/D RATIO: 0.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 20 DEGR  
 ROTATION ANGLE: 10 DEGR  
 AREA PER NOZZLE: 10.752 EINH  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 EINH  
 ORIFICE BETA: 0.497  
 UPRATE AREA: 107.510 EINH  
 ATM. PRESSURE: 29.96 EINH

N	FOR	DPOR	TOR	TUPT	TAKE	PUP	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF N2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.70	22.1	55.0	109.2	67.4	3.70	3.92	0.00	0.000	111111
2	0.70	22.1	55.4	109.0	67.4	4.55	2.07	0.00	12.566	111111
3	0.70	22.0	55.2	109.0	67.4	5.05	1.40	0.00	25.133	111111
4	0.70	21.9	55.4	109.0	67.4	5.65	0.81	0.00	50.263	111111
5	0.70	22.1	55.6	109.2	67.4	6.25	0.32	0.00	100.531	111111
6	0.70	22.2	55.6	109.2	67.4	6.40	0.10	0.00	150.796	111111
7	0.70	22.1	54.0	109.0	60.0	6.50	0.02	0.00	111111	111111

# SECONDARY BOX

N	He	P#	T#	PA/T#	MPT#	44	HP	HS	UP	UM	UUP	UPT	MACH
RUN													
1	0.0000	0.4057	0.9265	0.4370	0.0000	0.0000	3.7641	0.0000	161.82	72.73	72.74	0.062	
2	0.1642	0.2706	0.9268	0.3919	0.1500	0.1500	3.7627	0.6130	181.26	63.49	72.51	0.062	
3	0.2783	0.2015	0.9268	0.2174	0.2692	0.2692	3.7549	1.0452	180.62	90.83	72.26	0.062	
4	0.4120	0.1112	0.9268	0.1199	0.3993	0.3993	3.7456	1.5464	179.88	99.44	71.96	0.062	
5	0.5127	0.0429	0.9265	0.0463	0.4950	0.4950	3.7620	1.9287	180.51	106.40	72.21	0.062	
6	0.5799	0.0244	0.9269	0.0264	0.5600	0.5600	3.7704	2.1865	180.86	111.22	72.35	0.062	
7	0.0000	0.0027	0.9279	0.0029	0.0000	0.0000	3.7649	3.7927	180.46	0.0000	72.19	0.062	

TABLE 17 - PCD DATA FOR 20/10 NOZZLES WITH L/D=1.75 STACK

# TESTIAPY BOX

N	MTV	PTC	779	PTX-TT9	MTT1-44	MM	MT	UE
LBM/SEC LBM/SEC FT/SEC								
RUN								
1	111111	0.0000	0.9265	0.0000	111111	3.764	111111	111111
2	111112	0.0000	0.9268	0.0000	111112	4.381	111112	111112
3	111113	0.0000	0.9268	0.0000	111113	4.800	111113	111113
4	111114	0.0000	0.9268	0.0000	111114	5.292	111114	111114
5	111115	0.0000	0.9265	0.0000	111115	5.691	111115	111115
6	111116	0.0000	0.9269	0.0000	111116	5.957	111116	111116
7	111117	0.0000	0.9279	0.0000	111117	6.888	111117	111117

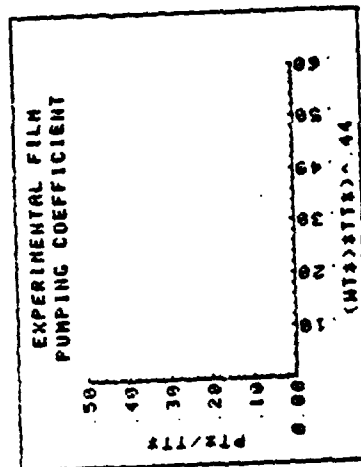
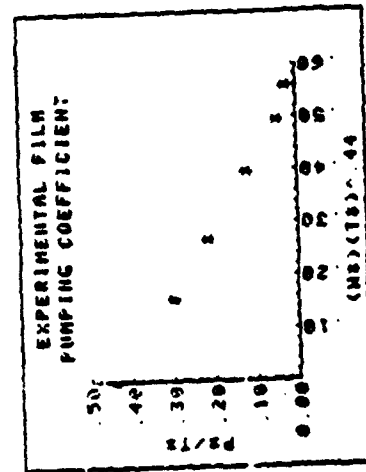


TABLE 17.1 - PCD DATA (CONT) FOR 20/10 NOZZLES WITH L/D-1.75 STACK

# MIXING STACK DATA FOR PUM 7

## TOP (POSITION 'A') DATA:

X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PHST
0.0A	-2.039	96	-0.290
0.25	-1.180	24	-0.161
0.50	-0.740	22	-0.101
0.75	-0.405	18	-0.055
1.00	-0.140	13	-0.019
1.25	-0.410	46	-0.056
1.50	0.100	10	0.025

## DIAGONAL (POSITION 'B') DATA:

X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PHST
0.00	-1.370	96	-0.187
0.25	-0.105	24	-0.023
0.50	-0.135	22	-0.010
0.75	-0.120	18	-0.016
1.00	0.060	13	0.000
1.25	-0.090	46	-0.012
1.50	-0.000	10	-0.011

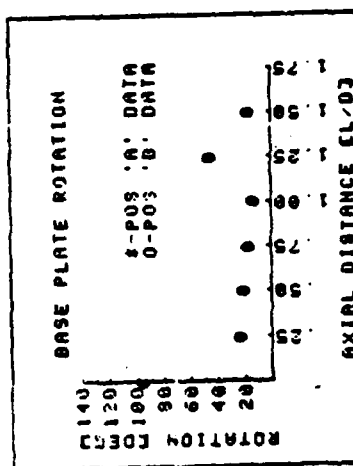
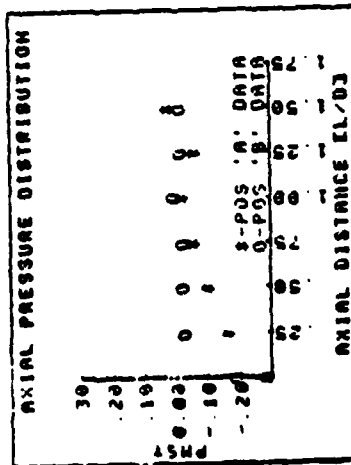
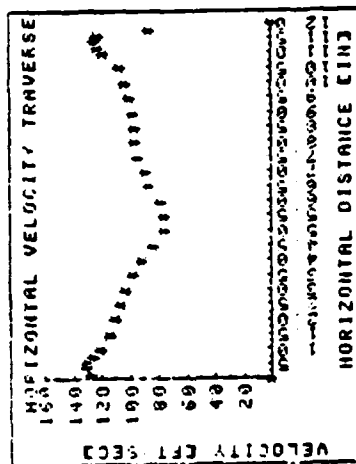


TABLE 17.2 - MSD DATA FOR 20/10 NOZZLES WITH L/D-1.75 STACK

WIND TUNNEL VELOCITY TRAVERSE AT BASE POSITION OF 05 DEGREES

POSITION	0.00	0.20	0.40	0.60	0.80	1.00	1.50
VELOCITY	0.00	3.70	3.30	3.80	3.60	3.30	3.00
VELOCITY	0.00	128.26	131.68	129.98	126.51	121.13	115.49
POSITION	2.00	2.50	3.00	3.50	4.00	4.50	5.00
VELOCITY	2.50	2.60	2.40	2.20	1.90	1.60	1.30
VELOCITY	111.57	107.51	103.30	99.90	91.91	84.34	76.02
POSITION	5.50	6.00	6.50	7.00	7.50	8.00	8.50
VELOCITY	1.30	1.40	1.70	1.80	2.00	2.10	2.10
VELOCITY	76.62	78.82	86.94	89.46	94.30	96.62	96.62
POSITION	9.00	9.50	10.00	10.50	11.00	11.20	11.40
VELOCITY	2.20	2.30	2.40	2.60	3.20	3.40	3.50
VELOCITY	98.30	101.12	103.30	107.51	119.20	122.95	124.74
POSITION	11.60	11.80	12.00				
VELOCITY	3.40	1.70	0.00				



DIAGONAL VELOCITY TRAVERSE FOR BASE POSITION OF 05 DEGREES

POSITION	0.00	0.20	0.40	0.60	0.80	1.00	1.50
VELOCITY	0.00	1.20	4.40	4.70	4.70	4.40	3.70
VELOCITY	0.00	73.84	139.85	144.55	144.55	139.86	128.26
POSITION	2.00	2.50	3.00	3.50	4.00	4.50	5.00
VELOCITY	3.10	2.70	2.40	2.20	1.90	1.60	1.30
VELOCITY	117.40	109.56	103.30	98.90	91.91	84.34	76.02
POSITION	5.50	6.00	6.50	7.00	7.50	8.00	8.50
VELOCITY	1.30	1.50	1.80	1.90	2.10	2.20	2.20
VELOCITY	76.62	81.65	89.46	91.91	96.62	98.90	98.90
POSITION	9.00	9.50	10.00	10.50	11.00	11.20	11.40
VELOCITY	2.40	2.60	3.10	3.70	4.10	4.30	4.40
VELOCITY	103.30	107.51	117.40	128.26	135.01	138.27	139.86
POSITION	11.60	11.80	12.00				
VELOCITY	4.10	2.80	0.00				

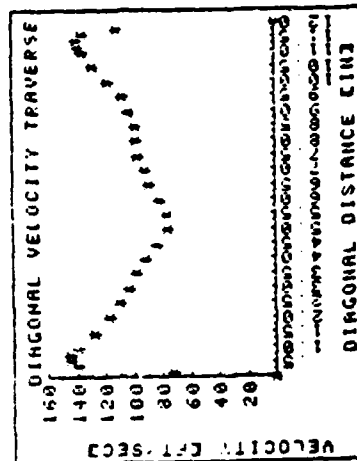


TABLE 17.3 - VTD DATA FOR 20/10 NOZZLES WITH L/D=1.75 STACK

DATA TAKEN ON: 10 AUG 91  
 DATA TAKEN BY: DAVIS/DRUCKER  
 NOZZLE AM/AP AREA RATIO: 2.50 20 TILT/20 ROTATION/0.5 S/D  
 COMMENTS:  
 MIXING STACK INFORMATION:  
 LENGTH: 20.48 [IN] 20 IDEG3  
 DIAMETER: 11.79 [IN] 20 IDEG3  
 L/D RATIO: 1.75 20 IDEG3  
 S/D RATIO: 0.50 4  
 PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 20 IDEG3  
 ROTATION ANGLE: 20 IDEG3  
 AREA PER NOZZLE: 10.752 [IN]2  
 NUMBER OF NOZZLES: 4  
 MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 [IN]  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 [IN]2  
 ATM. PRESSURE: 30.05 [IN]HG

N	POR	DPOR	TOR	TUPT	TAMB	PUP	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F					IN OF H2O		SQUARE INCHES	SQUARE INCHES
1	0.71	22.0	58.6	112.2	71.0	3.50	2.99	0.00	0.000	111111
2	0.70	22.0	58.6	112.2	72.0	4.30	2.13	0.00	12.566	111111
3	0.69	21.0	59.2	112.6	72.2	4.90	1.51	0.00	25.133	111111
4	0.70	22.0	58.0	112.6	72.2	5.60	0.87	0.00	50.265	111111
5	0.70	22.0	59.2	112.6	72.2	6.10	0.33	0.00	100.531	111111
6	0.70	22.0	59.2	112.6	72.2	6.20	0.19	0.00	150.796	111111
7	0.70	22.0	58.0	112.6	72.4	6.35	0.01	0.00	111111	111111

# SECONDARY BOX

M	Wt	P#	T#	P#T#	W#T#	44	NP	HS	UP	UM	UPT	UPT	NACH
RUN							LBN/SEC	LBN/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	
1	0.0000	0.4055	0.9294	0.4363	0.0000	3.7481	0.0000	131.44		72.58	72.58	0.062	
2	0.1660	0.2902	0.9297	0.3121	0.1615	3.7482	0.6251	181.06		63.60	72.43	0.062	
3	0.2622	0.2083	0.9294	0.2241	0.2733	3.7290	1.0525	179.99		90.82	72.00	0.061	
4	0.4264	0.1192	0.9294	0.1202	0.4120	3.7474	1.5970	180.59		100.81	72.24	0.062	
5	0.5254	0.0434	0.9294	0.0408	0.5087	3.7460	1.9681	180.28		107.30	72.12	0.062	
6	0.5900	0.0251	0.9294	0.0201	0.5790	3.7460	2.2400	180.22		112.14	72.10	0.061	
7	0.6333	0.0014	0.9290	0.0015	0.6111	3.7475	2.6747	180.21		111.11	72.09	0.061	

TABLE 18 - PCD DATA FOR 20/20 NOZZLES WITH L/D=1.75 STACK

# TESTIRY BOX

N	WT	PT	ITS	PTS/ITS	WTIT-44	WH	HT	UE
LBM/SEC LBM/SEC FT/SEC								
1	211111	0.0000	0.9294	0.0000	211111	3.748	111111	111111
2	211111	0.0000	0.9297	0.0000	211111	4.373	111111	111111
3	211111	0.0000	0.9294	0.0000	211111	4.781	111111	111111
4	211111	0.0000	0.9294	0.0000	211111	5.345	111111	111111
5	211111	0.0000	0.9294	0.0000	211111	5.714	111111	111111
6	211111	0.0000	0.9294	0.0000	211111	5.986	111111	111111
7	211111	0.0000	0.9298	0.0000	211111	111111	111111	111111

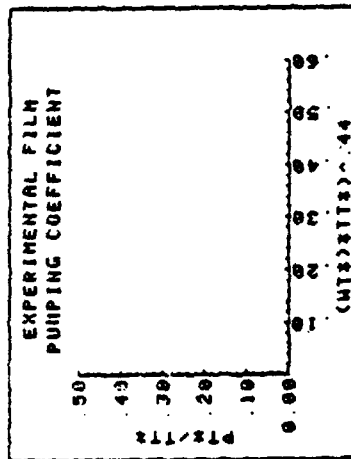
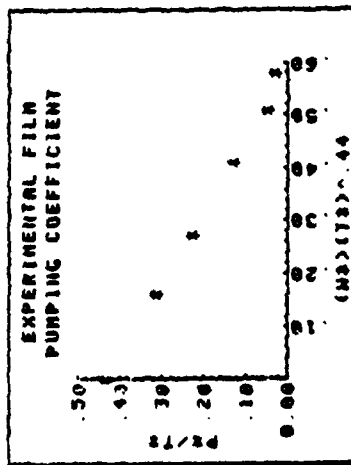


TABLE 18.1 - PCD DATA (CONT) FOR 20/20 NOZZLES WITH L/D=1.75 STACK



# MIXING STACK DATA FOR RUN 7

## TOP (POSITION 'A') DATA

X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PMS
0.00	-1.935	72	-0.266
0.25	-1.205	26	-0.166
0.50	-0.695	12	-0.123
0.75	-0.525	15	-0.072
1.00	-0.320	6	-0.044
1.25	-0.465	30	-0.064
1.50	0.105	6	0.025

## DIAGONAL (POSITION 'B') DATA

X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PMS
0.00	-1.410	72	-0.194
0.25	-0.605	26	-0.083
0.50	-0.265	12	-0.036
0.75	-0.145	15	-0.020
1.00	-0.030	6	-0.004
1.25	-0.105	30	-0.014
1.50	-0.075	6	-0.010

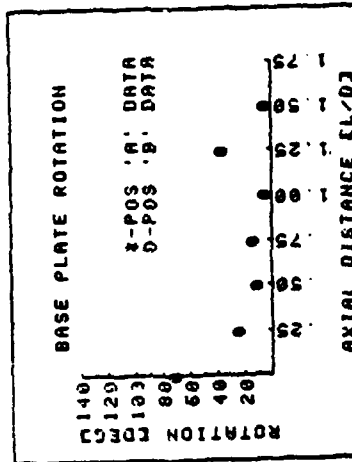
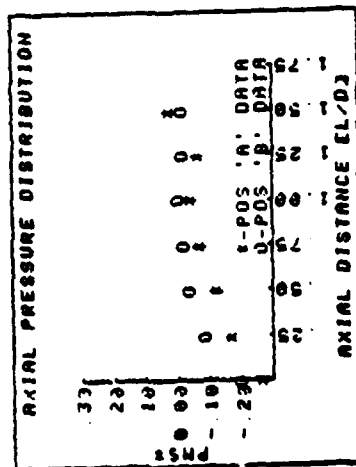
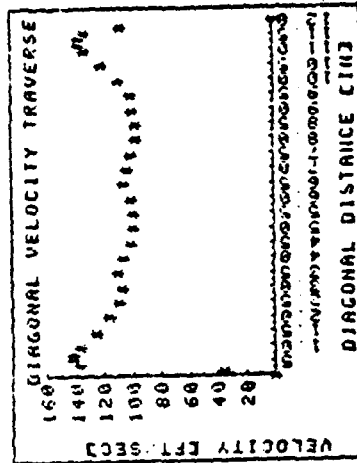
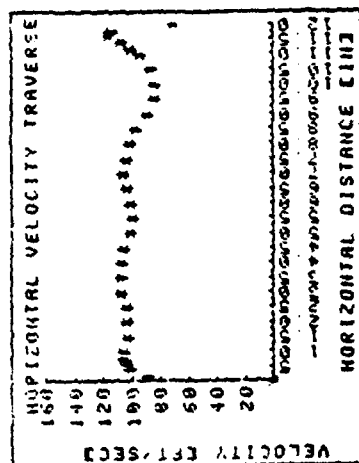


TABLE 18.2 - MSD DATA FOR 20/20 NOZZLES WITH L/D=1.75 STACK



HORIZONTAL VELOCITY TRAVERSE AT		BASE ROTATION OF 72 DEGREES	
FLIN FLIN	0.00	0.20	0.40
FLIN H2O1	0.00	1.30	2.30
VEFT SEC1	0.00	89.69	101.39
POS FLIN	2.00	2.50	3.00
FLIN H2O1	2.40	2.40	2.60
VEFT SEC1	103.57	103.57	107.80
POS FLIN	5.50	6.00	6.50
FLIN H2O1	2.20	2.30	2.40
VEFT SEC1	99.16	141.39	103.57
POS FLIN	9.00	9.50	10.00
FLIN H2O1	1.00	1.60	1.60
VEFT SEC1	89.69	84.56	84.56
POS FLIN	11.60	11.80	12.00
FLIN H2O1	3.60	2.90	1.10

RUN	M	POR	IN OF H2O	DPOR	TOR	TUPT	TANB	PUPT	PSEC	PTER	SECONDARY AREA SQUARE INCHES	TERTIARY AREA SQUARE INCHES
1	1	0.70	22.0	61.0	113.6	70.4	3.40	3.05	0.00	0.00	0.000	0.000
2	2	0.70	22.0	60.0	113.0	70.4	4.30	2.19	0.00	0.00	12.566	0.000
3	3	0.70	22.0	60.4	113.6	70.6	4.90	1.57	0.00	0.00	25.133	0.000
4	4	0.70	22.0	60.0	113.0	70.6	5.55	0.96	0.00	0.00	50.205	0.000
5	5	0.70	22.0	60.6	113.8	70.8	6.10	0.34	0.00	0.00	100.531	0.000
6	6	0.70	21.9	61.0	114.0	71.2	6.20	0.20	0.00	0.00	150.796	0.000
7	7	0.50	21.0	41.0	114.0	71.4	6.35	0.01	0.00	0.00	0.000	0.000

SECONDARY BOX											
N	WS	PS	IS	PS/IS	WT/4	HP	MS	UP	UM	UPT	UPT MACH
LBM/SEC LBM/SEC FT/SEC FT/SEC											
RUN											
1	0.0000	0.4123	0.9246	0.4459	0.0000	3.7433	0.0000	181.31	72.53	72.53	0.062
2	0.1697	0.2970	0.9243	0.3213	0.1639	3.7440	0.6354	181.03	83.72	72.42	0.062
3	0.2873	0.2136	0.9250	0.2309	0.2776	3.7454	1.0759	180.76	91.45	72.31	0.062
4	0.4254	0.1174	0.9247	0.1270	0.4110	3.7440	1.5929	180.44	100.51	72.10	0.061
5	0.5308	0.0459	0.9250	0.0496	0.5129	3.7447	1.9875	180.24	107.47	72.10	0.061
6	0.6000	0.0269	0.9254	0.0290	0.5884	3.7340	2.2737	179.76	112.40	71.91	0.061
7	0.6000	0.0014	0.9257	0.0015	0.5885	3.7340	2.6799	179.60	118.88	71.00	0.061

TABLE 19 - PCD DATA FOR 20/30 NOZZLES WITH L/D=1.75 STACK

TERTIARY BOX

N	WT	PTS	TTS	PTT-TT	NTSTT-44	UN	WT	UE
LBM/SEC LBM/SEC FT/SEC								
RUN								
1	111111	0.0000	0.9246	0.0000	111111	3.743	111111	111111
2	111111	0.0000	0.9243	0.0000	111111	4.379	111111	111111
3	111111	0.0000	0.9250	0.0000	111111	4.021	111111	111111
4	111111	0.0000	0.9247	0.0000	111111	5.337	111111	111111
5	111111	0.0000	0.9250	0.0000	111111	5.732	111111	111111
6	111111	0.0000	0.9254	0.0000	111111	6.008	111111	111111
7	111111	0.0000	0.9257	0.0000	111111	111111	111111	111111

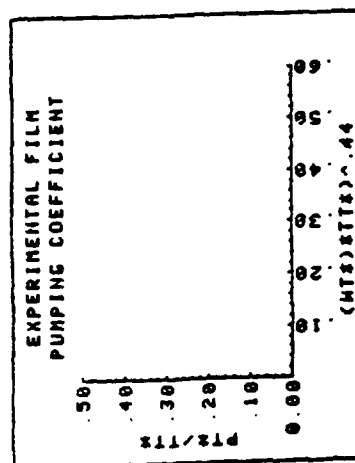
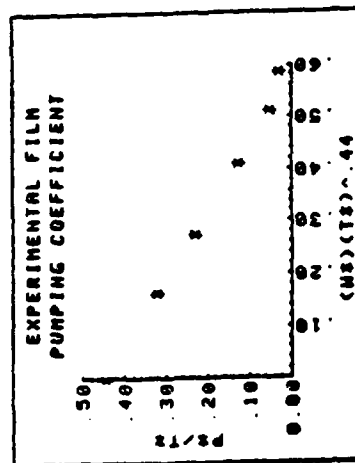


TABLE 18.1 - PCD DATA (CONT) FOR 20/30 NOZZLES WITH L/D=1.75 STACK

DATA TAKEN ON: 19 AUG 81  
DATA TAKEN BY: C.C. DAVIS

NOZZLE AN/AP AREA RATIO: 2.50 22.5 TILT/10 ROTATION/PCD  
COMMENTS:  
MIXING STACK INFORMATION: 20.40 L/NJ  
LENGTH: 11.70 L/NJ  
DIAMETER: 1.75  
L/D RATIO: 0.50  
PRIMARY NOZZLE INFORMATION:  
TILT ANGLE: 22.5 LDEGJ  
ROTATION ANGLE: 10 LDEGJ  
AREA PER NOZZLE: 10.752 L/N2J  
NUMBER OF NOZZLES: 4  
MISCELLANEOUS INFORMATION:  
ORIFICE DIAMETER: 6.902 L/NJ  
ORIFICE BETA: 0.497  
UPTAKE AREA: 107.510 L/N2J  
ATM. PRESSURE: 30.12 L/NHCG

N	POR	DPOR	TOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES	F	IN OF H2O	IN OF H2O	IN OF H2O	IN OF H2O	IN OF H2O	SQUARE INCHES	SQUARE INCHES
1	0.70	22.1	60.2	113.4	70.8	4.10	2.95	0.00	0.000	*****
2	0.70	22.0	60.0	113.6	70.8	4.75	2.01	0.00	12.566	*****
3	0.70	22.1	60.6	113.0	70.8	5.35	1.44	0.00	25.133	*****
4	0.70	21.9	60.4	114.0	71.2	5.95	0.78	0.00	50.265	*****
5	0.70	22.2	60.2	113.0	71.4	6.45	0.38	0.00	100.531	*****
6	0.70	22.1	60.4	113.0	71.2	6.60	0.17	0.00	150.796	*****
7	0.70	22.1	61.0	114.0	71.4	6.70	0.01	0.00	*****	*****

#### SECONDARY BOX

N	M2	P2	T2	P2/T2	M2/T2	MP	MS	UP	UM	UPT	UPT MACH
RUN						LBN/SEC	LBN/SEC	FT/SEC	FT/SEC	FT/SEC	
1	0.0000	0.3965	0.9257	0.4203	0.0000	3.7553	0.0000	101.72	72.69	72.70	0.062
2	0.1625	0.2732	0.9253	0.2952	0.1571	3.7446	0.6086	180.86	83.17	72.35	0.062
3	0.2740	0.1945	0.9250	0.2103	0.2648	3.7538	1.0286	181.11	90.75	72.45	0.062
4	0.4056	0.1070	0.9254	0.1156	0.3920	3.7375	1.5161	190.10	99.03	72.04	0.061
5	0.4995	0.0407	0.9261	0.0440	0.4829	3.7638	1.8801	181.08	105.92	72.44	0.062
6	0.5655	0.0232	0.9257	0.0251	0.5466	3.7546	2.1233	100.50	110.04	72.24	0.062
7	0.6000	0.0007	0.9257	0.0007	0.6000	3.7524	1.0953	100.47	0.0000	72.19	0.061

TABLE 20 - PCD DATA FOR 22.5/10 NOZZLES WITH L/D-1.75 STACK

TERTIARY BOX

N	WT	PT	TT	PT-TT	WT-TT	HM	WT	UE
RUN						LB/SEC	LB/SEC	FT/SEC
1	33333	0.0000	0.9257	0.0000	33333	3.755	33333	33333
2	33333	0.0000	0.9253	0.0000	33333	4.353	33333	33333
3	33333	0.0000	0.9250	0.0000	33333	4.782	33333	33333
4	33333	0.0000	0.9254	0.0000	33333	5.254	33333	33333
5	33333	0.0000	0.9261	0.0000	33333	5.644	33333	33333
6	33333	0.0000	0.9257	0.0000	33333	5.878	33333	33333
7	33333	0.0000	0.9257	0.0000	33333	5.878	33333	33333

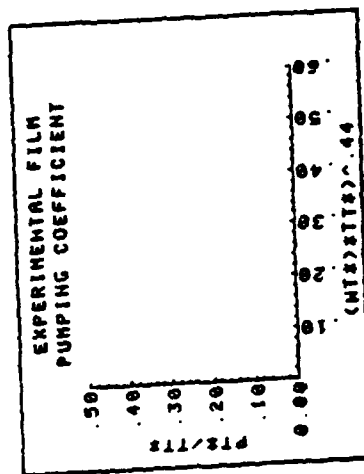
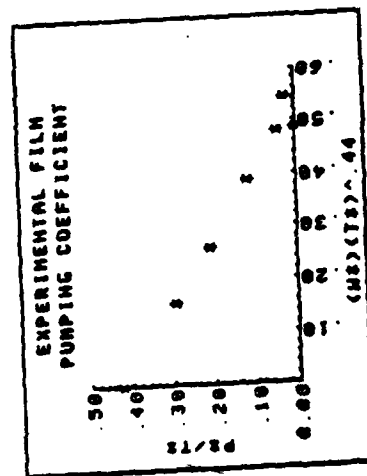


TABLE 20.1 - PCD DATA (CONT) FOR 22.5/10 NOZZLES WITH L/D=1.75 STACK

DATA TAKEN ON: 19 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

NOZZLE AN/AP AREA RATIO: 2.50 22.5 TILT/20 ROTATION/PCD

MIXING STACK INFORMATION:  
 LENGTH: 20.46 E1N2  
 DIAMETER: 11.78 E1N3  
 L/D RATIO: 1.75  
 S/D RATIO: 0.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 22.5 EDEG3  
 ROTATION ANGLE: 20 EDEG3  
 AREA PER NOZZLE: 18.752 E1N23  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 E1N3  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 187.518 E1N23  
 ATM. PRESSURE: 30.13 E1NNG3

M	POR	DPOR	TOR	TUPT	TANG	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.69	22.1	68.2	113.4	71.8	3.79	2.95	0.00	0.000	0.000
2	0.69	22.0	68.2	113.8	71.6	4.55	2.13	0.00	12.566	0.000
3	0.69	22.0	68.2	113.8	71.6	5.10	1.51	0.00	25.133	0.000
4	0.69	22.0	68.2	113.8	71.8	5.88	0.83	0.00	50.265	0.000
5	0.70	22.1	68.2	113.8	71.8	6.35	0.31	0.00	100.531	0.000
6	0.69	22.1	68.2	113.8	71.8	6.45	0.16	0.00	150.796	0.000
7	0.70	22.0	68.4	114.0	72.0	6.60	0.01	0.00	0.000	0.000

# SECONDARY BOX

M	HS	PS	TS	PS/TS	WGT/44	NP	WS	UP	UM	UWPT	UPT	MACH
RUN							LBM/SEC	LBM/SEC	FT/SEC	FT/SEC		
1	0.0000	0.3992	0.9274	0.4304	0.0000	3.7556	0.0000	181.72	72.69	72.69	0.062	
2	0.1671	0.2892	0.9264	0.3122	0.1616	3.7471	0.6261	181.06	83.58	72.43	0.062	
3	0.2014	0.2957	0.9264	0.2220	0.2721	3.7471	1.0544	180.79	91.18	72.32	0.062	
4	0.4172	0.1135	0.9268	0.1224	0.4034	3.7471	1.5631	180.49	100.06	72.20	0.062	
5	0.5087	0.0423	0.9268	0.0456	0.4920	3.7556	1.9106	180.66	106.32	72.27	0.062	
6	0.5002	0.0210	0.9268	0.0236	0.5302	3.7556	2.0509	180.60	108.94	72.25	0.062	
7	0.0000	0.0007	0.9268	0.0007	0.0000	3.7464	1.0944	180.15	0.0000	72.07	0.061	

TABLE 21 - PCD DATA FOR 22.5/20 NOZZLES WITH L/D-1.75 STACK

TERTIARY BOX

N	MTS	PT4	ITS	PT2/ITS	MTSTT-44	MM	MT	UE
RUN						LBM/SEC	LBM/SEC	FT/SEC
1	0.0000	0.0000	0.9274	0.0000	0.0000	3.756	4.418	0.0000
2	0.0000	0.0000	0.9264	0.0000	0.0000	4.373	4.418	0.0000
3	0.0000	0.0000	0.9264	0.0000	0.0000	4.802	4.418	0.0000
4	0.0000	0.0000	0.9260	0.0000	0.0000	5.310	4.418	0.0000
5	0.0000	0.0000	0.9260	0.0000	0.0000	5.666	4.418	0.0000
6	0.0000	0.0000	0.9260	0.0000	0.0000	5.815	4.418	0.0000
7	0.0000	0.0000	0.9260	0.0000	0.0000	0.0000	0.0000	0.0000

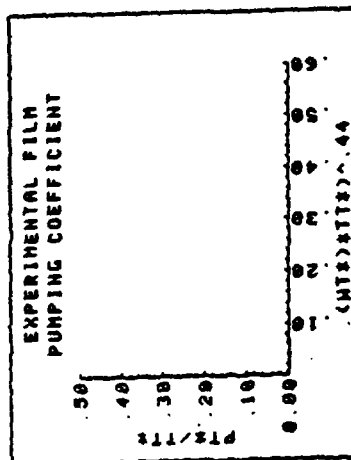
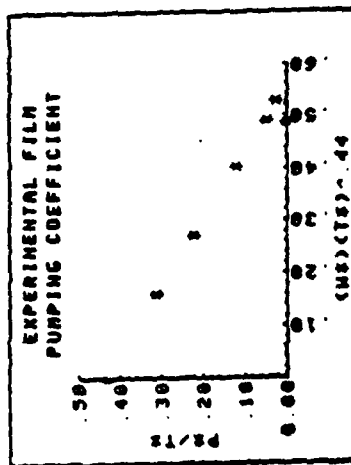


TABLE 21.1 - PCD DATA (CONT) FOR 22.5/20 NOZZLES WITH L/D=1.75 STACK



DATA TAKEN ON: 19 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

NOZZLE AN/AP AREA RATIO: 2.50  
 22.5 TILT/25 ROTATION/PCD

MIXING STACK INFORMATION:  
 LENGTH: 20.40 CINH  
 DIAMETER: 11.70 CINH  
 L/D RATIO: 1.75  
 S/D RATIO: 0.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 22.5 DEGR  
 ROTATION ANGLE: 25 DEGR  
 AREA PER NOZZLE: 10.752 CINH2  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINH2  
 ATM PRESSURE: 30.13 CINH2

RUN	N	POR	DPOR	TOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA		TERTIARY AREA	
										SQUARE INCHES	SQUARE INCHES	SQUARE INCHES	SQUARE INCHES
1	0.70	22.1	59.4	113.2	71.0	3.55	3.12	0.00	0.00	0.000	0.000	0.000	0.000
2	0.70	21.9	59.4	113.2	72.0	4.45	2.20	0.00	0.00	12.566	12.566	12.566	12.566
3	0.70	22.1	59.2	113.0	72.0	5.05	1.50	0.00	0.00	25.133	25.133	25.133	25.133
4	0.69	22.0	58.0	112.0	72.0	5.75	0.86	0.00	0.00	50.265	50.265	50.265	50.265
5	0.69	21.9	59.2	112.0	72.0	6.20	0.34	0.00	0.00	100.531	100.531	100.531	100.531
6	0.69	22.0	59.6	113.0	72.0	6.40	0.19	0.00	0.00	150.796	150.796	150.796	150.796
7	0.70	22.0	59.2	113.0	72.2	6.55	0.01	0.00	0.00	0.000	0.000	0.000	0.000

#### SECONDARY BOX

RUN	N	WS	PS	TS	PR-TS	M/T	44	HP	WS	UP	UM		UPT		UPT		MACH
											LBM/SEC	LBM/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	
1	0.000	0.4201	0.9277	0.4520	0.0000	3.7505	0.0000	181.06	72.75	72.75	72.75	72.75	72.75	72.75	72.75	72.75	0.062
2	0.1690	0.2997	0.9201	0.3229	0.1643	3.7415	0.6354	180.63	93.58	72.26	93.58	72.26	93.58	72.26	93.58	72.26	0.062
3	0.2064	0.2130	0.9294	0.2303	0.2771	3.7592	1.0765	181.15	91.65	72.47	91.65	72.47	91.65	72.47	91.65	72.47	0.062
4	0.4237	0.1179	0.9207	0.1265	0.4101	3.7551	1.5908	180.57	100.59	72.23	100.59	72.23	100.59	72.23	100.59	72.23	0.062
5	0.5307	0.0462	0.9207	0.0490	0.5137	3.7422	1.9850	179.72	107.29	71.89	107.29	71.89	107.29	71.89	107.29	71.89	0.061
6	0.5903	0.0261	0.9204	0.0201	0.5791	3.7493	2.2433	180.06	112.02	72.03	112.02	72.03	112.02	72.03	112.02	72.03	0.061
7	0.0000	0.0007	0.9200	0.0007	0.0000	3.7507	1.0940	180.04	0.000	72.02	0.000	72.02	0.000	72.02	0.000	72.02	0.061

TABLE 22 - PCD DATA FOR 22.5/25 NOZZLES WITH L/D=1.75 STACK

### 3.1.1

N	WTS	PIS	TTs	PIS/TTs	WTS/TTs	WTS	LBM/SEC	LBM/SEC	FT/SEC
RUN									
1	0.0000	0.0000	0.9277	0.0000	0.0000	3.758	0.0000	0.0000	0.0000
2	0.0000	0.0000	0.9281	0.0000	0.0000	4.377	0.0000	0.0000	0.0000
3	0.0000	0.0000	0.9284	0.0000	0.0000	4.836	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.9297	0.0000	0.0000	5.346	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.9287	0.0000	0.0000	5.728	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.9284	0.0000	0.0000	5.993	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.9280	0.0000	0.0000	6.328	0.0000	0.0000	0.0000

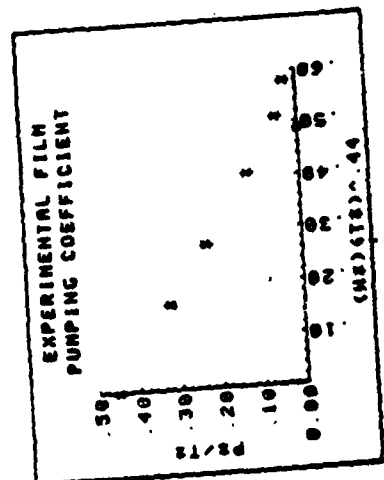
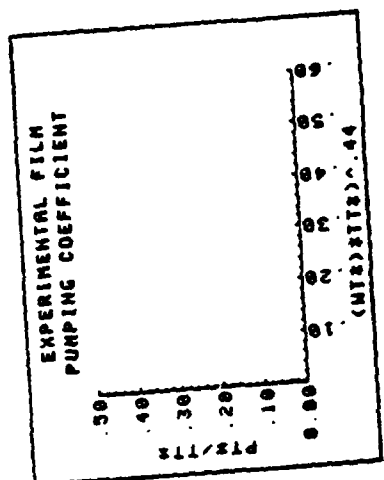


TABLE 22.1 - PCD DATA (CONT) FOR 22.5/25 NOZZLES WITH L/D=1.75 STACK

DATA TAKEN ON: 20 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 17.55 INJ  
 DIAMETER: 11.70 INJ  
 L/D RATIO: 1.50  
 S/D RATIO: 0.50

NOZZLE AN/AP AREA RATIO: 2.50

COMMENTS:  
 STRAIGHT NOZZLES CAL L/D=1.5

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 INJ  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.519 INH2  
 ATM. PRESSURE: 30.06 INHG

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 0.0 DEEG  
 ROTATION ANGLE: 0.0 DEEG  
 AREA PER NOZZLE: 10.752 INH2  
 NUMBER OF NOZZLES: 4

N	POR	DPOR	TOR	TUPT	TAMB	PUP	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.70	22.1	57.6	110.4	66.0	3.25	3.25	0.00	0.000	xxxxxx
2	0.70	21.9	57.0	110.6	66.0	4.20	2.14	0.00	12.566	xxxxxx
3	0.70	22.1	57.4	110.6	66.6	4.85	1.49	0.00	25.133	xxxxxx
4	0.70	22.0	57.6	110.6	66.6	5.50	0.78	0.00	50.265	xxxxxx
5	0.70	21.9	58.0	110.0	66.0	5.95	0.27	0.00	100.531	xxxxxx
6	0.70	21.9	57.6	110.0	66.0	6.05	0.15	0.00	150.756	xxxxxx
7	0.70	22.1	57.0	111.0	67.0	6.20	0.01	0.00	xxxxxx	xxxxxx

SECONDARY BOX

N	M3	P3	T3	PS/T3	W3T3.44	MP	MS	UP	UM	UPT	UPT MACH
RUN							LBM/SEC	LBM/SEC	FT/SEC	FT/SEC	
1	0.0000	0.4353	0.9221	0.4721	0.0000	3.7609	0.0000	181.54	72.62	72.62	0.062
2	0.1684	0.2907	0.9210	0.3154	0.1624	3.7432	0.6302	180.26	83.24	72.11	0.062
3	0.2790	0.2006	0.9220	0.2174	0.2693	3.7617	1.0495	180.86	90.91	72.35	0.062
4	0.4054	0.1063	0.9220	0.1152	0.3913	3.7524	1.5212	180.10	98.95	72.05	0.062
5	0.4782	0.0371	0.9229	0.0402	0.4616	3.7425	1.7896	179.46	103.45	71.79	0.061
6	0.5254	0.0159	0.9229	0.0216	0.5072	3.7439	1.9672	179.48	106.60	71.80	0.061
7	0.5588	0.0007	0.9229	0.0007	0.5888	3.7602	1.9013	180.26	111.88	72.11	0.062

TABLE 23 - PCD DATA FOR STRAIGHT NOZZLES WITH L/D=1.5 STACK

TERTIARY BOX

N	WT	PT	TT	PT/TT	WT	UE
RUN						
1	3.761	0.0000	0.9221	0.0000	3.761	0.0000
2	4.373	0.0000	0.9218	0.0000	4.373	0.0000
3	4.811	0.0000	0.9220	0.0000	4.811	0.0000
4	5.274	0.0000	0.9220	0.0000	5.274	0.0000
5	5.532	0.0000	0.9229	0.0000	5.532	0.0000
6	5.711	0.0000	0.9229	0.0000	5.711	0.0000
7	5.711	0.0000	0.9229	0.0000	5.711	0.0000

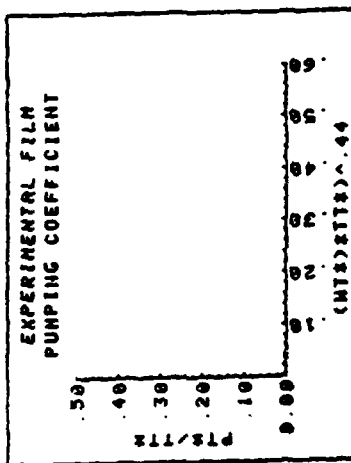
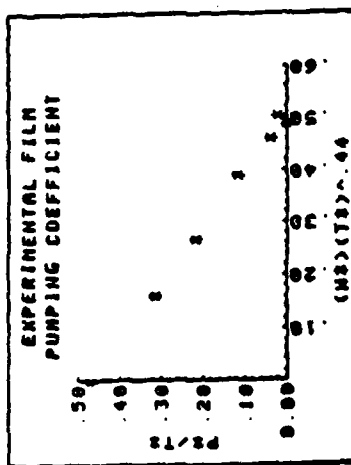


TABLE 23.1 - PCD DATA (CONT) FOR STRAIGHT NOZZLES WITH L/D=1.5 STACK

# MIXING STACK DATA FOR RUN 7

## TOP (POSITION 'A') DATA

X/D	PRESSURE CIN H2O3	ROTATION DEG	PMS*
0.00	-2.100	45	-0.297
0.25	-0.965	45	-0.131
0.50	-0.735	45	-0.100
0.75	-0.595	45	-0.081
1.00	-0.385	45	-0.052
1.25	-0.240	45	-0.033

## CIRCULAR (POSITION 'B') DATA

X/D	PRESSURE CIN H2O3	ROTATION DEG	PMS*
0.00	-1.010	45	-0.246
0.25	-0.890	45	-0.121
0.50	-0.695	45	-0.095
0.75	-0.575	45	-0.070
1.00	-0.435	45	-0.059
1.25	-0.255	45	-0.035

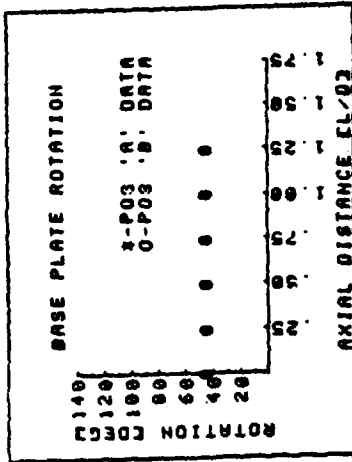
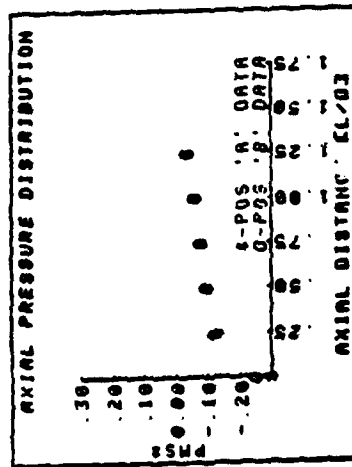
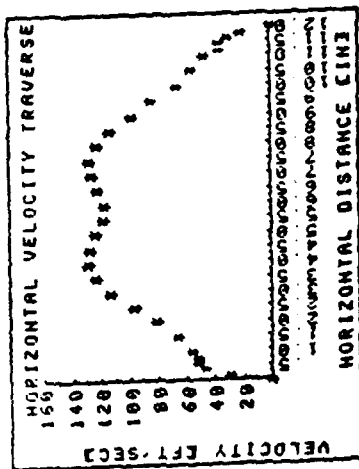


TABLE 23.2 - MSD DATA FOR STRAIGHT NOZZLES WITH L/D=1.5 STACK

HORIZONTAL VELOCITY TRAVERSE AT BASE ROTATION OF 00 DEGREES

POSITIVEIN3	0.00	0.20	0.40	0.60	0.80	1.00	1.50
PEIN M203	0.00	0.20	0.50	0.60	0.60	0.70	1.00
VEFT/SEC3	0.00	29.74	47.02	51.51	51.51	55.64	66.50
POSITIVEIN3	2.00	2.50	3.00	3.50	4.00	4.50	5.00
PEIN M203	1.50	2.10	2.90	3.50	3.80	3.70	3.50
VEFT/SEC3	81.45	95.37	113.25	124.42	129.64	127.92	124.42
POSITIVEIN3	5.50	6.00	6.50	7.00	7.50	8.00	8.50
PEIN M203	3.20	3.10	3.40	3.60	3.70	3.40	2.90
VEFT/SEC3	110.96	117.09	122.63	126.18	127.92	122.63	113.25
POSITIVEIN3	9.00	9.50	10.00	10.50	11.00	11.20	11.40
PEIN M203	2.20	1.60	1.00	0.70	0.50	0.30	0.30
VEFT/SEC3	98.64	84.12	66.50	55.64	47.02	36.45	36.45
POSITIVEIN3	11.60	11.00	12.00				
PEIN M203	0.20	0.10	0.00				



DIAGONAL VELOCITY TRAVERSE FOR BASE ROTATION OF 00 DEGREES

POSITIVEIN3	0.00	0.20	0.40	0.60	0.80	1.00	1.50
PEIN M203	0.00	0.90	1.50	1.80	2.00	2.30	3.60
VEFT/SEC3	0.00	63.09	81.45	89.22	94.05	100.86	126.18
POSITIVEIN3	2.00	2.50	3.00	3.50	4.00	4.50	5.00
PEIN M203	4.90	5.80	5.80	5.20	4.50	4.00	3.50
VEFT/SEC3	147.21	160.16	160.16	151.65	141.07	133.01	124.42
POSITIVEIN3	5.50	6.00	6.50	7.00	7.50	8.00	8.50
PEIN M203	3.20	3.10	3.40	4.00	4.70	5.40	5.90
VEFT/SEC3	118.96	117.09	122.63	133.01	144.18	154.54	161.54
POSITIVEIN3	9.00	9.50	10.00	10.50	11.00	11.20	11.40
PEIN M203	6.10	5.90	4.90	3.40	2.30	2.00	1.00
VEFT/SEC3	164.25	161.54	147.21	122.63	100.86	94.05	89.22
POSITIVEIN3	11.60	11.00	12.00				
PEIN M203	1.50	0.90	0.00				

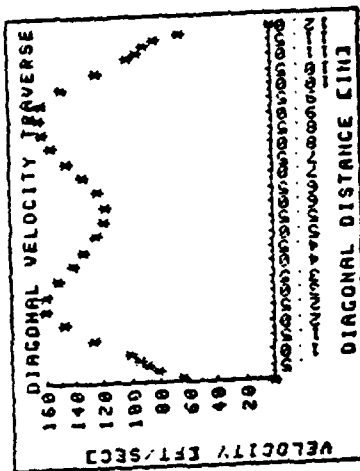


TABLE 23.3 - VTD DATA FOR STRAIGHT NOZZLES WITH L/D=1.5 STACK

DATA TAKEN ON: 23 AUG 81  
 DATA TAKEN BY: C.C. DAVIS  
 NOZZLE AM/OP AREA RATIO: 2.50  
 COMMENTS:  
 10 TILT/10 POTATION/PCD ONLY  
 MIXING STACK INFORMATION:  
 LENGTH: 17.55 CINS  
 DIAMETER: 11.70 CINS  
 L/D RATIO: 1.50  
 S/D RATIO: 0.50  
 PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 10.0 CODEGJ  
 ROTATION ANGLE: 10 CODEGJ  
 AREA PER NOZZLE: 10.752 CINS2  
 NUMBER OF NOZZLES: 4  
 MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINS  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINS2  
 ATM. PRESSURE: 30.02 CINHGS

N	POR	DPOR	TOR	TUPT	TAMB	PUP	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF N2O	DEGREES F	IN OF N2O	IN OF N2O	IN OF N2O	IN OF N2O	IN OF N2O	IN OF N2O	SQARE INCHES	SQARE INCHES
1	0.71	22.2	60.2	112.2	69.4	3.20	3.10	0.00	0.000	*****
2	0.70	22.0	60.0	112.4	69.6	4.10	2.21	0.00	12.566	*****
3	0.70	21.9	60.2	112.6	69.6	4.69	1.56	0.00	25.133	*****
4	0.70	22.1	60.4	112.6	69.6	5.40	0.84	0.00	50.265	*****
5	0.70	22.0	60.4	113.0	69.0	5.90	0.31	0.00	100.531	*****
6	0.70	22.0	60.4	113.2	70.0	6.05	0.16	0.00	150.796	*****
7	0.70	22.0	60.6	113.4	70.2	6.20	0.01	0.00	*****	*****

SECONDARY BOX

N	M0	P0	T0	P0/T0	M0/T0	HP	MS	UP	UM	UUP	UPT	MACH
RUN									FT/SEC	FT/SEC		
1	0.0000	0.4263	0.9232	0.4600	0.0000	3.7575	0.0000	102.16	72.07	72.07	0.062	
2	0.1705	0.3002	0.9252	0.3245	0.1640	3.7412	0.6379	101.01	83.77	72.41	0.062	
3	0.2072	0.2135	0.9249	0.2300	0.2775	3.7320	1.0719	100.34	91.23	72.14	0.062	
4	0.4197	0.1144	0.9249	0.1237	0.4055	3.7403	1.5730	100.00	100.34	72.33	0.062	
5	0.3110	0.0425	0.9246	0.0459	0.4936	3.7390	1.9109	100.20	106.16	72.12	0.061	
6	0.3505	0.0219	0.9246	0.0237	0.5319	3.7390	2.0508	100.20	100.01	72.12	0.061	
7	0.0000	0.0007	0.9246	0.0007	0.0000	3.7391	1.0943	100.24	88.88	72.10	0.061	

TABLE 24 - PCD DATA FOR 10/10 NOZZLES WITH L/D=1.5 STACK

TERTIARY BOX

N	MT	PT	TT	PT/TT	MT/TT	44	MM	WT	UE
LBN/SEC LBN/SEC FT/SEC									
1	33333	0.0000	0.9252	0.0000	33333	3.757	33333	33333	33333
2	33333	0.0000	0.9252	0.0000	33333	4.379	33333	33333	33333
3	33333	0.0000	0.9249	0.0000	33333	4.804	33333	33333	33333
4	33333	0.0000	0.9249	0.0000	33333	5.321	33333	33333	33333
5	33333	0.0000	0.9246	0.0000	33333	5.651	33333	33333	33333
6	33333	0.0000	0.9246	0.0000	33333	5.799	33333	33333	33333
7	33333	0.0000	0.9246	0.0000	33333	33333	33333	33333	33333

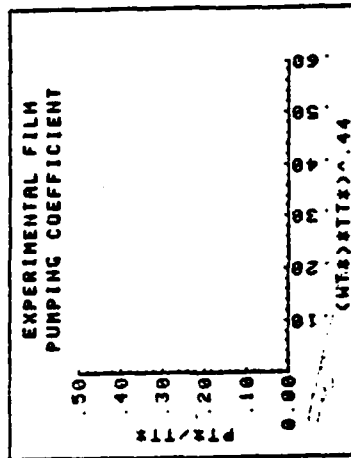
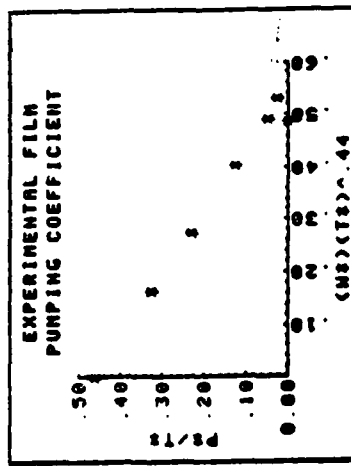


TABLE 24.1 - PCD DATA (CONT) FOR 10/10 NOZZLES WITH L/D=1.5 STACK



DATA TAKEN ON: 23 AUG 81  
 DATA TAKEN BY: C. C. DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 17.55 EINH  
 DIAMETER: 11.70 EINH  
 L/D RATIO: 1.50  
 S/D RATIO: 0.50

NOZZLE AN/AP AREA RATIO: 2.50

COMMENTS:  
 10 TILT/20 ROTATION/PCD

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 10.0 CDEGJ  
 ROTATION ANGLE: 20 CDEGJ  
 AREA PER NOZZLE: 10.752 EINH2J  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 EINH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 EINH2J  
 ATM. PRESSURE: 30.03 EINHGJ

N	POR	DPOR	TOR	TUPT	TANB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F					IN OF H2O		SQUARE INCHES	SQUARE INCHES
1	0.71	22.1	60.0	113.6	70.2	3.25	3.15	0.00	0.000	*****
2	0.70	21.9	60.2	113.6	70.2	4.15	2.13	0.00	12.566	*****
3	0.70	22.1	60.0	113.4	70.2	4.05	1.51	0.00	25.133	*****
4	0.70	22.0	60.2	113.4	70.4	5.45	0.79	0.00	50.265	*****
5	0.70	21.9	60.0	113.0	70.6	5.90	0.27	0.00	100.531	*****
6	0.70	21.9	61.0	113.0	70.6	6.05	0.14	0.00	150.796	*****
7	0.71	22.1	60.0	114.0	70.0	6.25	0.01	0.00	*****	*****

SECONDARY BOX

N	WS	PS	TS	PS/TS	WST	44	HP	WS	UP	UM	UPT	UPT MACH
RUN								LBM/SEC	LBM/SEC	FT/SEC	FT/SEC	
1	0.0000	0.4233	0.9243	0.4580	0.0000	0.0000	3.7475	0.0000	182.05	72.82	72.83	0.062
2	0.1677	0.2900	0.9243	0.3137	0.1620	0.1620	3.7326	0.6260	180.87	83.51	72.36	0.062
3	0.2811	0.2844	0.9246	0.2211	0.2715	0.2715	3.7504	1.0541	181.39	91.35	72.56	0.062
4	0.4075	0.1073	0.9250	0.1166	0.3930	0.3930	3.7412	1.5246	180.63	99.44	72.26	0.062
5	0.4770	0.0371	0.9247	0.0402	0.4616	0.4616	3.7305	1.7823	180.01	103.80	72.01	0.061
6	0.5161	0.0193	0.9247	0.0200	0.4987	0.4987	3.7290	1.9251	179.92	106.31	71.97	0.061
7	0.5555	0.0007	0.9247	0.0007	0.5388	0.5388	3.7475	1.0935	180.77	108.88	72.32	0.062

TABLE 25 - PCD DATA FOR 10/20 NOZZLES WITH L/D=1.5 STACK

TERTIARY BOX

N	WT	PT	TT	PTT	WT	44	MM	WT	UE
RUN							LBM/SEC	LBM/SEC	FT/SEC
1	220000	0.0000	0.9243	0.0000	220000	3.747	220000	220000	220000
2	220000	0.0000	0.9243	0.0000	220000	4.359	220000	220000	220000
3	220000	0.0000	0.9246	0.0000	220000	4.805	220000	220000	220000
4	220000	0.0000	0.9250	0.0000	220000	5.266	220000	220000	220000
5	220000	0.0000	0.9247	0.0000	220000	5.513	220000	220000	220000
6	220000	0.0000	0.9247	0.0000	220000	5.655	220000	220000	220000
7	220000	0.0000	0.9247	0.0000	220000	5.655	220000	220000	220000

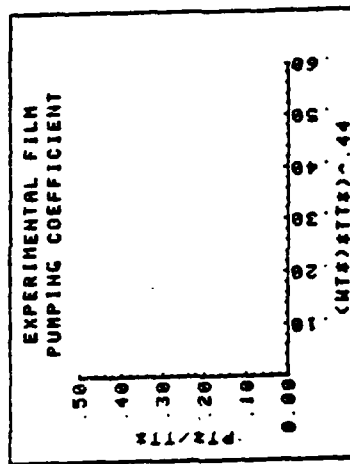
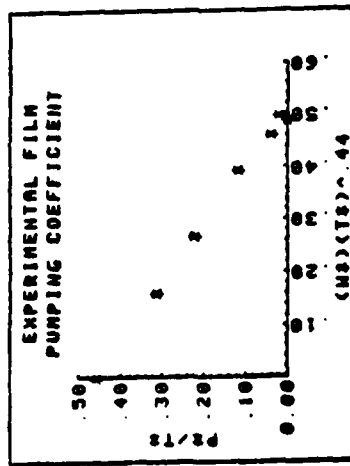


TABLE 25.1 - PCD DATA (CONT) FOR 10/20 NOZZLES WITH L/D=1.5 STACK

DATA TAKEN ON: 23 AUG 81  
DATA TAKEN BY: C.C. DAVIS

NOZZLE AN/AP AREA RATIO: 2.50 10 TILT/30 POTATION/PCD  
COMMENTS:  
MIXING STACK INFORMATION:  
LENGTH: 17.55 CINH  
DIAMETER: 11.70 CINH  
L/D RATIO: 1.50  
S/D RATIO: 0.50

PRIMARY NOZZLE INFORMATION:  
TILT ANGLE: 10.0 CODEG  
ROTATION ANGLE: 30 CODEG  
AREA PER NOZZLE: 10.752 CINH2  
NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
ORIFICE DIAMETER: 6.982 CINH  
ORIFICE BETA: 0.497  
UPTAKE AREA: 107.510 CINH2  
ATH. PRESSURE: 30.03 CINH2

N	POR	DPOR	TOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.72	22.3	60.4	113.6	70.0	3.45	3.04	0.00	0.000	*****
2	0.71	22.2	60.4	113.6	70.0	4.40	2.01	0.00	12.566	*****
3	0.71	22.1	60.4	113.0	71.0	4.95	1.37	0.00	25.133	*****
4	0.71	22.2	60.0	113.0	71.0	5.65	0.71	0.00	50.265	*****
5	0.71	22.3	60.4	113.0	71.0	6.05	0.25	0.00	100.531	*****
6	0.71	22.1	60.4	113.0	71.2	6.20	0.12	0.00	150.796	*****
7	0.70	22.0	60.4	113.0	71.4	6.20	0.01	0.00	*****	*****

SECONDARY BOX

N	W2	P2	T2	P2/T2	W2/T2	44	HP	WS	UP	UM	UUP	UPT	MACH
RUN								LBH/SEC	LBH/SEC	FT/SEC	FT/SEC	FT/SEC	
1	0.0900	0.4053	0.9253	0.4300	0.0000	0.0000	3.7658	0.0000	182.89	73.16	73.16	0.062	
2	0.1619	0.2711	0.9253	0.2930	0.1565	0.1565	3.7531	0.6077	181.81	83.57	72.73	0.062	
3	0.2676	0.1857	0.9254	0.2087	0.2587	0.2587	3.7489	1.0033	181.38	90.47	72.56	0.062	
4	0.3843	0.0961	0.9254	0.1030	0.3714	0.3714	3.7500	1.4445	181.57	98.42	72.63	0.062	
5	0.4573	0.0341	0.9254	0.0360	0.4420	0.4420	3.7489	1.7144	180.89	102.96	72.36	0.062	
6	0.4751	0.0164	0.9257	0.0177	0.4593	0.4593	3.7404	1.7013	180.03	104.14	72.34	0.062	
7	0.0000	0.0007	0.9261	0.0007	0.0000	0.0000	3.7404	1.0925	180.37	88.88	72.15	0.061	

TABLE 28 - PCD DATA FOR 10/30 NOZZLES WITH L/D=1.5 STACK

TERTIARY BOX

N	HTS	PTC	TTT	PTT/TTT	WTST	44	MM	HT	UE
RUN							LBM/SEC	LBM/SEC	FT/SEC
1	0.0000	0.0000	0.9253	0.0000	0.0000	0.0000	3.766	0.0000	0.0000
2	0.0000	0.0000	0.9253	0.0000	0.0000	0.0000	4.361	0.0000	0.0000
3	0.0000	0.0000	0.9254	0.0000	0.0000	0.0000	4.752	0.0000	0.0000
4	0.0000	0.0000	0.9254	0.0000	0.0000	0.0000	5.203	0.0000	0.0000
5	0.0000	0.0000	0.9254	0.0000	0.0000	0.0000	5.463	0.0000	0.0000
6	0.0000	0.0000	0.9257	0.0000	0.0000	0.0000	5.530	0.0000	0.0000
7	0.0000	0.0000	0.9261	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

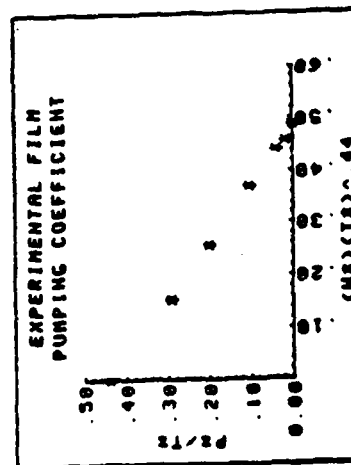
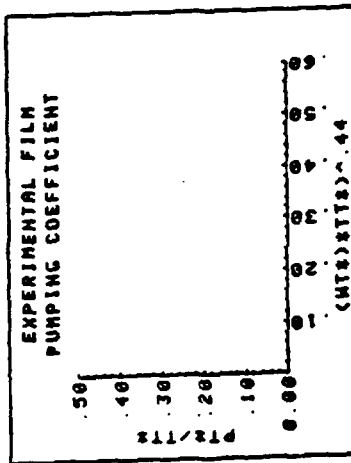


TABLE 26.1 - PCD DATA (CONT) FOR 10/30 NOZZLES WITH L/D=1.5 STACK

DATA TAKEN ON: 23 AUG 81  
 DATA TAKEN BY: C. C. DAVIS

NOZZLE AN/AP AREA RATIO: 2.50  
 10 TILT/40 ROTATION/PCD

MIXING STACK INFORMATION:  
 LENGTH: 17.55 INJ  
 DIAMETER: 11.70 INJ  
 L/D RATIO: 1.50  
 S/D RATIO: 0.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 10.0 DEGJ  
 ROTATION ANGLE: 40 DEGJ  
 AREA PER NOZZLE: 10.752 INJ2J  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 INJ  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 INJ2J  
 ATM. PRESSURE: 30.03 INJHGJ

N	POR	DPOR	TOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.71	22.0	60.4	113.0	71.4	3.55	2.20	0.00	0.000	0.000
2	0.70	21.9	60.6	113.0	71.2	4.50	1.83	0.00	12.566	0.000
3	0.71	22.2	59.0	113.6	71.4	5.15	1.25	0.00	25.133	0.000
4	0.70	22.1	60.4	113.6	71.4	5.75	0.62	0.00	50.265	0.000
5	0.70	22.0	60.2	113.0	71.6	6.15	0.21	0.00	100.531	0.000
6	0.71	22.1	60.0	113.6	71.6	6.25	0.11	0.00	150.796	0.000
7	0.71	22.1	60.2	113.6	71.8	6.35	0.01	0.00	0.000	0.000

# SECONDARY BOX

N	M8	P8	T8	PS/TS M8T8.44	HP	M8	UP	UM	UUP	UPT	MACH
RUN						LBM/SEC	LBM/SEC	FT/SEC	FT/SEC		
1	0.0000	0.2986	0.9261	0.3225	0.0000	3.7404	0.0000	181.34	72.34	72.34	0.062
2	0.1534	0.2500	0.9257	0.2701	0.1502	3.7312	0.5797	180.77	82.65	72.30	0.062
3	0.2540	0.1689	0.9264	0.1823	0.2464	3.7535	0.9580	181.70	89.83	72.72	0.062
4	0.3593	0.0845	0.9264	0.0912	0.3400	3.7409	1.3494	180.99	96.50	72.40	0.062
5	0.4190	0.0208	0.9264	0.0311	0.4059	3.7412	1.5704	180.50	100.27	72.20	0.062
6	0.4546	0.0150	0.9267	0.0162	0.4396	3.7503	1.7040	180.03	102.00	72.34	0.062
7	0.0000	0.0007	0.9271	0.0007	0.0000	3.7496	1.0917	180.75	0.0000	72.31	0.062

TABLE 27 - PCD DATA FOR 10/40 NOZZLES WITH L/D=1.5 STACK

TERTIARY BOX

N	NTS	PTS	ITS	PTI/ITI	MTITI^44	NH	NT	UE
LBM/SEC LBM/SEC FT/SEC								
RUN								
1	0.0000	0.0000	0.9261	0.0000	0.0000	3.740	0.0000	0.0000
2	0.0000	0.0000	0.9257	0.0000	0.0000	4.311	0.0000	0.0000
3	0.0000	0.0000	0.9264	0.0000	0.0000	4.710	0.0000	0.0000
4	0.0000	0.0000	0.9264	0.0000	0.0000	5.096	0.0000	0.0000
5	0.0000	0.0000	0.9264	0.0000	0.0000	5.312	0.0000	0.0000
6	0.0000	0.0000	0.9267	0.0000	0.0000	5.455	0.0000	0.0000
7	0.0000	0.0000	0.9271	0.0000	0.0000	0.0000	0.0000	0.0000

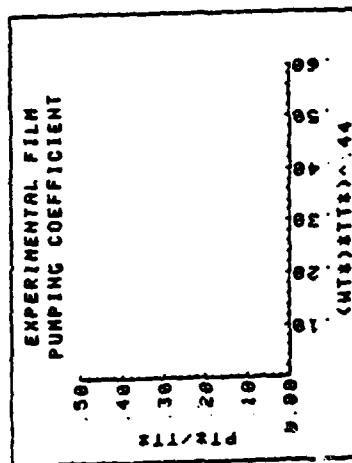
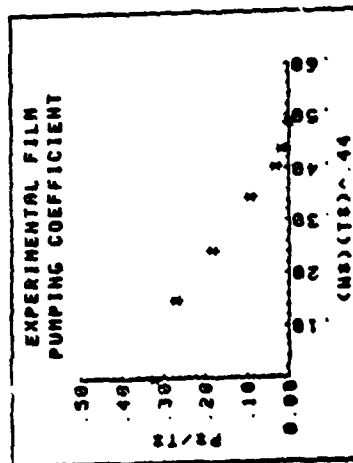


TABLE 27.1 - PCD DATA (CONT) FOR 10/40 NOZZLES WITH L/D=1.5 STACK

DATA TAKEN ON: 23 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 17.55 EINH  
 DIAMETER: 11.78 EINH  
 L/D RATIO: 1.50  
 S/D RATIO: 0.50

NOZZLE MM/AP AREA RATIO: 2.50

COMMENTS:  
 15 TILT/10 POTATION/PCD

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 15.0 COEG3  
 ROTATION ANGLE: 10 EDEG3  
 AREA PER NOZZLE: 10.752 EINH23  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 EINH3  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 EINH23  
 ATM. PRESSURE: 30.03 EINHG3

M	POR	OPOR	TOR	TUPT	TANB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F			IN OF H2O				SQUARE INCHES	SQUARE INCHES
1	0.70	22.2	59.6	113.4	70.4	3.45	3.07	0.00	0.000	0.000
2	0.70	22.1	59.0	113.2	70.4	4.25	2.19	0.00	12.566	0.000
3	0.70	21.9	60.2	113.4	70.4	4.75	1.56	0.00	25.133	0.000
4	0.70	21.0	59.0	113.4	70.6	5.40	0.87	0.00	50.265	0.000
5	0.70	22.1	60.0	113.4	70.0	6.00	0.33	0.00	100.531	0.000
6	0.70	22.0	59.2	113.2	70.0	6.15	0.17	0.00	150.796	0.000
7	0.70	22.0	60.0	113.4	71.0	6.27	0.01	0.00	0.000	0.000

SECONDARY BOX

M	WS	PS	Tz	PS/TS	MS/T-44	MP	WS	UP	UX	UPT	UPT MACH
RUN							LBM/SEC	LBM/SEC	FT/SEC	FT/SEC	
1	0.0000	0.4104	0.9250	0.4437	0.0000	3.7603	0.0000	102.57	73.03	73.04	0.062
2	0.1692	0.2957	0.9253	0.3195	0.1635	3.7511	0.6346	101.67	83.99	72.67	0.062
3	0.2070	0.2132	0.9250	0.2305	0.2773	3.7327	1.0712	100.56	91.33	72.23	0.062
4	0.4294	0.1190	0.9253	0.1295	0.4150	3.7256	1.5996	179.91	100.50	71.97	0.061
5	0.5253	0.0450	0.9257	0.0486	0.5077	3.7504	1.9700	100.07	107.50	72.35	0.062
6	0.5664	0.0233	0.9260	0.0251	0.5475	3.7440	2.1210	100.46	110.03	72.19	0.062
7	0.0000	0.0007	0.9260	0.0007	0.0000	3.7419	1.0932	100.31	0.0000	72.13	0.061

TABLE 28 - PCD DATA FOR 15/10 NOZZLES WITH L/D=1.5 STACK

TERTIARY BOX

N	WT8	PT8	TT8	PT8/TT8	WT8TT8-44	HM	HT	UE
RUN						LBN/SEC	LBN/SEC	FT/SEC
1	333333	0.0000	0.9250	0.0000	333333	3.760	333333	333333
2	333333	0.0000	0.9253	0.0000	333333	4.386	333333	333333
3	333333	0.0000	0.9250	0.0000	333333	4.804	333333	333333
4	333333	0.0000	0.9253	0.0000	333333	5.325	333333	333333
5	333333	0.0000	0.9257	0.0000	333333	5.720	333333	333333
6	333333	0.0000	0.9260	0.0000	333333	5.866	333333	333333
7	333333	0.0000	0.9260	0.0000	333333	333333	333333	333333

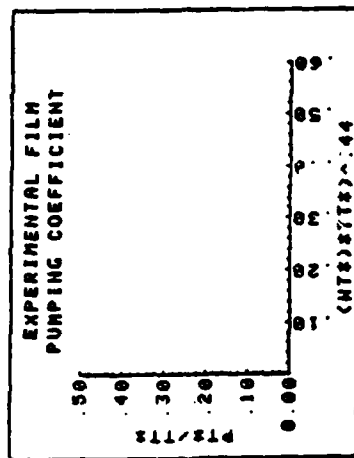
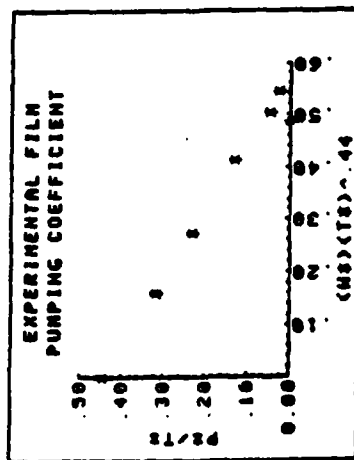


TABLE 28.1 - PCD DATA FOR 15/10 NOZZLES WITH L/D-1.5 STACK



DATA TAKEN ON: 23 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

NOZZLE AM/AP AREA RATIO: 2.50  
 15 TILT/20 ROTATION/PCD

COMMENTS:  
 MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.982 E1N3  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 E1N23  
 ATM. PRESSURE: 30.03 E1NMG3

MIXING STACK INFORMATION:  
 LENGTH: 17.55 E1N3  
 DIAMETER: 11.70 E1N3  
 L/D RATIO: 1.50  
 S/D RATIO: 0.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 13.0 E0EG3  
 ROTATION ANGLE: 20 E0EG3  
 AREA PER NOZZLE: 10.752 E1N23  
 NUMBER OF NOZZLES: 4

N	POR	DPOR	TOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF N2O	DEGREES F	IN OF N2O	IN OF N2O	IN OF N2O	IN OF N2O	IN OF N2O	IN OF N2O	SQUARE INCHES	SQUARE INCHES
1	0.70	22.1	59.2	112.8	70.8	3.25	3.11	0.00	0.000	0.000
2	0.70	21.9	59.4	112.8	70.8	4.10	2.21	0.00	12.566	0.000
3	0.70	22.0	59.0	112.8	70.8	4.75	1.59	0.00	25.133	0.000
4	0.71	22.2	59.0	112.6	70.8	5.45	0.89	0.00	50.265	0.000
5	0.71	22.1	59.2	112.6	71.0	6.00	0.33	0.00	100.531	0.000
6	0.71	22.1	59.8	112.4	71.2	6.15	0.17	0.00	150.796	0.000
7	0.71	22.2	59.0	112.6	71.2	6.30	0.01	0.00	0.000	0.000

# SECONDARY BOX

N	Ms	Pz	Tz	Pz/Tz	Mz/Tz	44	HP	WS	UP	UM	UPT	UPT MACH
RUN												
1	0.8240	0.4184	0.9266	0.4515	0.0000	3.7533	0.0000	102.06	72.83	72.83	0.062	0.062
2	0.1786	0.3015	0.9265	0.3254	0.1650	3.7355	0.6373	100.00	03.69	72.32	0.062	0.062
3	0.2086	0.2164	0.9266	0.2335	0.2791	3.7455	1.0011	101.00	91.70	72.41	0.062	0.062
4	0.4239	0.1203	0.9270	0.1300	0.4150	3.7624	1.6176	101.44	101.45	72.50	0.062	0.062
5	0.5240	0.0451	0.9273	0.0406	0.5077	3.7532	1.9697	100.75	107.46	72.31	0.062	0.062
6	0.5647	0.0232	0.9200	0.0250	0.5464	3.7547	2.1202	100.69	110.14	72.20	0.062	0.062
7	0.0000	0.0007	0.9277	0.0007	0.0000	3.7624	1.0020	101.05	0.0000	72.43	0.062	0.062

TABLE 20 - PCD DATA FOR 15/20 NOZZLES WITH L/D=1.5 STACK

TERTIARY BOX

N	WT	PT	TT	PT/TT	WT/TT	WT	UE
1	0.0000	0.0000	0.9266	0.0000	0.0000	3.753	0.0000
2	0.0000	0.0000	0.9266	0.0000	0.0000	4.373	0.0000
3	0.0000	0.0000	0.9266	0.0000	0.0000	4.827	0.0000
4	0.0000	0.0000	0.9270	0.0000	0.0000	5.380	0.0000
5	0.0000	0.0000	0.9273	0.0000	0.0000	5.723	0.0000
6	0.0000	0.0000	0.9280	0.0000	0.0000	5.875	0.0000
7	0.0000	0.0000	0.9277	0.0000	0.0000	0.0000	0.0000

LBM/SEC LBM/SEC FT/SEC

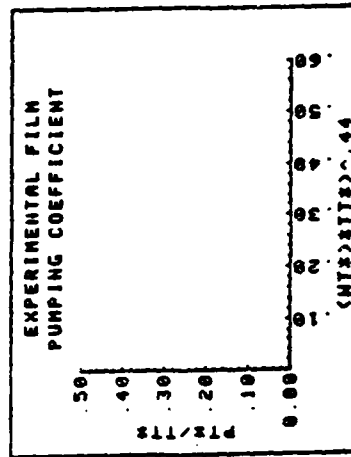
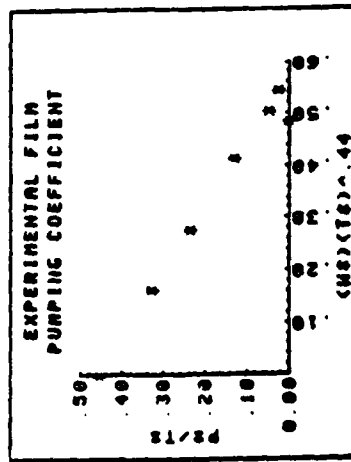


TABLE 29.1 - PCD DATA (CONT) FOR 15/20 NOZZLES WITH L/D=1.5 STACK

DATA TAKEN ON: 24 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 17.55 CINH  
 DIAMETER: 11.78 CINH  
 L/D RATIO: 1.50  
 S/D RATIO: 0.50

NOZZLE AN/AP AREA RATIO: 2.50

COMMENTS:  
 15 TILT/20 POTATION/FULL PUN

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 15.0 CDEGJ  
 ROTATION ANGLE: 20 CDEGJ  
 AREA PER NOZZLE: 10.752 CINH2  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINH2  
 ATN. PRESSURE: 30.02 CINH2

N	POR	DPOR	TOR	TUPT	TAMB	PAPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.71	22.0	59.0	111.6	69.0	3.25	3.11	0.00	0.000	0.000
2	0.70	22.1	58.0	111.6	69.0	4.15	2.23	0.00	12.566	0.000
3	0.70	22.0	59.2	112.0	70.0	4.65	1.61	0.00	25.133	0.000
4	0.71	22.2	59.0	112.0	70.2	5.45	0.90	0.00	50.265	0.000
5	0.71	22.1	59.2	112.0	70.2	6.00	0.32	0.00	100.531	0.000
6	0.71	22.1	58.0	112.0	70.4	6.15	0.17	0.00	150.796	0.000
7	0.71	22.0	59.0	112.2	70.6	6.30	0.01	0.00	0.000	0.000

# SECONDARY BOX

N	WS	PS	TS	PS/TS	WAT-44	WP	WS	UP	UN	UPT	UPT MACH
RUN							LBM/SEC	LBM/SEC	FT/SEC	FT/SEC	
1	0.0000	0.4211	0.9260	0.4344	0.0000	3.7440	0.0000	181.33	72.54	72.54	0.062
2	0.1706	0.3010	0.9260	0.3256	0.1650	3.7541	0.6406	181.30	93.97	72.56	0.062
3	0.2907	0.2195	0.9265	0.2369	0.2011	3.7441	1.0805	180.75	91.71	72.31	0.062
4	0.4326	0.1220	0.9269	0.1316	0.4104	3.7610	1.6273	181.29	101.53	72.52	0.062
5	0.5172	0.0437	0.9269	0.0472	0.5082	3.7526	1.9487	180.59	106.04	72.24	0.062
6	0.5651	0.0232	0.9272	0.0251	0.5466	3.7541	2.1214	180.59	110.00	72.24	0.062
7	0.0000	0.0014	0.9273	0.0015	0.0000	3.7440	2.6779	180.14	0.0000	72.06	0.061

TABLE 30 - PCD DATA FOR 15/20 NOZZLES WITH L/D-1.5 STACK (FULL RUN)

TERTIARY BOX

W	WTB	PTB	YTB	PTB/TTB	WTTB	HT	UE
					44		
LBH/SEC	LBH/SEC	FT/SEC					
LBH/SEC	LBH/SEC	FT/SEC					
1	0.0000	0.9268	0.0000	0.0000	3.745	0.0000	0.0000
2	0.0000	0.9268	0.0000	0.0000	4.395	0.0000	0.0000
3	0.0000	0.9265	0.0000	0.0000	4.833	0.0000	0.0000
4	0.0000	0.9269	0.0000	0.0000	5.389	0.0000	0.0000
5	0.0000	0.9269	0.0000	0.0000	5.693	0.0000	0.0000
6	0.0000	0.9272	0.0000	0.0000	5.875	0.0000	0.0000
7	0.0000	0.9273	0.0000	0.0000	0.0000	0.0000	0.0000

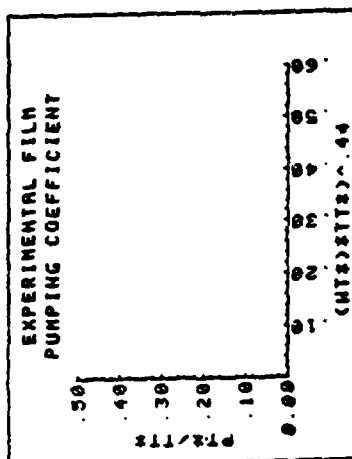
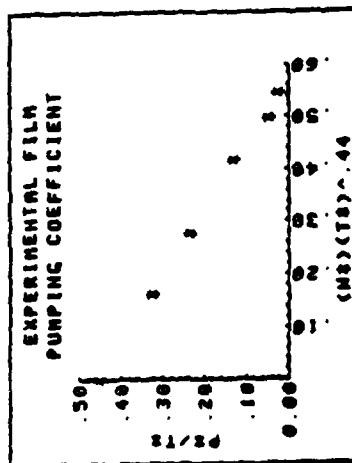


TABLE 30.1 - PCD DATA (CONT) FOR 15/20 NOZZLES WITH L/D=1.5 STACK

# MIXING STACK DATA FOR RUN 7

TOP (POSITION 'A') DATA				DIAGONAL (POSITION 'B') DATA			
X/D	PRESSURE EIN H2O3	ROTATION EDEC3	PMS*	X/D	PRESSURE EIN H2O3	ROTATION EDEC3	PMS*
0.00	-2.440	04	-0.335	0.00	-1.590	04	-0.210
0.25	-1.215	24	-0.167	0.25	-1.060	24	-0.146
0.50	-0.970	22	-0.133	0.50	-0.790	22	-0.109
0.75	-0.800	24	-0.110	0.75	-0.695	24	-0.095
1.00	-0.660	22	-0.091	1.00	-0.375	22	-0.052
1.25	-0.360	12	-0.049	1.25	-0.210	12	-0.029

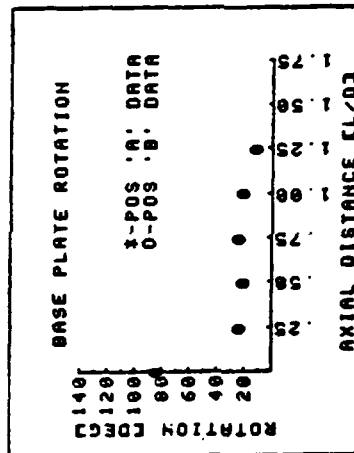
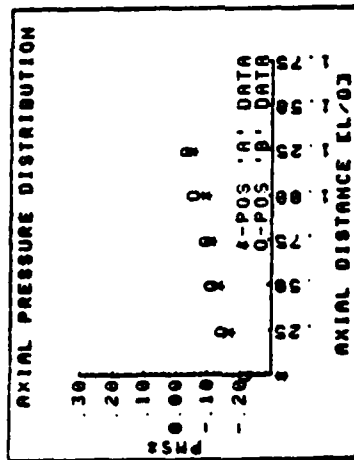
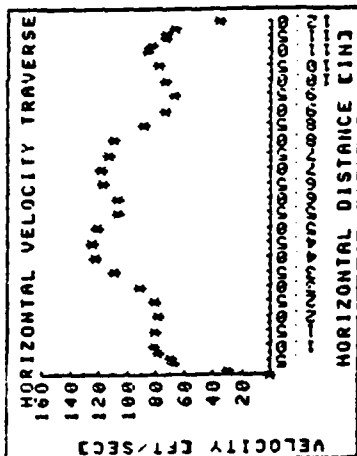


TABLE 30.2 - MSD DATA FOR 15/20 NOZZLES WITH L/D-1.5 STACK

# HORIZONTAL VELOCITY TRAVERSE AT BASE ROTATION OF 94 DEGREES

POSITION:	0.00	0.20	0.40	0.60	0.80	1.00	1.50
PEIN H203:	0.00	0.20	1.00	1.10	1.40	1.50	1.50
VEFT/SEC:	0.00	29.86	66.77	70.03	79.01	81.78	81.78
POSITION:	2.00	2.50	3.00	3.50	4.00	4.50	5.00
PEIN H203:	1.40	1.50	1.90	2.70	3.40	3.50	3.30
VEFT/SEC:	79.01	81.78	92.04	109.72	123.13	124.92	121.30
POSITION:	5.50	6.00	6.50	7.00	7.50	8.00	8.50
PEIN H203:	2.60	2.60	3.10	3.20	2.90	2.70	1.80
VEFT/SEC:	107.67	117.57	119.45	113.71	109.72	109.59	89.59
POSITION:	9.00	9.50	10.00	10.50	11.00	11.20	11.40
PEIN H203:	1.20	1.00	1.20	1.40	1.70	1.60	1.20
VEFT/SEC:	73.15	66.77	73.15	79.01	87.06	84.46	73.15
POSITION:	11.60	11.80	12.00				
PEIN H203:	1.20	1.00	0.30				



# DIAGONAL VELOCITY TRAVERSE FOR BASE ROTATION OF 94 DEGREES

POSITION:	0.00	0.20	0.40	0.60	0.80	1.00	1.50
PEIN H203:	0.00	1.20	3.50	4.00	4.40	4.50	4.60
VEFT/SEC:	0.00	73.15	124.92	133.55	140.07	141.65	143.22
POSITION:	2.00	2.50	3.00	3.50	4.00	4.50	5.00
PEIN H203:	4.10	3.40	3.10	3.00	3.40	3.50	3.20
VEFT/SEC:	135.21	123.13	117.57	115.66	123.13	124.92	119.45
POSITION:	5.50	6.00	6.50	7.00	7.50	8.00	8.50
PEIN H203:	2.60	2.70	3.10	3.30	2.90	2.70	2.90
VEFT/SEC:	107.67	109.72	117.57	121.30	113.71	109.72	113.71
POSITION:	9.00	9.50	10.00	10.50	11.00	11.20	11.40
PEIN H203:	3.20	3.50	4.10	4.20	4.10	3.40	3.10
VEFT/SEC:	119.45	124.92	135.21	136.05	135.21	123.13	117.57
POSITION:	11.60	11.80	12.00				
PEIN H203:	2.70	2.30	0.40				

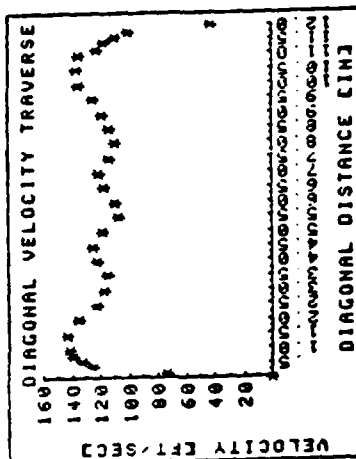


TABLE 30.3 - VTD DATA FOR 15/20 NOZZLES WITH L/D=1.5 STACK

DATA TAKEN ON: 23 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 17.55 CINH  
 DIAMETER: 11.70 CINH  
 L/D RATIO: 1.50  
 S/D RATIO: 0.50

NOZZLE AN/AP AREA RATIO: 2.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 15.0 COEG3  
 ROTATION ANGLE: 30 IDEG3  
 AREA PER NOZZLE: 10.752 CINH2  
 NUMBER OF NOZZLES: 4

COMMENTS:  
 15 TILT/30 ROTATION/PCD

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINH2  
 ATM. PRESSURE: 30.03 CINH2

N	POR	DPOR	YOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O			DEGREES F			IN OF H2O		SQUARE INCHES	SQUARE INCHES
1	0.70	22.0	50.4	112.2	71.0	3.30	3.09	0.00	0.000	xxxxxx
2	0.70	21.9	50.4	112.2	71.0	4.20	2.16	0.00	12.566	xxxxxx
3	0.71	22.1	50.4	112.2	71.0	4.00	1.57	0.00	25.133	xxxxxx
4	0.70	22.0	50.2	112.0	71.2	5.45	0.86	0.00	50.265	xxxxxx
5	0.70	21.9	50.0	112.2	71.2	6.00	0.31	0.00	100.531	xxxxxx
6	0.70	22.1	50.4	112.2	71.2	6.15	0.16	0.00	150.795	xxxxxx
7	0.70	22.0	50.4	112.0	71.4	6.30	0.01	0.00	xxxxxx	xxxxxx

# SECONDARY BOX

N	WS	PS	YS	PS/TS	WST-44	MP	WS	UP	UN	UUPY	UPT	MACH
RUN							LBM/SEC	LBM/SEC	FT/SEC	FT/SEC		
1	0.0000	0.4100	0.9200	0.4505	0.0000	3.7476	0.0000	181.59	72.64	72.64	0.062	
2	0.1605	0.2949	0.9200	0.3170	0.1630	3.7391	0.6299	180.76	83.55	72.31	0.062	
3	0.2059	0.2130	0.9200	0.2296	0.2767	3.7561	1.0741	181.32	91.70	72.53	0.062	
4	0.4241	0.1177	0.9206	0.1268	0.4105	3.7484	1.5895	180.56	100.61	72.23	0.062	
5	0.5107	0.0428	0.9203	0.0461	0.4942	3.7377	1.9087	179.87	106.04	71.95	0.061	
6	0.5476	0.0219	0.9203	0.0236	0.5300	3.7562	2.0569	180.69	109.01	72.20	0.062	
7	xxxxxx	0.0007	0.9200	0.0007	xxxxxx	3.7477	1.0925	180.15	xxxxxx	72.07	0.061	

TABLE 31 - PCD DATA FOR 15/30 NOZZLES WITH L/D=1.5 STACK

TERTIARY BOX

N	WT	PT	TT	PT/TT	WT/TT	WT	UE
PUN							
1	3.746	0.0000	0.9280	0.0000	3.746	3.746	0.0000
2	4.369	0.0000	0.9280	0.0000	4.369	4.369	0.0000
3	4.830	0.0000	0.9280	0.0000	4.830	4.830	0.0000
4	5.338	0.0000	0.9280	0.0000	5.338	5.338	0.0000
5	5.646	0.0000	0.9280	0.0000	5.646	5.646	0.0000
6	5.813	0.0000	0.9280	0.0000	5.813	5.813	0.0000
7	5.813	0.0000	0.9280	0.0000	5.813	5.813	0.0000

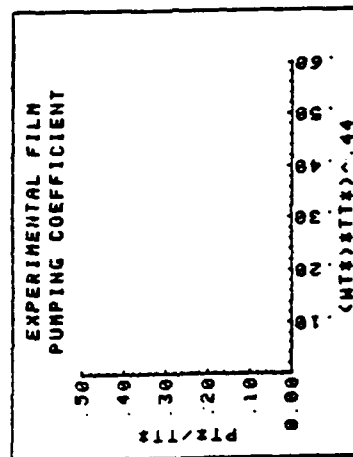
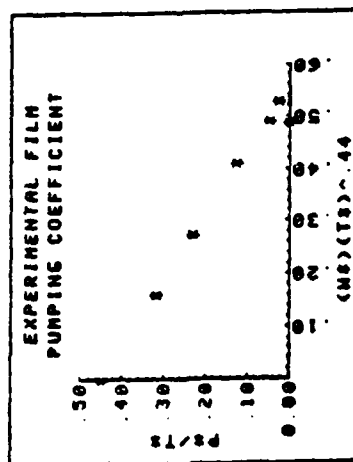


TABLE 31.1 - PCD DATA (CONT) FOR 15/30 NOZZLES WITH L/D=1.5 STACK



DATA TAKEN ON: 24 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 17.55 L INJ  
 DIAMETER: 11.70 L INJ  
 L/D RATIO: 1.50  
 S/D RATIO: 0.50

NOZZLE AN/AP AREA RATIO: 2.50

COMMENTS:  
 20 TILT/10 ROTATION/PCD

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.982 L INJ  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 L INJ  
 ATM. PRESSURE: 30.03 L INJ

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 20.0 CDEGJ  
 ROTATION ANGLE: 10 CDEGJ  
 AREA PER NOZZLE: 10.752 L INJ  
 NUMBER OF NOZZLES: 4

N	POR	DPOR	TOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA SQUARE INCHES	TERTIARY AREA SQUARE INCHES
RUN	IN OF H2O	DEGREES F				IN OF H2O				
1	0.71	22.1	57.6	111.6	72.0	3.80	2.86	0.00	0.000	xxxxxx
2	0.70	22.0	57.0	111.4	71.6	4.43	1.97	0.00	12.566	xxxxxx
3	0.70	22.1	57.8	111.6	71.6	4.35	1.44	0.00	25.133	xxxxxx
4	0.70	22.1	57.6	111.6	71.6	5.53	0.00	0.00	50.265	xxxxxx
5	0.70	22.0	57.6	111.6	71.6	6.00	0.30	0.00	100.531	xxxxxx
6	0.70	22.0	57.2	111.2	71.0	6.15	0.16	0.00	150.796	xxxxxx
7	0.70	22.0	57.2	111.2	71.0	6.25	0.01	0.00	xxxxxx	xxxxxx

SECONDARY BOX

N	MS	Pz	Tz	Pz/Tz WGT-44	MP	WS	UP	UN	UUP	UPT	MACH
RUN						LBM/SEC	LBM/SEC	FT/SEC	FT/SEC		
1	0.0000	0.3865	0.9307	0.4153	0.0000	3.7520	0.0000	101.84	72.74	72.74	0.062
2	0.1602	0.2683	0.9303	0.2084	0.1552	3.7527	0.6012	101.00	83.10	72.44	0.062
3	0.2735	0.1959	0.9300	0.2107	0.2649	3.7583	1.0281	101.17	90.05	72.40	0.062
4	0.4077	0.1091	0.9300	0.1174	0.3949	3.7591	1.5325	100.92	99.76	72.30	0.062
5	0.5004	0.0412	0.9300	0.0443	0.4847	3.7505	1.0769	100.29	105.65	72.12	0.062
6	0.5479	0.0220	0.9310	0.0237	0.5309	3.7520	2.0557	100.10	100.02	72.08	0.062
7	0.5833	0.0014	0.9310	0.0015	0.5833	3.7520	2.6753	100.11	xxxxxx	72.05	0.062

TABLE 32 - PCD DATA FOR 20/10 NOZZLES WITH L/D=1.5 STACK

# TERTIARY BOX

N	NTS	PTA	ITT	PT3/112	NT3YT	44	NH	HT	UE
RUN							LBM/SEC	LBM/SEC	FT/SEC
1	0.0000	0.0000	0.9307	0.0000	0.0000	0.0000	3.759	0.0000	0.0000
2	0.0000	0.0000	0.9303	0.0000	0.0000	0.0000	4.354	0.0000	0.0000
3	0.0000	0.0000	0.9300	0.0000	0.0000	0.0000	4.786	0.0000	0.0000
4	0.0000	0.0000	0.9300	0.0000	0.0000	0.0000	5.292	0.0000	0.0000
5	0.0000	0.0000	0.9300	0.0000	0.0000	0.0000	5.627	0.0000	0.0000
6	0.0000	0.0000	0.9310	0.0000	0.0000	0.0000	5.000	0.0000	0.0000
7	0.0000	0.0000	0.9310	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

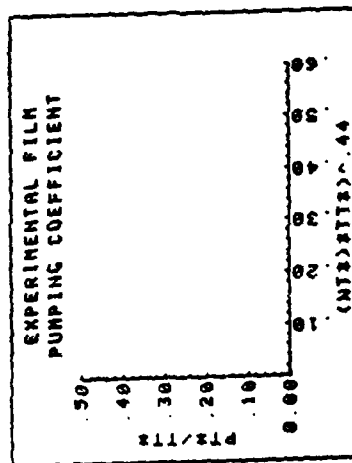
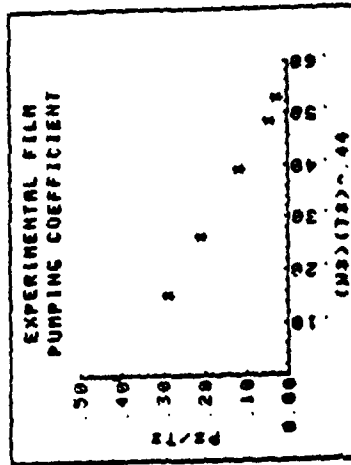


TABLE 32.1 - PCD DATA (CONT) FOR 20/10 NOZZLES WITH L/D=1.5 STACK

DATA TAKEN ON: 24 AUG 81  
DATA TAKEN BY: C.C. DAVIS

NOZZLE RH/AP AREA RATIO: 2.50  
20 TILT/20 ROTATION/PCD

COMMENTS:

MIXING STACK INFORMATION:  
LENGTH: 17.55 INJ  
DIAMETER: 11.78 INJ  
L/D RATIO: 1.50  
S/D RATIO: 0.50

PRIMARY NOZZLE INFORMATION:  
TILT ANGLE: 20.0 DEGCJ  
ROTATION ANGLE: 20 DEGCJ  
AREA PER NOZZLE: 10.752 INJ2J  
NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
ORIFICE DIAMETER: 6.902 INJ  
ORIFICE BETA: 0.497  
UPTAKE AREA: 107.510 INJ2J  
ATM. PRESSURE: 30.03 INJHGJ

N	FOR	DPOR	TOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.71	22.2	57.4	111.4	71.6	3.55	2.94	0.00	0.000	0.000
2	0.70	22.1	57.2	111.2	71.4	4.25	2.14	0.00	12.566	0.000
3	0.70	22.0	57.0	111.0	71.4	4.80	1.51	0.00	25.133	0.000
4	0.70	22.1	57.4	111.4	71.4	5.45	0.83	0.00	50.265	0.000
5	0.70	22.0	57.2	111.4	71.4	5.90	0.31	0.00	100.531	0.000
6	0.70	22.1	57.0	111.6	71.4	6.10	0.16	0.00	150.796	0.000
7	0.70	22.0	57.0	111.6	71.6	6.25	0.01	0.00	0.000	0.000

SECONDARY BOX

N	MS	PS	TS	PS/TS	MS/TS	HP	NS	UP	UN	UPT	UPT MACH
RUN						LBM/SEC	LBM/SEC	FT/SEC	FT/SEC	FT/SEC	
1	0.0000	0.3952	0.9303	0.4240	0.0000	3.7683	0.0000	102.26	72.91	72.91	0.062
2	0.1667	0.2901	0.9303	0.3119	0.1614	3.7685	0.6267	101.46	83.79	72.59	0.062
3	0.2806	0.2063	0.9306	0.2217	0.2710	3.7527	1.0529	100.75	91.11	72.30	0.062
4	0.4133	0.1132	0.9300	0.1217	0.4022	3.7598	1.5613	100.91	100.26	72.37	0.062
5	0.5086	0.0426	0.9300	0.0450	0.4926	3.7520	1.9003	100.31	106.22	72.13	0.062
6	0.5472	0.0219	0.9296	0.0236	0.5299	3.7503	2.0563	100.61	100.90	72.25	0.062
7	0.0000	0.0014	0.9300	0.0015	0.0000	3.7490	2.0758	100.13	0.0000	72.06	0.062

TABLE 33 - PCD DATA FOR 20/20 NOZZLES WITH L/D=1.5 STACK

TERTIARY BOX

N	WT	PT	TT	PTT/TT	WT/TT	WT	UE
1	3.768	0.0000	0.9303	0.0000	3.768	0.0000	0.0000
2	4.397	0.0000	0.9303	0.0000	4.397	0.0000	0.0000
3	4.806	0.0000	0.9306	0.0000	4.806	0.0000	0.0000
4	5.321	0.0000	0.9300	0.0000	5.321	0.0000	0.0000
5	5.660	0.0000	0.9300	0.0000	5.660	0.0000	0.0000
6	5.815	0.0000	0.9296	0.0000	5.815	0.0000	0.0000
7	5.815	0.0000	0.9300	0.0000	5.815	0.0000	0.0000

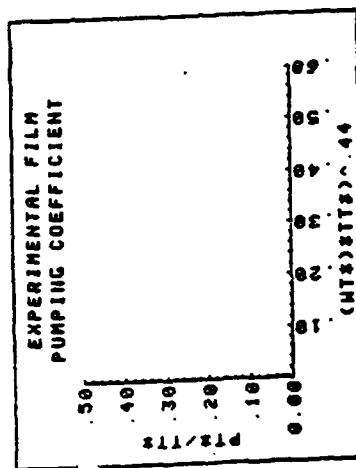
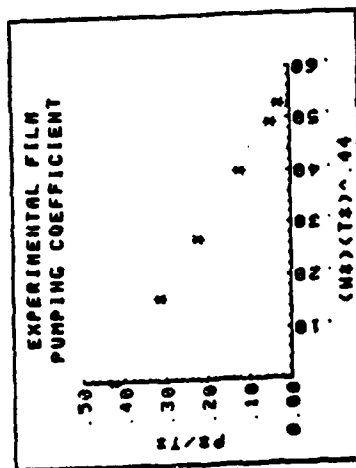


TABLE 33.1 - PCD DATA (CONT) FOR 20/20 NOZZLES WITH L/D=1.5 STACK

DATA TAKEN ON: 24 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 17.55 EINH  
 DIAMETER: 11.70 EINH  
 L/D RATIO: 1.50  
 S/D RATIO: 0.50

NOZZLE AM/OP AREA RATIO: 2.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 20.0 DEGR  
 ROTATION ANGLE: 30 DEGR  
 AREA PER NOZZLE: 10.752 EINH  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 EINH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 EINH  
 ATM. PRESSURE: 30.03 EINH

COMMENTS:  
 20 TILT/30 POTATION/PCD

N	POR	OPOR	TOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.70	22.0	57.4	111.4	71.2	3.20	3.07	0.00	0.000	xxxxxx
2	0.71	22.2	57.6	111.4	71.2	4.15	2.20	0.00	12.566	xxxxxx
3	0.71	22.2	57.0	111.2	71.2	4.75	1.57	0.00	25.133	xxxxxx
4	0.70	22.0	56.0	111.2	71.2	5.35	0.07	0.00	50.265	xxxxxx
5	0.70	22.1	57.2	111.2	71.2	5.95	0.33	0.00	100.531	xxxxxx
6	0.70	22.1	57.0	111.0	71.2	6.10	0.10	0.00	150.796	xxxxxx
7	0.70	22.0	57.0	111.2	71.4	6.25	0.01	0.00	xxxxxx	xxxxxx

# SECONDARY BOX

N	MS	P3	T3	PS/TS	MS/TS	HP	HS	UP	UM	UPT	UPT	MACH
RUN							LBN/SEC	LBN/SEC	FT/SEC	FT/SEC		
1	0.000	0.4159	0.9296	0.4474	0.0000	3.7513	0.0000	101.50	72.60	72.61	0.062	
2	0.1687	0.2967	0.9296	0.3192	0.1634	3.7675	0.6356	101.09	84.11	72.76	0.062	
3	0.2849	0.2123	0.9299	0.2203	0.2759	3.7697	1.0739	101.65	91.04	72.67	0.062	
4	0.4259	0.1191	0.9299	0.1201	0.4125	3.7534	1.5987	100.56	100.70	72.23	0.062	
5	0.5237	0.0451	0.9299	0.0405	0.5072	3.7605	1.9693	100.66	107.43	72.27	0.062	
6	0.5000	0.0246	0.9303	0.0265	0.5619	3.7612	2.1016	100.57	111.19	72.23	0.062	
7	0.0000	0.0014	0.9303	0.0015	0.0000	3.7527	2.6763	100.15	xxxxxx	72.06	0.062	

TABLE 34 - PCD DATA FOR 20/30 NOZZLES WITH L/D=1.5 STACK

VERTIARY BOX

N	WT	PT	TT	PT/TT	WT/TT	WT	UE
RUN							
1	0.0000	0.0000	0.9296	0.0000	0.0000	2.751	0.0000
2	0.0000	0.0000	0.9296	0.0000	0.0000	4.483	0.0000
3	0.0000	0.0000	0.9299	0.0000	0.0000	4.844	0.0000
4	0.0000	0.0000	0.9299	0.0000	0.0000	5.352	0.0000
5	0.0000	0.0000	0.9299	0.0000	0.0000	5.730	0.0000
6	0.0000	0.0000	0.9303	0.0000	0.0000	5.943	0.0000
7	0.0000	0.0000	0.9303	0.0000	0.0000	0.0000	0.0000

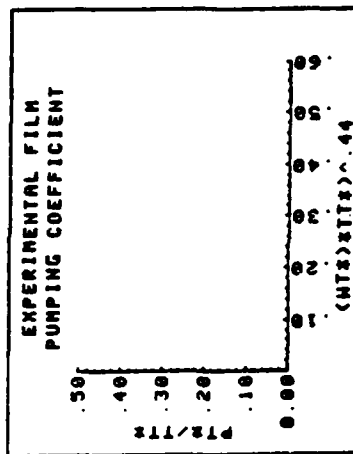
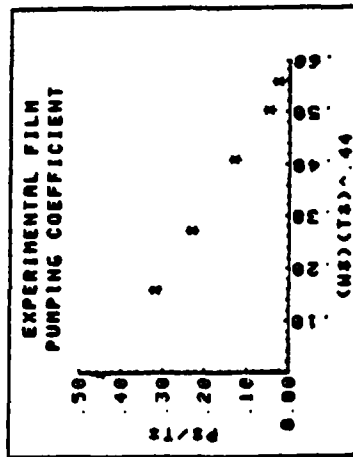


TABLE 34.1 - PCD DATA (CONT) FOR 20/30 NOZZLES WITH L/D-1.5 STACK

DATA TAKEN ON: 24 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 17.55 CINH  
 DIAMETER: 11.70 CINH  
 L/D RATIO: 1.50  
 S/D RATIO: 0.50

NOZZLE AN/AP AREA RATIO: 2.50

COMMENTS:  
 22.5 TILT/10 ROTATION/PCD

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 22.5 CDEGJ  
 ROTATION ANGLE: 10 CDEGJ  
 AREA PER NOZZLE: 10.752 CINHJ  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINHJ  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINHJ  
 ATM. PRESSURE: 30.03 CINHJ

N	POR	DPOR	TOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.71	22.1	56.6	110.6	71.4	4.15	2.78	0.00	0.000	0.000
2	0.70	21.9	57.2	110.0	71.2	4.75	1.92	0.00	12.566	0.000
3	0.71	22.2	57.0	111.0	71.2	5.35	1.39	0.00	25.133	0.000
4	0.70	22.0	56.8	110.0	71.2	5.95	0.77	0.00	50.265	0.000
5	0.70	22.0	56.0	110.6	71.2	6.40	0.29	0.00	100.531	0.000
6	0.70	22.1	56.4	110.6	71.2	6.60	0.15	0.00	150.796	0.000
7	0.70	22.1	56.0	110.6	71.4	6.70	0.01	0.00	0.000	0.000

# SECONDARY BOX

N	Wt	Pt	Tt	Pz/Tz	WtT.44	MP	WS	UP	UM	UOPT	UPT	MACH
RUN							LBH/SEC	LBH/SEC	FT/SEC	FT/SEC		
1	0.0000	0.3760	0.9313	0.4030	0.0000	3.7627	0.0000	101.66	72.67	72.67	0.062	
2	0.1586	0.2632	0.9306	0.2020	0.1537	3.7435	0.5937	180.42	92.77	72.17	0.062	
3	0.2680	0.1803	0.9303	0.2024	0.2596	3.7697	1.0104	181.51	90.65	72.61	0.062	
4	0.4007	0.1056	0.9306	0.1135	0.3802	3.7534	1.5041	180.39	99.02	72.16	0.062	
5	0.4915	0.0390	0.9309	0.0420	0.4762	3.7564	1.8461	180.25	105.07	72.11	0.062	
6	0.5292	0.0205	0.9309	0.0221	0.5120	3.7634	1.9915	180.53	107.70	72.22	0.062	
7	0.0000	0.0014	0.9313	0.0015	0.0000	3.7620	2.6763	100.40	0.0000	72.17	0.062	

TABLE 35 - PCD DATA FOR 22.5/10 NOZZLES WITH L/D=1.5 STACK

TERTIARY BOX

N	WT#	PT#	TT#	PT#-TT#	WT#TT#	.44	NH	WT	UE
RUN									
1	0.0000	0.0000	0.9313	0.0000	0.0000		3.763	0.0000	0.0000
2	0.0000	0.0000	0.9306	0.0000	0.0000		4.337	0.0000	0.0000
3	0.0000	0.0000	0.9303	0.0000	0.0000		4.780	0.0000	0.0000
4	0.0000	0.0000	0.9306	0.0000	0.0000		5.258	0.0000	0.0000
5	0.0000	0.0000	0.9309	0.0000	0.0000		5.602	0.0000	0.0000
6	0.0000	0.0000	0.9309	0.0000	0.0000		5.755	0.0000	0.0000
7	0.0000	0.0000	0.9313	0.0000	0.0000		0.0000	0.0000	0.0000

LBN/SEC LBN/SEC FT/SEC

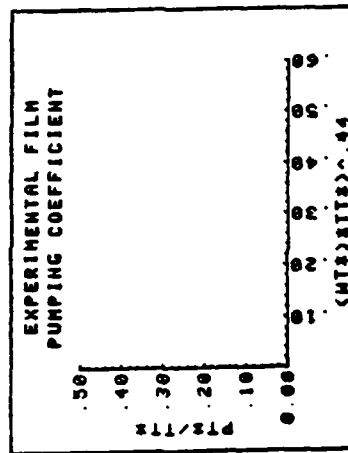
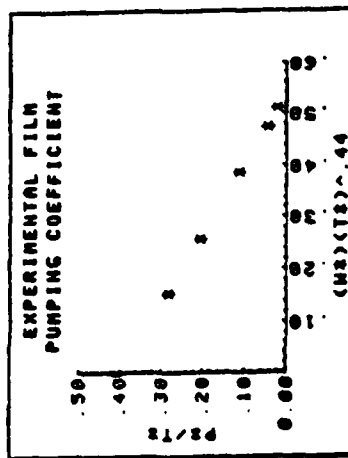


TABLE 35.1 - PCD DATA (CONT) FOR 22.5/10 NOZZLES WITH L/D=1.5



DATA TAKEN ON: 24 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

NOZZLE AM/AR AREA RATIO: 2.50  
 COMMENTS: 22.5 TILT/20 ROTATION/PCD

MIXING STACK INFORMATION:  
 LENGTH: 17.55 CINS  
 DIAMETER: 11.70 CINS  
 L/D RATIO: 1.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 22.5 COEGJ  
 ROTATION ANGLE: 20 IDEGJ  
 AREA PER NOZZLE: 10.792 CINSJ  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.982 CINS  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINSJ  
 ATM. PRESSURE: 30.03 CINHJ

SECONDARY BOX

N	Ms	P2	Ys	P2/12	WST	44	NP	WS	UP	UM	UUPY	UPT	MACH
LBM/SEC LBM/SEC FT/SEC FT/SEC													
SUM													
1	0.0000	0.3910	0.9306	0.4223	0.0000	0.0000	3.7690	0.3000	102.10	72.84	72.85	0.062	
2	0.1639	0.2808	0.9302	0.3018	0.1508	0.1508	3.7612	0.6166	101.34	83.55	72.54	0.062	
3	0.2760	0.1995	0.9302	0.2145	0.2674	0.2674	3.7527	1.0358	100.66	90.76	72.27	0.062	
4	0.4102	0.1106	0.9306	0.1189	0.3974	0.3974	3.7605	1.5426	100.75	99.05	72.31	0.062	
5	0.4919	0.0399	0.9306	0.0429	0.4766	0.4766	3.7527	1.8461	100.14	105.03	72.06	0.062	
6	0.5494	0.0221	0.9306	0.0230	0.5323	0.5323	3.7435	2.0569	179.64	108.59	71.06	0.061	
7	0.88888	0.0014	0.9306	0.0015	0.88888	0.88888	3.7697	2.6760	100.03	0.0000	72.34	0.062	

TABLE 36 - PCD DATA FOR 22.5/20 NOZZLES WITH L/D=1.5 STACK

# TERTIARY BOX

N	MTS	PTS	TTs	PIs/TTs	MTTT	.44	MM	MT	UE
LBM/SEC LBM/SEC FT/SEC									
RUN									
1	333333	0.0000	0.9306	0.0000	333333	3.769	333333	333333	333333
2	333333	0.0000	0.9302	0.0000	333333	4.370	333333	333333	333333
3	333333	0.0000	0.9300	0.0000	333333	4.700	333333	333333	333333
4	333333	0.0000	0.9306	0.0000	333333	5.303	333333	333333	333333
5	333333	0.0000	0.9306	0.0000	333333	5.599	333333	333333	333333
6	333333	0.0000	0.9306	0.0000	333333	5.000	333333	333333	333333
7	333333	0.0000	0.9306	0.0000	333333	333333	333333	333333	333333

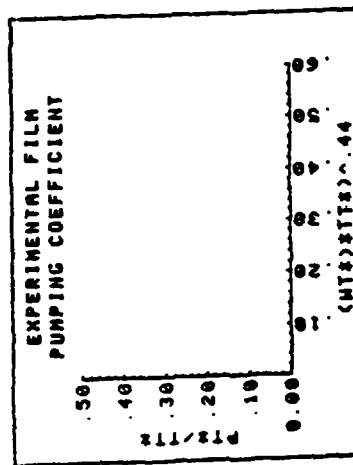
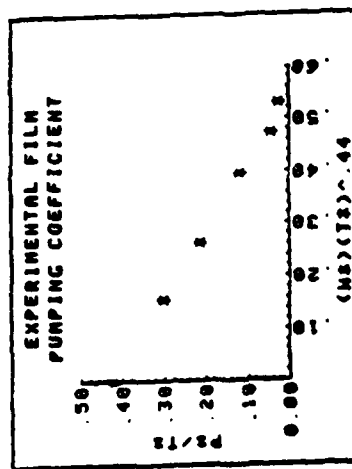


TABLE 36.1 - PCD DATA (CONT) FOR 22.5/20 NOZZLES WITH L/D=1.5 STACK

DATA TAKEN ON: 23 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 14.63 CINH  
 DIAMETER: 11.70 CINH  
 L/D RATIO: 1.25  
 S/D RATIO: 0.50

NOZZLE AN/AP AREA RATIO: 2.50  
 NOZZLE AN/AP AREA RATIO: 2.50  
 STRAIGHT NOZZLE CAL RUH

COMMENTS:  
 MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINH2  
 ATM. PRESSURE: 30.03 CINH2

N	POR	OPOR	TOR	TUPT	TAMB	PUP	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F					IN OF H2O		SQUARE INCHES	SQUARE INCHES
1	0.70	22.0	57.2	110.4	66.4	3.35	3.17	0.00	0.000	0.000
2	0.70	22.1	57.0	110.6	66.6	4.40	2.04	0.00	12.565	0.000
3	0.70	22.0	58.0	110.6	66.0	5.00	1.37	0.00	25.133	0.000
4	0.70	22.1	57.0	110.8	66.0	5.62	0.73	0.00	50.265	0.000
5	0.70	22.0	57.2	110.0	67.2	6.05	0.26	0.00	100.531	0.000
6	0.70	22.1	57.0	111.0	67.4	6.20	0.13	0.00	150.796	0.000
7	0.70	22.1	57.0	111.0	68.2	6.32	0.01	0.00	0.000	0.000

SECONDARY BOX

N	WS	PS	IS	P2/T2	WST	44	WP	WS	UP	UN	UUP	UPT	MACH
RUN								LBH/SEC	LBH/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC
1	0.0000	0.4267	0.9220	0.4623	0.0000	3.7520	0.300	101.26	72.51	72.51	0.062	0.062	0.062
2	0.1636	0.2751	0.9220	0.2901	0.1579	3.7503	0.6147	161.12	83.34	72.46	0.062	0.062	0.062
3	0.2607	0.1063	0.9232	0.2010	0.2594	3.7491	1.0073	180.30	90.00	72.16	0.062	0.062	0.062
4	0.3913	0.0990	0.9229	0.1073	0.3777	3.7503	1.4706	180.61	90.29	72.25	0.062	0.062	0.062
5	0.4676	0.0355	0.9236	0.0304	0.4516	3.7520	1.7546	180.09	103.14	72.04	0.062	0.062	0.062
6	0.4951	0.0177	0.9236	0.0192	0.4701	3.7503	1.8607	180.40	103.15	72.17	0.062	0.062	0.062
7	0.0000	0.0014	0.9250	0.0015	0.0000	3.7503	2.6844	180.35	0.0000	72.15	0.062	0.062	0.062

TABLE 37 - PCD DATA FOR STRAIGHT NOZZLES WITH L/D=1.25 STACK

TERTIARY BOX

W	WT#	PT#	TT#	FT#/TT#	WT#TT#-44	NH	HT	UE
RUN						LBN/SEC	LBN/SEC	FT/SEC
1	00000	0	0000	0	9228	0	0000	0000
2	00000	0	0000	0	9228	0	0000	0000
3	00000	0	0000	0	9232	0	0000	0000
4	00000	0	0000	0	9229	0	0000	0000
5	00000	0	0000	0	9236	0	0000	0000
6	00000	0	0000	0	9236	0	0000	0000
7	00000	0	0000	0	9230	0	0000	0000

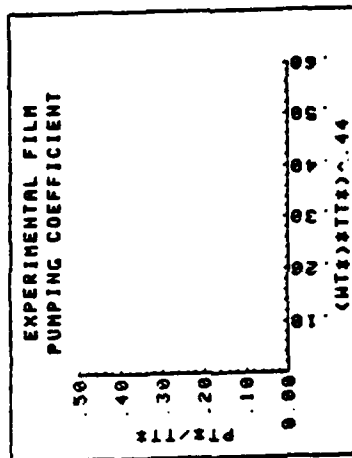
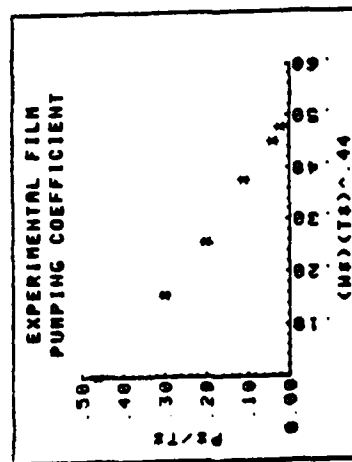


TABLE 37.1 - PCD DATA (CONT) FOR STRAIGHT NOZZLES WITH L/D=1.25 STACK

# MIXING STACK DATA FOR RUN 7

TOP (POSITION 'A') DATA				DIAGONAL (POSITION 'B') DATA			
X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PHS#	X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PHS#
0.00	-1.570	45	-0.214	0.00	-1.145	45	-0.156
0.25	-0.025	45	-0.113	0.25	-0.805	45	-0.110
0.50	-0.570	45	-0.078	0.50	-0.560	45	-0.076
0.75	-0.475	45	-0.065	0.75	-0.465	45	-0.063
1.00	-0.285	45	-0.039	1.00	-0.300	45	-0.041
1.25	-0.105	45	-0.014	1.25	-0.115	45	-0.016

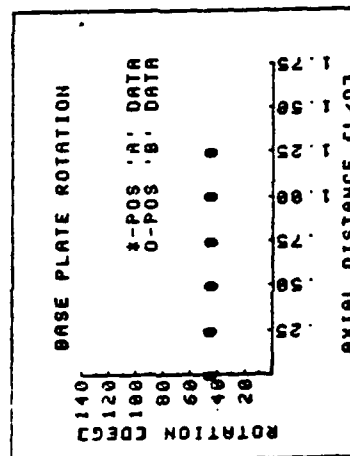
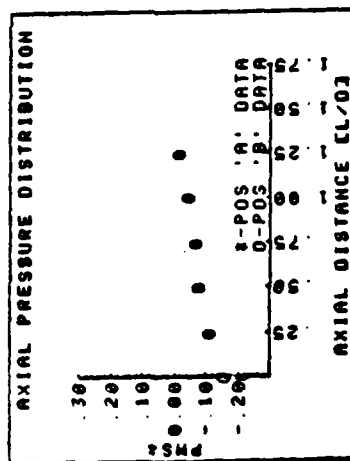
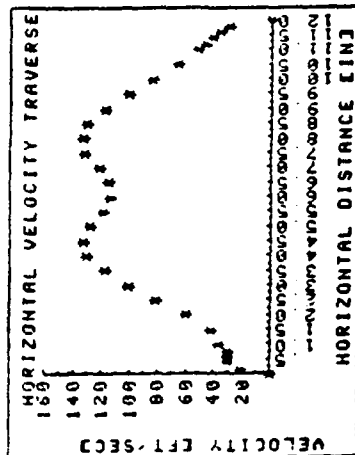


TABLE 37.2 - MSD DATA FOR STRAIGHT NOZZLES WITH L/D=1.25 STACK

HORIZONTAL VELOCITY TRAVERSE AT BASE ROTATION OF 00 DEGREES

POSITION	0 00	0 20	0 40	0 60	0 80	1 00	1 50
PEIN H203	0 00	0 10	0 20	0 20	0 20	0 30	0 40
VEFT/SEC3	0 00	21 06	29 79	29 79	29 79	36 49	42 13
POSITION	2 00	2 50	3 00	3 50	4 00	4 50	5 00
PEIN H203	0 00	1 50	2 30	3 10	3 80	4 00	3 70
VEFT/SEC3	59 58	81 58	101 02	117 28	129 95	133 22	128 13
POSITION	5 50	6 00	6 50	7 00	7 50	8 00	8 50
PEIN H203	3 20	2 90	3 00	3 30	3 90	4 00	3 80
VEFT/SEC3	119 16	113 44	115 38	121 01	131 55	133 22	129 85
POSITION	9 00	9 50	10 00	10 50	11 00	11 20	11 40
PEIN H203	3 10	2 30	1 60	1 00	0 60	0 50	0 40
VEFT/SEC3	117 28	101 02	84 26	66 61	51 60	47 10	42 13
POSITION	11 60	11 80	12 00				
PEIN H203	0 30	0 20	0 00				



DIAGONAL VELOCITY TRAVERSE FOR BASE ROTATION OF 00 DEGREES

POSITION	0 00	0 20	0 40	0 60	0 80	1 00	1 50
PEIN H203	0 00	0 30	0 65	0 80	1 00	1 20	2 10
VEFT/SEC3	0 00	36 49	53 70	59 58	66 61	72 57	96 53
POSITION	2 00	2 50	3 00	3 50	4 00	4 50	5 00
PEIN H203	3 60	5 40	6 70	6 70	5 70	4 60	3 70
VEFT/SEC3	126 39	154 79	172 42	172 42	159 03	142 87	128 13
POSITION	5 50	6 00	6 50	7 00	7 50	8 00	8 50
PEIN H203	3 20	2 80	2 90	3 20	3 80	4 70	5 80
VEFT/SEC3	119 16	111 46	113 44	119 16	129 85	144 41	160 42
POSITION	9 00	9 50	10 00	10 50	11 00	11 20	11 40
PEIN H203	6 60	6 90	6 20	4 80	3 20	2 60	2 20
VEFT/SEC3	171 13	174 98	165 86	145 94	119 16	107 41	98 88
POSITION	11 60	11 80	12 00				
PEIN H203	1 90	1 60	0 00				

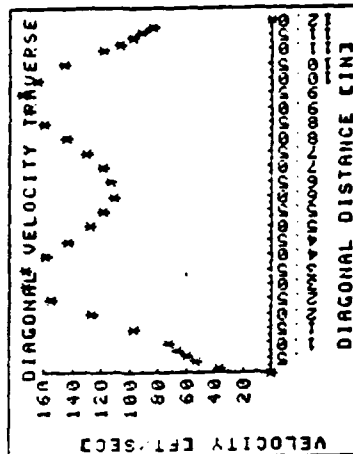


TABLE 37.3 - VTD DATA FOR STRAIGHT NOZZLES WITH L/D=1.25 STACK

DATA TAKEN ON: 26 AUG 81  
 DATA TAKEN BY: DRUCKER/DAVIS

NOZZLE AM/AP AREA RATIO: 2.50  
 10 TILT/10 ROTATION/PCD

MIXING STACK INFORMATION:  
 LENGTH: 14.63 [IN]  
 DIAMETER: 11.70 [IN]  
 L/D RATIO: 1.25  
 S/D RATIO: 0.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 10.0 [DEG]  
 ROTATION ANGLE: 10 [DEG]  
 AREA PER NOZZLE: 10.752 [IN2]  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 [IN]  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 [IN2]  
 ATM. PRESSURE: 29.90 [INHG]

COMMENTS:

N	POR	IN OF H2O	DPOR	TOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA SQUARE INCHES	TERTIARY AREA SQUARE INCHES
RUN					DEGREES F			IN OF H2O			
1	0.71	22.0	59.2	113.0	71.0	3.20	3.15	0.00	0.00	2.000	xxxxxx
2	0.71	22.2	59.2	112.0	71.0	4.20	2.19	0.00	0.00	12.566	xxxxxx
3	0.71	22.0	59.2	112.0	71.0	4.00	1.53	0.00	0.00	25.133	xxxxxx
4	0.71	22.0	59.2	112.6	71.0	5.50	0.83	0.00	0.00	50.265	xxxxxx
5	0.71	22.0	59.2	112.6	72.0	6.00	0.30	0.00	0.00	100.531	xxxxxx
6	0.71	22.0	59.4	112.0	72.0	6.10	0.15	0.00	0.00	150.796	xxxxxx
7	0.71	22.0	59.2	112.0	72.2	6.20	0.01	0.00	0.00	xxxxxx	xxxxxx

SECONDARY BOX

N	MS	P#	T#	P#T#	MSA.44	WP	MS	UP	UM	UUPT	UPT MACH
RUN							LBM/SEC	LBM/SEC	FT/SEC	FT/SEC	
1	0.0000	0.4261	0.9201	0.4592	0.0000	3.7416	0.0000	181.80	72.76	72.76	0.062
2	0.1685	0.2952	0.9284	0.3180	0.1631	3.7586	0.6332	182.21	84.23	72.89	0.062
3	0.2829	0.2008	0.9284	0.2249	0.2738	3.7416	1.0586	181.09	91.40	72.44	0.062
4	0.4160	0.1137	0.9287	0.1225	0.4034	3.7416	1.5594	180.72	100.21	72.29	0.062
5	0.5014	0.0412	0.9291	0.0444	0.4651	3.7416	1.8747	180.48	105.70	72.20	0.062
6	0.5315	0.0206	0.9207	0.0222	0.5145	3.7409	1.9884	180.44	107.00	72.10	0.062
7	0.5388	0.0014	0.9291	0.0015	0.5388	3.7416	2.6721	180.41	xxxxxx	72.17	0.062

TABLE 38 - PCD DATA FOR 10/10 NOZZLES WITH L/D-1.25 STACK

TERTIARY BOX

N	MTS	PTS	TTs	PTs/TTs	MTsTTs	UM	WT	UE
LBM/SEC LBM/SEC FT/SEC								
RUN								
1	0.0000	0.0000	0.9291	0.0000	0.0000	3.742	0.0000	0.0000
2	0.0000	0.0000	0.9284	0.0000	0.0000	4.392	0.0000	0.0000
3	0.0000	0.0000	0.9284	0.0000	0.0000	4.800	0.0000	0.0000
4	0.0000	0.0000	0.9287	0.0000	0.0000	5.301	0.0000	0.0000
5	0.0000	0.0000	0.9291	0.0000	0.0000	5.616	0.0000	0.0000
6	0.0000	0.0000	0.9287	0.0000	0.0000	5.729	0.0000	0.0000
7	0.0000	0.0000	0.9291	0.0000	0.0000	0.0000	0.0000	0.0000

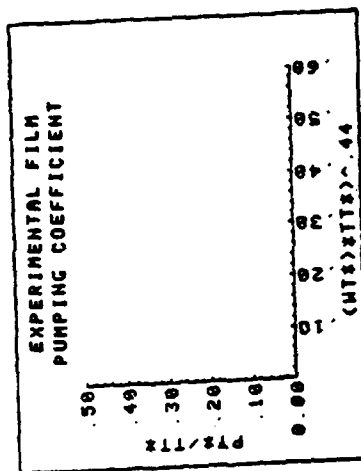
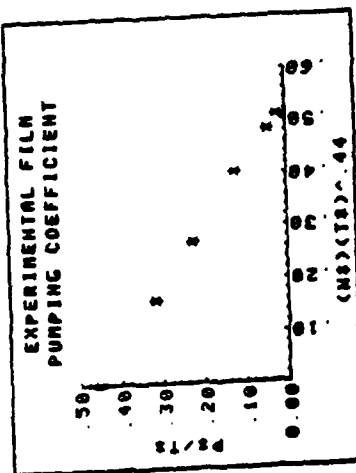


TABLE 38.1 -- PCD DATA (CONT) FOR 10/10 NOZZLES WITH L/D=1.25 STACK



DATA TAKEN ON: 26 AUG 81  
 DATA TAKEN BY: DRUCKER/DAVIS

NOZZLE AM/AP AREA RATIO: 2.50  
 COMMENTS: 10 TILT/20 ROTATION/PCD

MIXING STACK INFORMATION:  
 LENGTH: 14.63 CINS  
 DIAMETER: 11.70 CINS  
 L/D RATIO: 1.25  
 S/D RATIO: 0.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 10.0 CDEG  
 ROTATION ANGLE: 20 CDEG  
 AREA PER NOZZLE: 10.752 CINS<sup>2</sup>  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINS  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINS<sup>2</sup>  
 ATM. PRESSURE: 29.99 CINHGS

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SECONDARY BOX

N	WS	PS	TS	PT/TS	WAT/44	WP	WS	UP	UM	UPT	UPT MACH
RUN							LBM/SEC	LBM/SEC	FT/SEC	FT/SEC	
1	0.0000	0.4135	0.9291	0.4450	0.0000	3.7599	0.0000	102.61	73.05	73.05	0.062
2	0.1628	0.2764	0.9291	0.2975	0.1577	3.7430	0.6095	181.32	83.45	72.53	0.062
3	0.2710	0.1932	0.9294	0.2079	0.2632	3.7514	1.0196	181.39	90.83	72.56	0.062
4	0.3933	0.1015	0.9294	0.1092	0.3808	3.7429	1.4721	180.68	98.65	72.28	0.062
5	0.4653	0.0356	0.9291	0.0383	0.4505	3.7507	1.7452	180.90	103.63	72.37	0.062
6	0.3626	0.0096	0.9290	0.0104	0.3512	3.7451	1.3500	180.49	96.54	72.20	0.062
7	0.0000	0.0014	0.9290	0.0019	0.0000	3.7422	2.6720	180.32	0.0000	72.14	0.062

TABLE 39 - PCD DATA FOR 10/20 NOZZLES WITH L/D=1.25 STACK

TERTIARY BOX

N	WT	PT	TT	PTL/TT	NTTT	44	NM	NT	UE
LBM/SEC LBM/SEC FT/SEC									
RUN									
1	111111	0.0000	0.9291	0.0000	111111	3.760	111111	111111	111111
2	111111	0.0000	0.9291	0.0000	111111	4.352	111111	111111	111111
3	111111	0.0000	0.9294	0.0000	111111	4.771	111111	111111	111111
4	111111	0.0000	0.9294	0.0000	111111	5.215	111111	111111	111111
5	111111	0.0000	0.9291	0.0000	111111	5.496	111111	111111	111111
6	111111	0.0000	0.9298	0.0000	111111	5.103	111111	111111	111111
7	111111	0.0000	0.9290	0.0000	111111	111111	111111	111111	111111

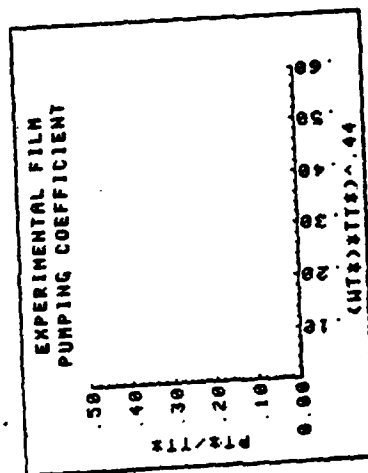
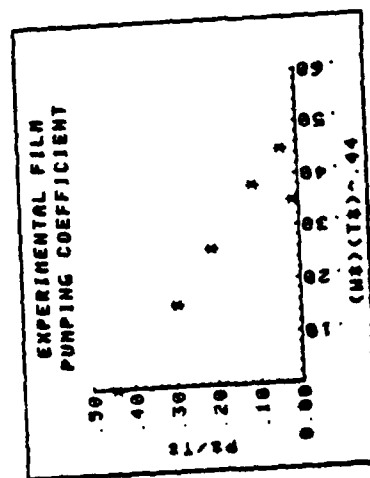


TABLE 39.1 - PCD DATA (CONT) FOR 10/20 NOZZLES WITH L/D=1.25 STACK

DATA TAKEN ON: 26 AUG 81  
 DATA TAKEN BY: DRUCKER/DAVIS  
 NOZZLE AM/AP AREA RATIO: 2.50  
 10 TILT/30 ROTATION/PCD  
 COMMENTS:  
 MIXING STACK INFORMATION:  
 LENGTH: 14.63 CINS  
 DIAMETER: 11.70 CINS  
 L/D RATIO: 1.25  
 S/D RATIO: 0.50  
 PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 10.0 COEG3  
 ROTATION ANGLE: 30 COEG3  
 AREA PER NOZZLE: 10.752 CINS2  
 NUMBER OF NOZZLES: 4  
 MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.982 CINS  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINS2  
 ATM. PRESSURE: 29.99 CINHG3

N	POR	DPOR	TOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA SQUARE INCHES	TERTIARY AREA SQUARE INCHES
RUN	IN CF H2O	DEGREES F					IN OF H2O			
1	0.71	22.0	59.0	112.6	72.4	3.40	2.95	0.00	0.000	*****
2	0.71	22.0	59.0	112.6	72.4	4.45	1.07	0.00	12.566	*****
3	0.71	22.0	59.0	112.6	72.2	5.10	1.27	0.00	25.133	*****
4	0.71	22.0	59.0	112.6	72.4	5.60	0.65	0.00	50.265	*****
5	0.70	22.0	59.0	112.6	72.4	6.00	0.23	0.00	100.531	*****
6	0.70	22.0	59.0	112.6	72.4	6.10	0.11	0.00	150.796	*****
7	0.70	21.9	59.6	112.6	72.4	6.20	0.01	0.00	*****	*****

# SECONDARY BOX

N	W6	PS	TS	PS/TS WGT-44	WP	WS	UP	UM	UPT	UPT MACH
RUN						LBM/SEC	LBM/SEC	FT/SEC	FT/SEC	
1	0.0000	0.4003	0.9290	0.4306	0.0000	3.7430	0.0000	101.67	72.67	72.67 0.062
2	0.1563	0.2551	0.9290	0.2744	0.1513	3.7430	0.5849	101.10	82.96	72.40 0.062
3	0.2576	0.1737	0.9294	0.1869	0.2495	3.7430	0.9643	100.92	89.65	72.37 0.062
4	0.3685	0.0892	0.9290	0.0960	0.3569	3.7430	1.3794	100.64	96.90	72.26 0.062
5	0.4385	0.0316	0.9294	0.0340	0.4246	3.7430	1.6411	100.52	101.62	72.21 0.062
6	0.4547	0.0151	0.9290	0.0163	0.4404	3.7437	1.7024	100.44	102.69	72.10 0.062
7	0.8888	0.0014	0.9290	0.0015	0.8888	3.7359	2.6720	100.02	*****	72.01 0.061

TABLE 40 - PCD DATA FOR 10/30 NOZZLES WITH L/D=1.25 STACK

TERTIARY BOX

N	MTS	PTS	TTX	PTS/TTX	MTT <sup>2</sup> ~.44	NR	MT	UE
RUN						LBM/SEC	LBM/SEC	FT/SEC
1	0.0000	0.0000	0.9298	0.0000	0.0000	3.743	0.0000	0.0000
2	0.0000	0.0000	0.9298	0.0000	0.0000	4.320	0.0000	0.0000
3	0.0000	0.0000	0.9294	0.0000	0.0000	4.707	0.0000	0.0000
4	0.0000	0.0000	0.9298	0.0000	0.0000	5.122	0.0000	0.0000
5	0.0000	0.0000	0.9294	0.0000	0.0000	5.384	0.0000	0.0000
6	0.0000	0.0000	0.9298	0.0000	0.0000	5.446	0.0000	0.0000
7	0.0000	0.0000	0.9298	0.0000	0.0000	0.0000	0.0000	0.0000

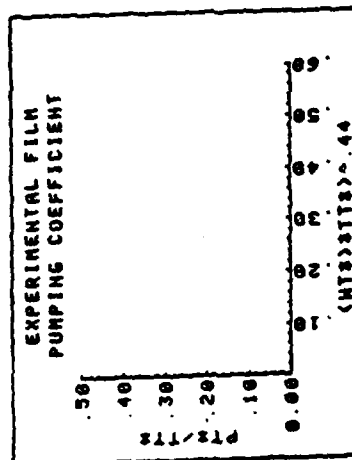
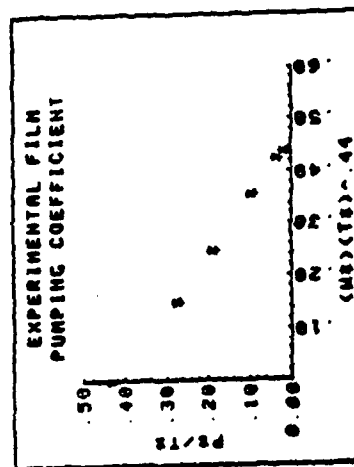


TABLE 40.1 - PCD DATA (CONT) FOR 10/30 NOZZLES WITH L/D=1.25 STACK

DATA TAKEN ON: 26 AUG 81  
 DATA TAKEN BY: DRUCKER-DAVIS  
 NOZZLE AM/AP AREA RATIO: 2.50  
 10 TILT/40 ROTATION/PCD

MIXING STACK INFORMATION:  
 LENGTH: 14.63 CINH  
 DIAMETER: 11.70 CINH  
 L/D RATIO: 1.25  
 S/D RATIO: 0.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 10.0 CDEG  
 ROTATION ANGLE: 40 CDEG  
 AREA PER NOZZLE: 10.752 CINH2  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINH2  
 ATM. PRESSURE: 29.99 CINHG

N	POR	DPOR	TOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES	F	IN OF H2O	IN OF H2O	IN OF H2O	IN OF H2O	IN OF H2O	SQUARE INCHES	SQUARE INCHES
1	0.71	22.2	50.6	112.4	72.4	3.70	2.00	0.00	0.000	0.000
2	0.71	22.0	50.6	112.4	72.4	4.65	1.60	0.00	12.566	0.000
3	0.71	22.0	50.0	112.4	72.4	5.20	1.11	0.00	25.133	0.000
4	0.71	22.0	50.6	112.4	72.4	5.00	0.56	0.00	50.265	0.000
5	0.71	22.0	50.4	112.4	72.4	6.15	0.19	0.00	100.531	0.000
6	0.71	22.0	50.4	112.4	72.6	6.25	0.10	0.00	150.796	0.000
7	0.71	22.0	50.2	112.2	72.6	6.30	0.01	0.00	0.000	0.000

# SECONDARY BOX

N	Wt	Pt	Tt	Pt/Tt	HST	44	WP	WS	UP	UN	UPT	UPT	MACH
RUN													
1	0.0000	0.3768	0.9301	0.4051	0.0000	0.0000	3.7614	0.0000	102.43	72.90	72.90	0.062	
2	0.1481	0.2294	0.9301	0.2466	0.1434	0.1434	3.7444	0.5544	181.10	62.30	72.45	0.062	
3	0.2408	0.1520	0.9301	0.1635	0.2332	0.2332	3.7437	0.9013	180.82	80.48	72.33	0.062	
4	0.3419	0.0769	0.9301	0.0827	0.3312	0.3312	3.7444	1.2804	180.61	95.19	72.25	0.062	
5	0.3983	0.0261	0.9301	0.0281	0.3050	0.3050	3.7451	1.4916	180.48	98.93	72.20	0.062	
6	0.4333	0.0130	0.9304	0.0140	0.4190	0.4190	3.7451	1.6229	180.44	101.27	72.10	0.062	
7	0.0000	0.0014	0.9300	0.0015	0.0000	0.0000	3.7450	2.6715	180.37	0.0000	72.15	0.062	

TABLE 41 - PCD DATA FOR 10/40 NOZZLES WITH L/D=1.25 STACK

TERTIARY BOX

N	WTS	PTS	ITS	PIR/ITS	WTS/ITS	WM	WT	UE
RUN						LBM/SEC	LBM/SEC	FT/SEC
1	0.0000	0.0000	0.9301	0.0000	0.0000	3.761	0.0000	0.0000
2	0.0000	0.0000	0.9301	0.0000	0.0000	4.299	0.0000	0.0000
3	0.0000	0.0000	0.9301	0.0000	0.0000	4.645	0.0000	0.0000
4	0.0000	0.0000	0.9301	0.0000	0.0000	5.025	0.0000	0.0000
5	0.0000	0.0000	0.9301	0.0000	0.0000	5.237	0.0000	0.0000
6	0.0000	0.0000	0.9301	0.0000	0.0000	5.369	0.0000	0.0000
7	0.0000	0.0000	0.9300	0.0000	0.0000	0.0000	0.0000	0.0000

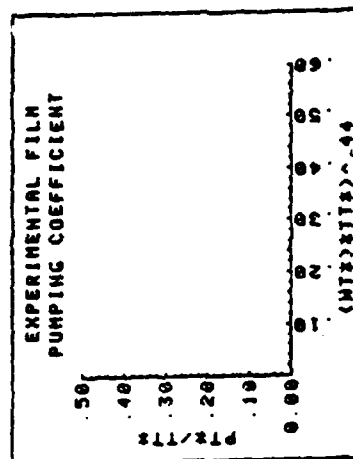
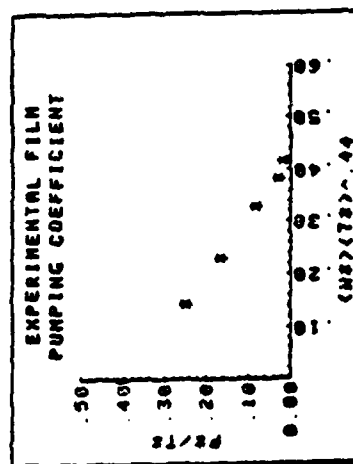


TABLE 41.1 - PCD DATA (CONT) FOR 10/40 NOZZLES WITH L/D-1.25 STACK

DATA TAKEN ON: 26 AUG 81  
 DATA TAKEN BY: DRUCKER/DAVIS

NOZZLE AH/AP AREA RATIO: 2.50

COMMENTS:  
 15 TILT/10 ROTATION/PCD

MIXING STACK INFORMATION:  
 LENGTH: 14.63 CINH  
 DIAMETER: 11.70 CINH  
 L/D RATIO: 1.25  
 S/D RATIO: 0.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 15.0 COEGJ  
 ROTATION ANGLE: 10 COEGJ  
 AREA PER NOZZLE: 10.752 CINH  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINH  
 ATM. PRESSURE: 29.99 CINH

N	FOR	OPOR	TOR	TUPT	TAMB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.71	22.2	50.2	112.2	72.4	3.45	3.10	0.00	0.000	xxxxxx
2	0.71	22.1	50.2	112.0	72.4	4.20	2.20	0.00	12.566	xxxxxx
3	0.70	22.0	50.6	112.0	72.4	4.00	1.56	0.00	25.133	xxxxxx
4	0.71	22.2	57.6	112.0	72.4	5.45	0.00	0.00	50.265	xxxxxx
5	0.71	22.1	50.4	112.2	72.4	5.95	0.33	0.00	100.531	xxxxxx
6	0.70	22.0	50.2	112.0	72.4	6.10	0.17	0.00	150.796	xxxxxx
7	0.70	22.0	50.0	112.0	72.4	6.25	0.01	0.00	xxxxxx	xxxxxx

# SECONDARY BOX

N	M2	P2	T2	P2/T2	MST	44	WP	WS	UP	UM	UPT	UPT	MACH
RUN								LBM/SEC	LBM/SEC	FT/SEC	FT/SEC		
1	0.0000	0.4165	0.9304	0.4477	0.0000	3.7620	0.0000	102.57	73.03	73.04	0.062		
2	0.1620	0.2935	0.9307	0.3207	0.1637	3.7543	0.6344	101.69	84.05	72.60	0.062		
3	0.2854	0.2134	0.9307	0.2293	0.2765	3.7444	1.0685	100.93	91.52	72.38	0.062		
4	0.4263	0.1195	0.9307	0.1204	0.4130	3.7650	1.6050	101.62	101.41	72.65	0.062		
5	0.5237	0.0452	0.9304	0.0405	0.5073	3.7536	1.9650	100.09	107.59	72.36	0.062		
6	0.5650	0.0234	0.9307	0.0231	0.5474	3.7459	2.1164	100.30	110.08	72.16	0.062		
7	0.5888	0.0014	0.9307	0.0015	0.5888	3.7466	2.6720	100.34	xxxxxx	72.14	0.062		

TABLE 42 - PCD DATA FOR 15/10 NOZZLES WITH L/D=1.25 STACK

TERTIARY BOX

N	WTG	PTS	YTS	P12/118	WTST/1.44	HM	HT	UE
LBM/SEC LBM/SEC FT/SEC								
1	0.0000	0.0000	0.9304	0.0000	0.0000	3.763	0.0000	0.0000
2	0.0000	0.0000	0.9307	0.0000	0.0000	4.399	0.0000	0.0000
3	0.0000	0.0000	0.9307	0.0000	0.0000	4.813	0.0000	0.0000
4	0.0000	0.0000	0.9307	0.0000	0.0000	5.370	0.0000	0.0000
5	0.0000	0.0000	0.9304	0.0000	0.0000	5.719	0.0000	0.0000
6	0.0000	0.0000	0.9307	0.0000	0.0000	5.862	0.0000	0.0000
7	0.0000	0.0000	0.9307	0.0000	0.0000	0.0000	0.0000	0.0000

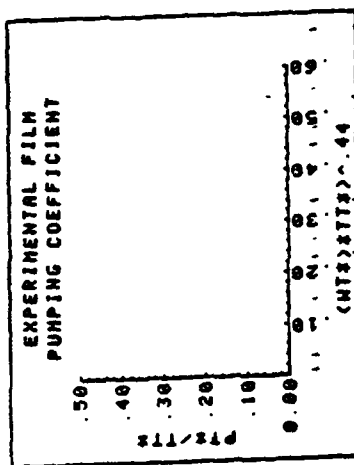
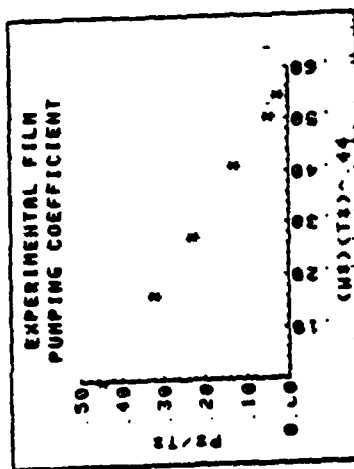


TABLE 42.1 - PCD DATA (CONT) FOR 15/10 NOZZLES WITH L/D=1.25 STACK



DATA TAKEN ON: 26 AUG 61  
 DATA TAKEN BY: DRUCKER/DAVIS  
 NOZZLE AN/AP AREA RATIO: 2.50  
 15 TILT/20 ROTATION/PCD  
 COMMENTS:  
 15 TILT/20 ROTATION/PCD  
 MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINJ  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINJ23  
 ATM. PRESSURE: 29.99 CINJG3

MIXING STACK INFORMATION:  
 LENGTH: 14.63 CINJ  
 DIAMETER: 11.70 CINJ  
 L/D RATIO: 1.25  
 S/D RATIO: 0.50  
 PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 15.0 EDEG3  
 ROTATION ANGLE: 20 EDEG3  
 AREA PER NOZZLE: 10.752 CINJ23  
 NUMBER OF NOZZLES: 4

N	POR	DPOR	TOR	TUPT	TANS	TUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.71	22.2	50.0	112.0	72.4	3.25	3.13	0.00	0.000	*****
2	0.70	22.0	50.0	112.0	72.4	4.15	2.20	0.00	12.566	*****
3	0.71	22.1	57.6	112.0	72.2	4.00	1.57	0.00	25.133	*****
4	0.70	22.0	50.0	112.0	72.4	5.45	0.85	0.00	50.265	*****
5	0.71	22.2	50.2	112.0	72.4	6.00	0.31	0.00	100.531	*****
6	0.70	22.1	50.2	112.0	72.4	6.15	0.16	0.00	150.796	*****
7	0.71	22.0	50.0	112.0	72.4	6.25	0.01	0.00	*****	*****

SECONDARY BOX

N	WS	PS	TS	PS/TS	WST-44	HP	WS	UP	UM	UPT	UPT MACH
RUN							LBM/SEC	LBM/SEC	FT/SEC	FT/SEC	
1	0.0000	0.4206	0.9307	0.4519	0.0000	3.7636	0.0000	182.56	73.03	73.03	0.062
2	0.1693	0.2997	0.9307	0.3220	0.1641	3.7466	0.6344	181.32	83.90	72.53	0.062
3	0.2854	0.2133	0.9304	0.2293	0.2765	3.7565	1.0721	181.51	91.02	72.61	0.062
4	0.4210	0.1166	0.9307	0.1252	0.4079	3.7466	1.5774	180.71	100.56	72.29	0.062
5	0.5063	0.0423	0.9307	0.0454	0.4906	3.7620	1.9053	181.26	106.65	72.51	0.062
6	0.5469	0.0219	0.9307	0.0236	0.5299	3.7544	2.0532	180.70	109.11	72.32	0.062
7	0.0000	0.0014	0.9307	0.0015	0.0000	3.7466	2.6720	180.34	113.88	72.14	0.062

TABLE 43 - PCD DATA FOR 15/20 NOZZLES WITH L/D=1.25 STACK

TERTIARY BOX

N	WT	PT	TT	PTT	WT	UE
1	0.0000	0.0000	0.9387	0.0000	3.764	0.0000
2	0.0000	0.0000	0.9387	0.0000	4.381	0.0000
3	0.0000	0.0000	0.9387	0.0000	4.829	0.0000
4	0.0000	0.0000	0.9387	0.0000	5.324	0.0000
5	0.0000	0.0000	0.9387	0.0000	5.568	0.0000
6	0.0000	0.0000	0.9387	0.0000	5.888	0.0000
7	0.0000	0.0000	0.9387	0.0000	6.000	0.0000

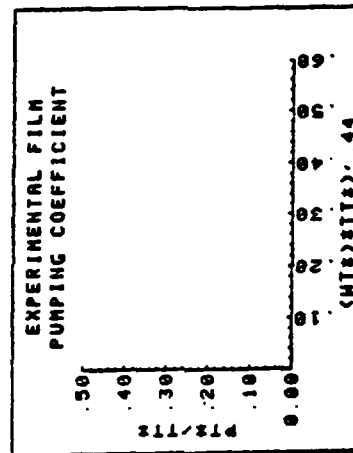
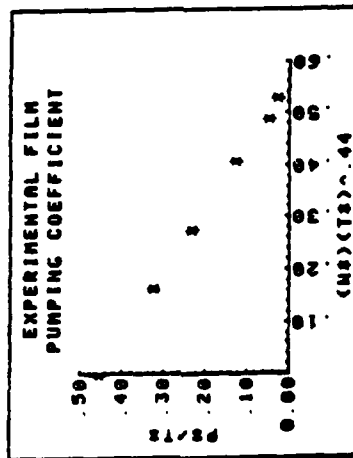


TABLE 43.1 - PCD DATA (CONT) FOR 15/20 NOZZLES WITH L/D=1.25 STACK

DATA TAKEN ON: 27 AUG 81  
 DATA TAKEN BY: DRUCKER/DAVIS

NOZZLE AN/AP AREA RATIO: 2.50

15 TILI/20 ROTATION/FULL RUN

COMMENTS:

MIXING STACK INFORMATION:  
 LENGTH: 14.63 CINI  
 DIAMETER: 11.70 CINI  
 L/D RATIO: 1.25  
 S/D RATIO: 0.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 15.0 CODEG  
 ROTATION ANGLE: 20 CODEG  
 AREA PER NOZZLE: 10.752 CINH2  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINI  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINH2  
 ATM. PRESSURE: 29.03 CINHG3

N	FOR	OPOR	TOR	TUPT	TANB	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.71	22.0	60.0	113.4	72.4	3.25	3.12	0.00	0.000	xxxxxx
2	0.71	22.1	60.6	113.6	72.6	4.20	2.20	0.00	12.566	xxxxxx
3	0.70	22.0	60.2	113.4	72.6	4.75	1.57	0.00	25.133	xxxxxx
4	0.71	22.2	61.0	113.6	72.0	5.50	0.86	0.00	50.265	xxxxxx
5	0.71	22.1	60.0	113.0	72.0	6.00	0.31	0.00	100.531	xxxxxx
6	0.71	22.1	61.4	114.4	73.0	6.15	0.16	0.00	150.796	xxxxxx
7	0.71	22.1	61.0	114.4	73.0	6.30	0.01	0.00	xxxxxx	xxxxxx

# SECONDARY BOX

N	W#	P#	T#	PS/TS	NAT#	44	WP	WS	UP	UN	UUPU	UPT	MACH
RUN							LBN/SEC	LBN/SEC	FT/SEC	FT/SEC	FT/SEC		
1	0.0000	0.4233	0.9285	0.4559	0.0000	0.0000	3.7262	0.0000	102.19	72.00	72.00	0.062	
2	0.1693	0.2903	0.9285	0.3212	0.1639	0.6326	3.7353	0.6326	102.29	84.32	72.92	0.062	
3	0.2067	0.2145	0.9208	0.2309	0.2775	1.0680	3.7203	1.0680	101.60	91.91	72.63	0.062	
4	0.4227	0.1170	0.9208	0.1259	0.4091	1.5817	3.7423	1.5817	102.02	101.34	72.82	0.062	
5	0.5086	0.0424	0.9205	0.0457	0.4922	2.0464	3.7346	2.0464	101.46	106.84	72.59	0.062	
6	0.5483	0.0219	0.9279	0.0236	0.5305	2.0464	3.7325	2.0464	101.48	109.51	72.60	0.062	
7	0.5668	0.0014	0.9279	0.0015	0.5305	2.6632	3.7339	2.6632	101.40	xxxxxx	72.60	0.062	

TABLE 44 - PCD DATA FOR 15/20 NOZZLES WITH L/D=1.25 STACK (FULL RUN)

TERTIARY BOX

N	WT	PI	IT	PI	IT	WT	UE
1	0.0000	0.0000	0.9285	0.0000	0.0000	0.0000	0.0000
2	0.0000	0.0000	0.9285	0.0000	0.0000	0.0000	0.0000
3	0.0000	0.0000	0.9285	0.0000	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.9285	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.9285	0.0000	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.9285	0.0000	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.9279	0.0000	0.0000	0.0000	0.0000

WT	PI	IT	PI	IT	WT	UE
3.726	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4.368	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4.797	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5.324	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5.634	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
5.779	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

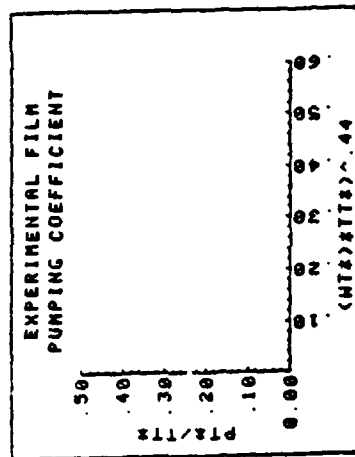
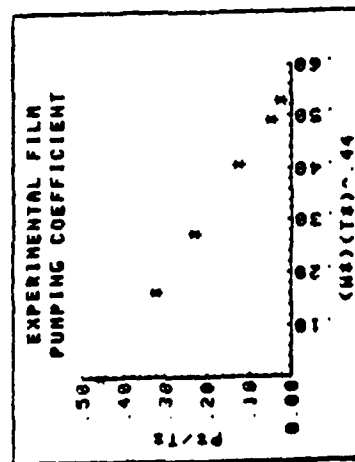


TABLE 44.1 - PCD DATA (CONT) FOR 15/20 NOZZLES WITH L/D=1.25 STACK

# MIXING STACK DATA FOR RUN 7

TOP (POSITION 'A') DATA				DIAGONAL (POSITION 'B') DATA			
X/D	PRESSURE EIN M203	ROTATION EDEC3	PMS*	X/D	PRESSURE EIN M203	ROTATION EDEC3	PMS*
0.00	-1.980	92	-0.271	0.00	-1.410	92	-0.193
0.25	-1.065	24	-0.146	0.25	-1.085	24	-0.138
0.50	-0.800	16	-0.120	0.50	-0.830	16	-0.114
0.75	-0.765	12	-0.105	0.75	-0.625	12	-0.086
1.00	-0.470	6	-0.064	1.00	-0.335	6	-0.046
1.25	-0.165	2	-0.023	1.25	-0.110	2	-0.015

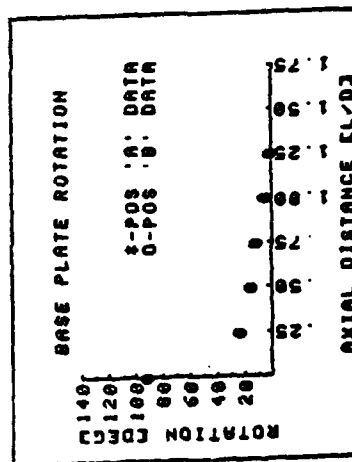
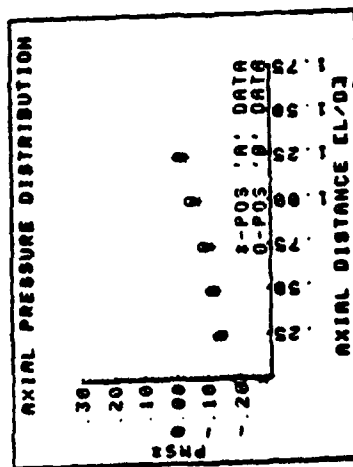
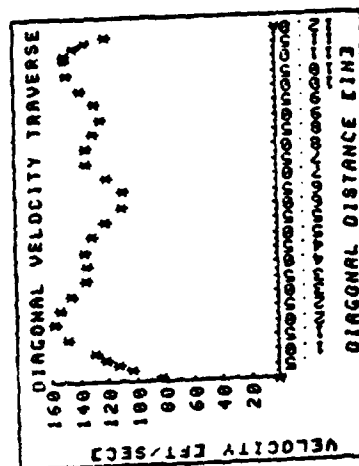
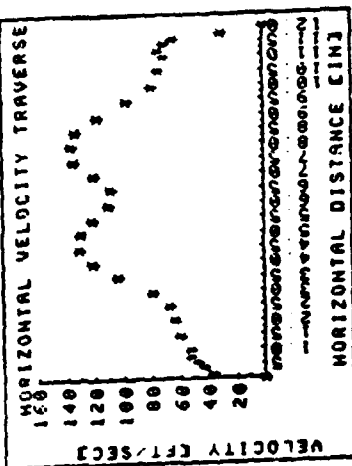


TABLE 44.2 - MSD DATA FOR 15/20 NOZZLES WITH L/D=1.25 STACK



HORIZONTAL VELOCITY TRAVERSE AT BASE ROTATION OF 04 DEGREES									
POSITION	0.00	0.20	0.40	0.60	0.80	1.00	1.20	1.40	1.60
PEIN H203	0.00	0.30	0.40	0.50	0.60	0.60	0.60	0.60	0.60
VEFT/SEC	0.00	36.78	42.47	47.48	52.01	52.01	52.01	52.01	52.01
POSITION	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00
PEIN H203	0.00	1.00	1.40	2.40	3.30	3.80	3.70	3.70	3.70
VEFT/SEC	63.78	67.14	79.45	104.02	121.97	130.89	129.15	129.15	129.15
POSITION	5.50	6.00	6.50	7.00	7.50	8.00	8.50	9.00	9.50
PEIN H203	3.30	2.70	2.60	3.20	4.00	4.10	3.90	3.90	3.90
VEFT/SEC	121.97	110.33	108.27	120.11	134.29	135.96	132.60	132.60	132.60
POSITION	9.00	9.50	10.00	10.50	11.00	11.20	11.40	11.40	11.40
PEIN H203	3.10	2.10	1.40	1.20	1.10	1.20	1.10	1.10	1.10
VEFT/SEC	110.22	97.30	79.45	73.55	70.42	73.55	70.42	73.55	70.42
POSITION	11.60	11.80	12.00	12.00	12.00	12.00	12.00	12.00	12.00
PEIN H203	0.90	0.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DIAGONAL VELOCITY TRAVERSE FOR BASE ROTATION OF 04 DEGREES									
POSITION	0.00	0.20	0.40	0.60	0.80	1.00	1.20	1.40	1.60
PEIN H203	0.00	1.50	2.40	2.80	3.30	3.70	4.90	4.90	4.90
VEFT/SEC	0.00	82.23	104.02	112.35	121.97	129.15	140.63	140.63	140.63
POSITION	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00
PEIN H203	5.50	5.20	4.70	4.10	4.00	4.10	3.80	3.80	3.80
VEFT/SEC	157.47	153.11	145.56	135.96	134.29	135.96	130.89	130.89	130.89
POSITION	5.50	6.00	6.50	7.00	7.50	8.00	8.50	9.00	9.50
PEIN H203	3.30	2.70	2.60	3.20	4.00	4.00	3.70	3.70	3.70
VEFT/SEC	121.97	110.33	108.27	120.11	134.29	134.29	129.15	129.15	129.15
POSITION	9.00	9.50	10.00	10.50	11.00	11.20	11.40	11.40	11.40
PEIN H203	3.40	3.60	4.20	4.00	4.90	4.90	4.90	4.90	4.90
VEFT/SEC	123.81	127.40	137.60	147.11	140.63	140.63	142.43	142.43	142.43
POSITION	11.60	11.80	12.00	12.00	12.00	12.00	12.00	12.00	12.00
PEIN H203	4.00	3.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00

TABLE 44.3 - VTD DATA FOR 15/20 NOZZLES WITH L/D=1.25 STACK

DATA TAKEN ON: 26 AUG 81  
DATA TAKEN BY: C.C. DAVIS

MIXING STACK INFORMATION:	
LENGTH:	14.63
DIAMETER:	11.70
L/D RATIO:	1.23
C/D RATIO:	0.50

N	POR	OPOR	TOR	TUPT	TANG	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF W20		DEGREES	F			IN OF W20		SQARE INCHES	SQARE INCHES
1	0.71	22.1	57.4	111.6	72.0	3.35	3.06	0.00	0.000	0.00000
2	0.70	21.9	57.4	111.6	72.0	4.25	2.06	0.00	12.566	0.00000
3	0.71	22.2	57.6	111.0	72.0	4.90	1.47	0.00	25.133	0.00000
4	0.70	22.6	57.6	111.0	72.0	5.55	0.70	0.00	50.265	0.00000
5	0.70	21.9	57.0	111.6	72.0	6.05	0.00	0.00	100.531	0.00000
6	0.70	22.1	58.6	111.0	72.0	6.15	0.14	0.00	150.796	0.00000
7	0.70	22.0	58.0	112.0	72.0	6.50	0.01	0.00	0.00000	0.00000

SECONDARY BOX												
N	MS	P3	T3	P3/T3	MAT <sup>1</sup> .44	WP	WS	UP	UM	UUPT	UPT	MACH
RUN						LBM/SEC	LBM/SEC	FT/SEC	FT/SEC	FT/SEC		
1	0.000	0.4136	0.3767	0.4376	0.0000	3.7373	0.0000	162.09	72.04	72.84	0.062	
2	0.1642	0.2020	0.3707	0.3730	0.1591	3.7402	0.6141	100.82	91.33	72.33	0.062	
3	0.2756	0.1990	0.3704	0.2139	0.2670	3.7450	1.9376	101.82	91.31	72.73	0.062	
4	0.4933	0.1063	0.3684	0.1193	0.3307	3.7480	1.5116	100.69	99.35	72.20	0.062	
5	0.4841	0.0860	0.3707	0.0415	0.4951	3.7417	1.8114	100.10	104.40	72.05	0.061	
6	0.5119	0.0324	0.3704	0.0206	0.4939	3.7529	1.9213	100.64	106.67	72.26	0.062	
7	0.3338	0.0014	0.3200	0.0015	0.3338	3.7455	2.6730	100.34	333.88	72.14	0.062	

**TABLE 45 - PCD DATA FOR 15/30 NOZZLES WITH L/D=1.25 STACK**

TERTIARY BOX

N	WT	PT	TT	PT/TT	WT/TT	WT	UE
RUN							
1	0.0000	0.0000	0.9307	0.0000	0.0000	3.757	0.0000
2	0.0000	0.0000	0.9307	0.0000	0.0000	4.354	0.0000
3	0.0000	0.0000	0.9304	0.0000	0.0000	4.803	0.0000
4	0.0000	0.0000	0.9304	0.0000	0.0000	5.260	0.0000
5	0.0000	0.0000	0.9307	0.0000	0.0000	5.553	0.0000
6	0.0000	0.0000	0.9304	0.0000	0.0000	5.674	0.0000
7	0.0000	0.0000	0.9300	0.0000	0.0000	0.0000	0.0000

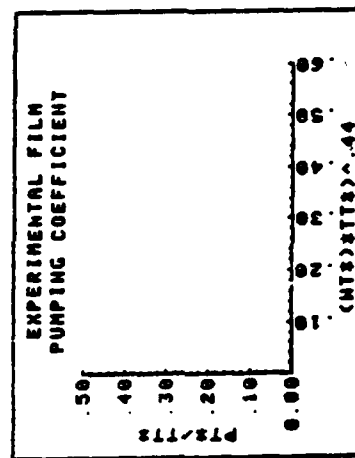
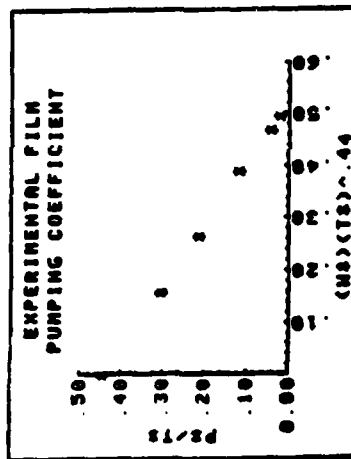


TABLE 45.1 - PCD DATA (CONT) FOR 15/30 NOZZLES WITH L/D=1.25 STACK



DATA TAKEN ON: 26 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

NOZZLE AN/AP AREA RATIO: 2.50  
 20 TILT/10 ROTATION/PCD

COMMENTS:  
 20 TILT/10 ROTATION/PCD

MIXING STACK INFORMATION:  
 LENGTH: 14.63 CINH  
 DIAMETER: 11.70 CINH  
 L/D RATIO: 1.25  
 S/D RATIO: 0.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 20.0 CDEG  
 ROTATION ANGLE: 10 CDEG  
 AREA PER NOZZLE: 10.752 CINH2  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINH2  
 ATM. PRESSURE: 29.99 CINH2

N	POR	DPOR	TOR	TUPT	TAMB	PUP	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
IN OF H2O	DEGREES F	IN OF H2O	IN OF H2O	IN OF H2O	IN OF H2O	IN OF H2O	IN OF H2O	IN OF H2O	SQUARE INCHES	SQUARE INCHES
1	0.71	22.1	50.2	111.0	72.0	3.70	2.03	0.00	0.000	0.000
2	0.70	21.9	50.0	111.0	71.0	4.45	1.96	0.00	12.566	0.000
3	0.71	22.2	57.6	111.0	72.0	4.95	1.40	0.00	25.133	0.000
4	0.70	22.1	57.6	111.0	72.0	5.45	0.79	0.00	50.265	0.000
5	0.70	22.0	57.6	111.0	72.0	5.85	0.31	0.00	100.531	0.000
6	0.71	22.1	50.0	111.0	72.0	6.05	0.16	0.00	150.796	0.000
7	0.71	22.1	50.4	112.0	71.0	6.15	0.01	0.00	0.000	0.000

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SECONDARY BOX

N	W2	P2	T2	P2/T2	W2/T2	44	NP	HS	UP	UM	UPT	UPT NACH
RUN								LBM/SEC	LBM/SEC	FT/SEC	FT/SEC	
1	0.0000	0.3027	0.9304	0.4114	0.0000	0.0000	3.7543	0.0000	101.91	72.77	72.77	0.062
2	0.1603	0.2684	0.9300	0.2085	0.1552	3.7301	0.5992	100.73	83.02	72.30	0.062	
3	0.2690	0.1097	0.9304	0.2039	0.2606	3.7643	1.0126	101.75	90.04	72.71	0.062	
4	0.4030	0.1070	0.9304	0.1159	0.3923	3.7965	1.5213	101.10	99.69	72.45	0.062	
5	0.5005	0.0426	0.9304	0.0450	0.4926	3.7400	1.9060	100.48	106.33	72.20	0.062	
6	0.5470	0.0219	0.9304	0.0236	0.5299	3.7551	2.0539	100.75	109.09	72.31	0.062	
7	0.0000	0.0014	0.9297	0.0015	0.0000	3.7536	2.6736	100.60	0.0000	72.20	0.062	

TABLE 46 - PCD DATA FOR 20/10 NOZZLES WITH L/D-1.25 STACK

TERTIARY BOX

N	NTS	PT#	TT#	PT#/TT#	WTSTT#	WM	WT	UE
LBM/SEC LBM/SEC FT/SEC								
RUN								
1	0.0000	0.0000	0.9304	0.0000	0.0000	3.754	0.0000	0.0000
2	0.0000	0.0000	0.9300	0.0000	0.0000	4.337	0.0000	0.0000
3	0.0000	0.0000	0.9304	0.0000	0.0000	4.777	0.0000	0.0000
4	0.0000	0.0000	0.9304	0.0000	0.0000	5.270	0.0000	0.0000
5	0.0000	0.0000	0.9304	0.0000	0.0000	5.654	0.0000	0.0000
6	0.0000	0.0000	0.9304	0.0000	0.0000	5.009	0.0000	0.0000
7	0.0000	0.0000	0.9297	0.0000	0.0000	0.0000	0.0000	0.0000

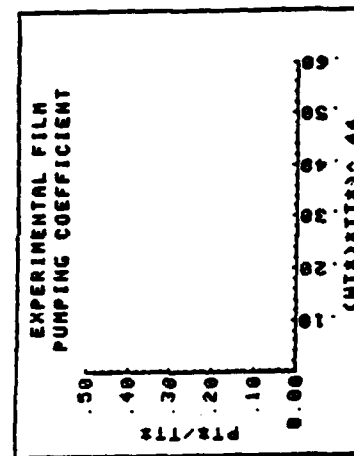
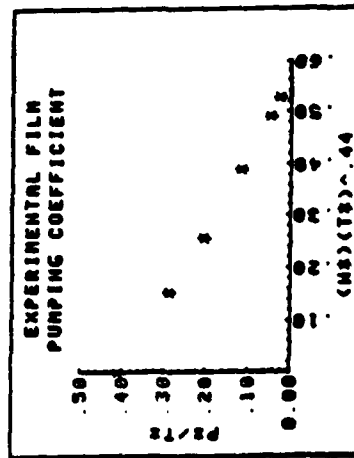


TABLE 48.1 - PCD DATA (CONT) FOR 20/10 NOZZLES WITH L/D=1.25 STACK

DATA TAKEN ON: 26 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

NOZZLE AN-AP AREA RATIO: 2.50  
 20 TILT/20 ROTATION/PCD

COMMENTS:  
 MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 EINH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 EINH<sup>2</sup>  
 ATM. PRESSURE: 29.99 EINH<sup>2</sup>

MIXING STACK INFORMATION:  
 LENGTH: 14.63 EINH  
 DIAMETER: 11.70 EINH  
 L/D RATIO: 1.25  
 S/D RATIO: 0.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 20.0 EDEG  
 ROTATION ANGLE: 20 EDEG  
 AREA PER NOZZLE: 10.752 EINH<sup>2</sup>  
 NUMBER OF NOZZLES: 4

N	POR	DPOR	TOR	TUPT	TAND	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.71	22.1	57.6	111.0	71.0	3.45	2.93	0.00	0.000	0.000
2	0.70	22.0	57.4	111.0	71.0	4.15	2.14	0.00	12.565	0.000
3	0.70	22.1	57.0	111.6	71.0	4.75	1.55	0.00	25.133	0.000
4	0.70	22.0	58.2	111.0	71.0	5.40	0.96	0.00	50.265	0.000
5	0.71	22.1	58.0	111.0	71.0	5.95	0.32	0.00	100.531	0.000
6	0.71	22.0	58.0	111.0	71.0	6.10	0.17	0.00	150.796	0.000
7	0.71	22.0	58.6	112.0	71.0	6.25	0.01	0.00	0.000	0.000

SECONDARY BOX

N	Wt	Pz	Tz	Pz/Tz	WST	44	WP	WS	UP	UM	UUPT	UPT	MACH
RUN													
1	0.0000	0.3954	0.9300	0.4252	0.0000	0.0000	3.7565	0.0000	102.06	72.03	72.03	0.062	
2	0.1670	0.2911	0.9300	0.3131	0.1618	0.1618	3.7488	0.6261	101.33	83.74	72.54	0.062	
3	0.2035	0.2105	0.9303	0.2263	0.2747	0.2747	3.7507	1.0657	101.49	91.68	72.60	0.062	
4	0.4230	0.1179	0.9300	0.1260	0.4105	0.4105	3.7459	1.5876	100.62	100.67	72.26	0.062	
5	0.5150	0.0430	0.9300	0.0471	0.4596	0.4596	3.7531	1.9360	100.02	107.01	72.34	0.062	
6	0.5652	0.0234	0.9300	0.0231	0.5474	0.5474	3.7466	2.1175	100.35	110.05	72.15	0.062	
7	0.0000	0.0014	0.9297	0.0015	0.0000	0.0000	3.7444	2.6736	100.24	0.0000	72.10	0.062	

TABLE 47 - PCD DATA FOR 20/20 NOZZLES WITH L/D=1.25 STACK

N	MTS	PIS	ITS	PIS/ITS	WSTT^-.44	LBM/SEC	LOM/SEC	HT	UE
1	0.0000	0.0000	0.0000	0.0000	0.0000	3.757	0.0000	0.0000	0.0000
2	0.0000	0.0000	0.0000	0.0000	0.0000	4.375	0.0000	0.0000	0.0000
3	0.0000	0.0000	0.0000	0.0000	0.0000	4.824	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000	0.0000	0.0000	5.333	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	0.0000	0.0000	5.662	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000	0.0000	0.0000	5.864	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000	0.0000	0.0000	6.000	0.0000	0.0000	0.0000

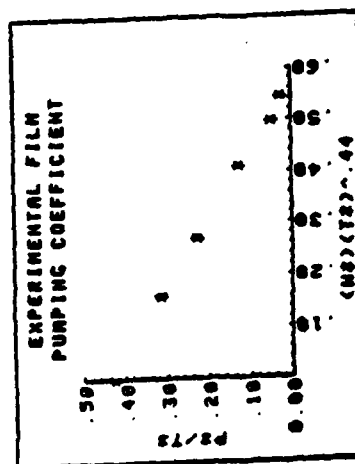
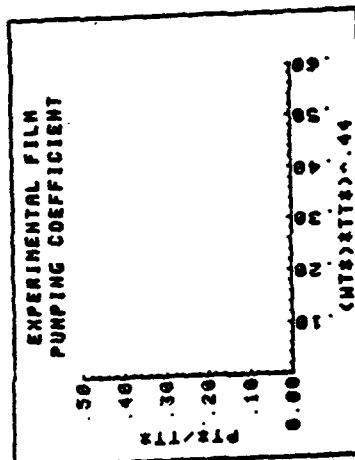


TABLE 47.1 -- PCD DATA (CONT) FOR 20/20 NOZZLES WITH L/D=1.25 STACK

DATA TAKEN ON: 27 AUG 81  
 DATA TAKEN BY: DRUCKER/DAVIS  
 NOZZLE AN/AP AREA RATIO: 2.50  
 20 TILT/20 ROTATION/FULL  
 COMMENTS:  
 MIXING STACK INFORMATION:  
 LENGTH: 14.63 L/N3  
 DIAMETER: 11.78 L/N3  
 L/D RATIO: 1.25  
 S/D RATIO: 0.50  
 PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 20.0 COEG3  
 ROTATION ANGLE: 20 COEG3  
 AREA PER NOZZLE: 10.752 L/N23  
 NUMBER OF NOZZLES: 4  
 MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 L/N3  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 L/N23  
 ATM. PRESSURE: 29.03 CINHG3

M	FOR	QPOP	TOR	TUPT	TANS	PUPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF N2O	DEGREES F					IN OF H2O		SQUARE INCHES	SQUARE INCHES
1	0.71	22.2	59.6	113.0	74.0	3.50	2.93	0.00	0.000	*****
2	0.71	22.2	59.6	113.0	74.0	4.20	2.14	0.00	12.566	*****
3	0.71	22.0	59.6	113.0	74.0	4.75	1.51	0.00	25.133	*****
4	0.71	22.1	59.0	113.2	73.0	5.45	0.85	0.00	50.265	*****
5	0.71	22.0	59.6	113.2	73.6	5.90	0.32	0.00	100.531	*****
6	0.71	22.0	59.4	113.2	73.0	6.05	0.17	0.00	150.796	*****
7	0.71	22.1	59.2	113.0	73.6	6.25	0.01	0.00	*****	*****

# SECONDARY BOX

N	W2	P2	T2	P2/T2	W2/T2	MP	WS	UP	UM	UPT	UPT MACH
RUN							LBM/SEC	LBM/SEC	FT/SEC	FT/SEC	
1	0.0000	0.3947	0.9319	0.4235	0.0000	3.7490	0.0000	103.10	73.25	73.25	0.062
2	0.1653	0.2897	0.9319	0.3109	0.1612	3.7477	0.6231	102.64	84.32	73.06	0.062
3	0.2006	0.2069	0.9319	0.2221	0.2720	3.7300	1.0469	101.53	91.54	72.62	0.062
4	0.4203	0.1163	0.9312	0.1240	0.4073	3.7305	1.5711	101.60	101.06	72.60	0.062
5	0.5169	0.0440	0.9309	0.0473	0.5009	3.7300	1.9204	101.06	107.25	72.42	0.062
6	0.5649	0.0234	0.9312	0.0251	0.5475	3.7315	2.1079	101.03	110.50	72.42	0.062
7	0.0000	0.0014	0.9312	0.0015	0.0000	3.7407	2.6619	101.34	0.0000	72.54	0.062

TABLE 48 - PCD DATA FOR 20/20 NOZZLES WITH L/D-1.25 STACK (FULL RUN)

TERTIARY BOX

N	MTS	PTS	ITS	PT2/IT2	WT2IT1^-.44	WM	WT	UE
RUN						LBM/SEC	LBM/SEC	FT/SEC
1	0.0000	0.0000	0.9319	0.0000	0.0000	3.750	0.0000	0.0000
2	0.0000	0.0000	0.9319	0.0000	0.0000	4.371	0.0000	0.0000
3	0.0000	0.0000	0.9319	0.0000	0.0000	4.778	0.0000	0.0000
4	0.0000	0.0000	0.9312	0.0000	0.0000	5.310	0.0000	0.0000
5	0.0000	0.0000	0.9309	0.0000	0.0000	5.659	0.0000	0.0000
6	0.0000	0.0000	0.9312	0.0000	0.0000	5.839	0.0000	0.0000
7	0.0000	0.0000	0.9312	0.0000	0.0000	0.0000	0.0000	0.0000

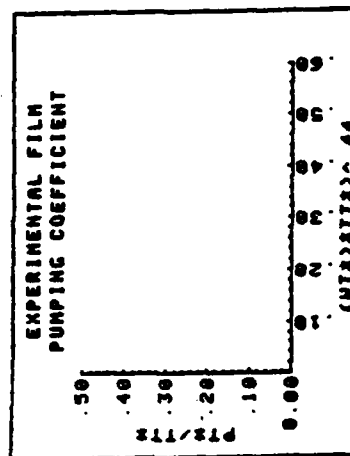
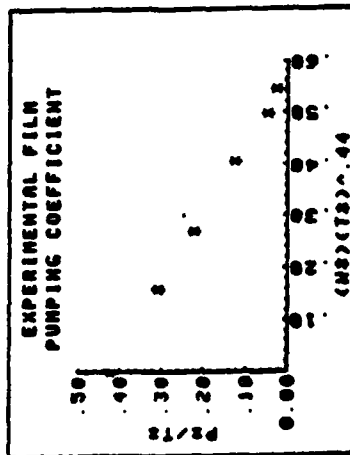


TABLE 48.1 - PCO DATA (CONT) FOR 20/20 NOZZLES WITH L/D=1.25 STACK

# MIXING STACK DATA FOR RUN 7

TOP (POSITION 'A') DATA			DIAGONAL (POSITION 'B') DATA		
X/D	PRESSURE [IN H2O]	ROTATION [DEG]	PMS	X/D	PRESSURE [IN H2O]
0.00	-2.040	22	-0.280	0.00	-1.510
0.25	-1.245	22	-0.171	0.25	-0.975
0.50	-0.090	17	-0.122	0.50	-0.595
0.75	-0.635	16	-0.087	0.75	-0.335
1.00	-0.410	4	-0.056	1.00	0.040
1.25	-0.210	14	-0.029	1.25	0.040
					0.005

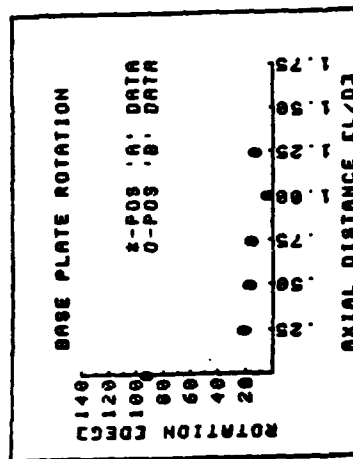
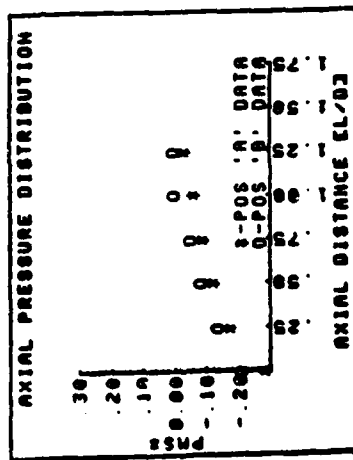
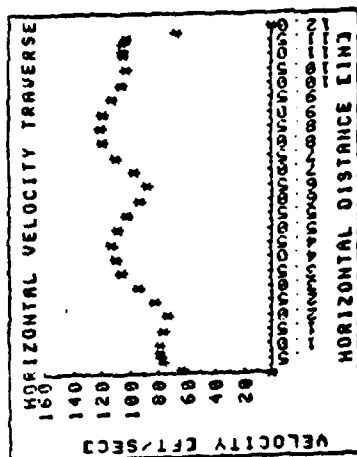


TABLE 48.2 - MSD DATA FOR 20/20 NOZZLES WITH L/D=1.25 STACK

HORIZONTAL VELOCITY TRAVERSE AT BASE ROTATION OF 85 DEGREES

POSITION	0.00	0.20	0.40	0.60	0.80	1.00	1.50
PEIN H203	0.00	0.90	1.30	1.40	1.40	1.40	1.30
VEFT/SEC	0.00	63.73	76.59	79.48	79.48	79.48	76.59
POSITION	2.00	2.50	3.00	3.50	4.00	4.50	5.00
PEIN H203	1.20	1.50	2.00	2.50	2.70	2.80	2.60
VEFT/SEC	73.59	92.27	95.00	106.21	110.39	112.41	103.32
POSITION	5.50	6.00	6.50	7.00	7.50	8.00	8.50
PEIN H203	2.30	1.90	1.70	2.10	2.70	3.10	3.20
VEFT/SEC	101.88	92.60	87.59	97.35	110.38	118.28	120.17
POSITION	9.00	9.50	10.00	10.50	11.00	11.20	11.40
PEIN H203	3.10	2.80	2.50	2.30	2.40	2.40	2.40
VEFT/SEC	110.28	112.41	106.21	101.88	104.07	104.07	104.07
POSITION	11.60	11.00	12.00				
PEIN H203	2.30	1.00	0.00				



DIAGONAL VELOCITY TRAVERSE FOR BASE ROTATION OF 85 DEGREES

POSITION	0.00	0.20	0.40	0.60	0.80	1.00	1.50
PEIN H203	0.00	1.20	4.10	4.70	4.90	5.10	4.90
VEFT/SEC	0.00	73.59	136.02	145.63	148.70	151.71	148.70
POSITION	2.00	2.50	3.00	3.50	4.00	4.50	5.00
PEIN H203	4.30	3.70	3.50	3.30	3.20	2.90	2.50
VEFT/SEC	139.38	129.22	125.68	122.03	120.17	114.40	106.21
POSITION	5.50	6.00	6.50	7.00	7.50	8.00	8.50
PEIN H203	2.10	1.80	1.60	2.20	2.80	3.10	3.00
VEFT/SEC	97.35	90.13	90.13	99.64	112.41	116.28	116.35
POSITION	9.00	9.50	10.00	10.50	11.00	11.20	11.40
PEIN H203	2.80	2.50	2.60	3.20	4.30	4.90	5.10
VEFT/SEC	112.41	106.21	108.32	120.17	139.38	148.70	151.71
POSITION	11.60	11.00	12.00				
PEIN H203	5.10	4.40	0.00				

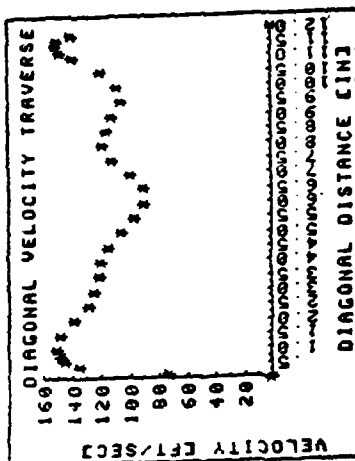


TABLE 48.3 - VTD DATA FOR 20/20 NOZZLES WITH L/D=1.25 STACK



DATA TAKEN ON: 27 AUG 81  
DATA TAKEN BY: C.C. DAVIS

MIXING STACK INFORMATION:  
LENGTH: 14.63 CINH  
DIAMETER: 11.70 CINH  
L/D RATIO: 1.25  
S/O RATIO: 0.50

NOZZLE AN/AP AREA RATIO: 2.50  
PRIMARY NOZZLE INFORMATION:  
TILT ANGLE: 20.0 COEG3  
ROTATION ANGLE: 30 COEG3  
AREA PER NOZZLE: 10.752 CINH2  
NUMBER OF NOZZLES: 4

COMMENTS:  
20 TILT/30 ROTATION/PCD  
MISCELLANEOUS INFORMATION:  
ORIFICE DIAMETER: 6.902 CINH  
ORIFICE BETA: 0.497  
UPTAKE AREA: 107.510 CINH2  
ATM. PRESSURE: 29.99 CINHG3

N	POR	DPOR	TOR	TUPT	TAMB	PUPPT	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F				IN OF H2O			SQUARE INCHES	SQUARE INCHES
1	0.71	22.2	50.0	111.0	71.6	3.20	3.14	0.00	0.000	xxxxxx
2	0.71	22.1	57.0	111.0	71.6	4.10	2.20	0.00	12.566	xxxxxx
3	0.70	22.0	57.0	111.0	71.6	4.65	1.50	0.00	25.133	xxxxxx
4	0.70	22.0	57.0	111.6	71.6	5.35	0.00	0.00	50.265	xxxxxx
5	0.71	22.1	57.6	111.6	71.6	5.90	0.33	0.00	100.531	xxxxxx
6	0.70	22.1	57.2	111.4	71.6	6.05	0.17	0.00	150.796	xxxxxx
7	0.70	22.0	56.6	111.2	71.6	6.20	0.01	0.00	xxxxxx	xxxxxx

# SECONDARY BOX

N	M3	P3	T3	P3/T3	W3T3	44	MP	NS	UP	UM	UUPPT	UPT	MACH
RUN													
1	0.0000	0.4216	0.9297	0.4535	0.0000	3.7636	0.0000	102.50	73.00	73.01	0.062		
2	0.1690	0.2900	0.9297	0.3205	0.1637	3.7558	0.6349	101.70	84.04	72.69	0.062		
3	0.2872	0.2156	0.9297	0.2320	0.2701	3.7473	1.0762	101.01	91.67	72.41	0.062		
4	0.4203	0.1204	0.9300	0.1295	0.4140	3.7502	1.6062	100.70	101.06	72.32	0.062		
5	0.5237	0.0451	0.9300	0.0405	0.5072	3.7565	1.9672	100.04	107.54	72.34	0.062		
6	0.5636	0.0233	0.9303	0.0250	0.5460	3.7500	2.1179	100.77	110.21	72.32	0.062		
7	0.5888	0.0014	0.9306	0.0015	0.5888	3.7517	2.6741	100.33	xxxxxx	72.14	0.062		

TABLE 49 - PCD DATA FOR 20/30 NOZZLES WITH L/D-1.25 STACK

TERMINARY BOX

N	MTS	PTS	TTs	PTs/TTs	MTsTTs	44	WM	WT	UE
RUN							LBM/SEC	LBM/SEC	FT/SEC
1	000000	0.0000	0.9297	0.0000	000000	000000	3.764	000000	000000
2	000000	0.0000	0.9297	0.0000	000000	000000	4.391	000000	000000
3	000000	0.0000	0.9297	0.0000	000000	000000	4.923	000000	000000
4	000000	0.0000	0.9300	0.0000	000000	000000	5.356	000000	000000
5	000000	0.0000	0.9300	0.0000	000000	000000	5.724	000000	000000
6	000000	0.0000	0.9303	0.0000	000000	000000	5.876	000000	000000
7	000000	0.0000	0.9306	0.0000	000000	000000	000000	000000	000000

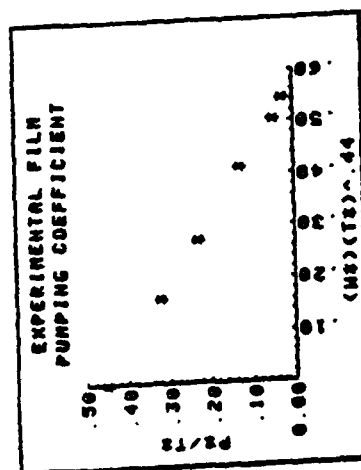
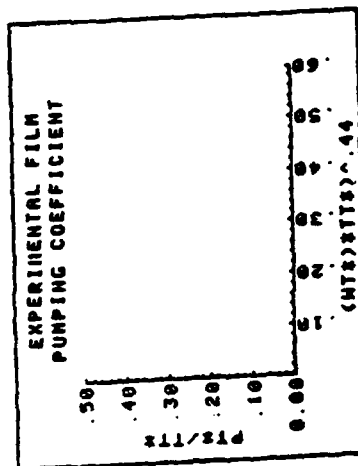


TABLE 49.1 - PCD DATA (CONT) FOR 20/30 NOZZLES WITH L/D=1.25 STACK

DATA TAKEN ON: 27 AUG 81  
 DATA TAKEN BY: C.C. DAVIS

MIXING STACK INFORMATION:  
 LENGTH: 14.63 LIN3  
 DIAMETER: 11.70 LIN3  
 L/D RATIO: 1.25  
 S/D RATIO: 0.50

NOZZLE AN/AP AREA RATIO: 2.50

COMMENTS:  
 22.5 TILT/10 ROTATION/PCD

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 22.5 CDEG3  
 ROTATION ANGLE: 10 CDEG3  
 AREA PER NOZZLE: 10.752 LIN23  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 LIN3  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 LIN23  
 ATH. PRESSURE: 29.03 CINHG3

N	FOR	DPOR	TOR	TUPT	TANB	PUP	PSEC	PTER	SECONDARY AREA	TERTIARY AREA
RUN	IN OF H2O	DEGREES F					IN OF H2O		SQUARE INCHES	SQUARE INCHES
1	0.71	22.2	56.0	111.0	71.0	4.35	2.78	0.00	0.000	0.000
2	0.71	22.1	56.0	111.0	71.0	4.95	1.95	0.00	12.566	0.000
3	0.70	22.0	56.0	111.0	71.0	5.40	1.39	0.00	25.133	0.000
4	0.71	22.2	56.0	111.0	71.0	6.05	0.79	0.00	50.265	0.000
5	0.71	22.1	57.2	111.0	72.0	6.50	0.30	0.00	100.531	0.000
6	0.71	22.1	57.0	111.2	71.0	6.65	0.16	0.00	150.796	0.000
7	0.70	22.1	57.6	111.4	72.0	6.00	0.01	0.00	0.000	0.000

# SECONDARY BOX

N	WS	PS	TS	PS/TS	MST-44	WP	WS	UP	UM	UPT	UPT MACH
RUN							LBM/SEC	LBM/SEC	FT/SEC	FT/SEC	
1	0.0000	0.3742	0.9313	0.4010	0.0000	3.7570	0.0000	102.70	73.12	73.12	0.062
2	0.1590	0.2640	0.9313	0.2043	0.1541	3.7494	0.5960	102.00	83.53	72.81	0.062
3	0.2690	0.1901	0.9313	0.2041	0.2600	3.7409	1.0065	101.33	90.65	72.54	0.062
4	0.4030	0.1074	0.9313	0.1153	0.3914	3.7570	1.5175	101.09	100.07	72.76	0.062
5	0.4909	0.0411	0.9317	0.0441	0.4836	3.7479	1.0700	101.19	106.15	72.48	0.062
6	0.5466	0.0219	0.9310	0.0235	0.5296	3.7406	2.0400	101.22	109.37	72.50	0.062
7	0.0000	0.0014	0.9310	0.0010	0.0000	3.7460	2.6659	101.11	0.0000	72.45	0.062

TABLE 50 - PCD DATA FOR 22.5/10 NOZZLES WITH L/D=1.25 STACK

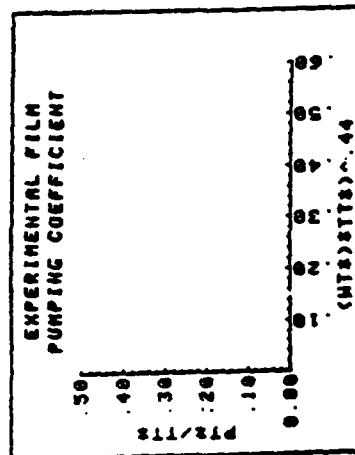
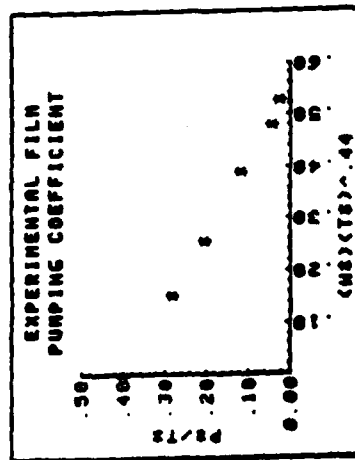
[illegible]

TABLE 50.1 - PCD DATA (CONT) FOR 22.5/10 NOZZLES WITH L/D=1.25 STACK

DATA TAKEN ON: 27 AUG 61  
 DATA TAKEN BY: C.C. DAVIS

NOZZLE AN/AP AREA RATIO: 2.50  
 COMMENTS: 22.5 TILT/20 ROTATION/PCD

MIXING STACK INFORMATION:  
 LENGTH: 14.63 CINH  
 DIAMETER: 11.70 CINH  
 L/D RATIO: 1.25  
 S/D RATIO: 0.50

PRIMARY NOZZLE INFORMATION:  
 TILT ANGLE: 22.5 DEGC3  
 ROTATION ANGLE: 20 DEGC3  
 AREA PER NOZZLE: 10.752 CINH2  
 NUMBER OF NOZZLES: 4

MISCELLANEOUS INFORMATION:  
 ORIFICE DIAMETER: 6.902 CINH  
 ORIFICE BETA: 0.497  
 UPTAKE AREA: 107.510 CINH2  
 ATM PRESSURE: 29.03 CINH2

N	POR	OPOR	TOR	TUPT	TAMB	PAPT	PSEC	PTER	SECONDARY AREA SQUARE INCHES	TERTIARY AREA SQUARE INCHES
RUN	IN OF H2O	DEGREES F					IN OF H2O			
1	0.71	22.2	56.6	111.0	72.0	3.90	2.94	0.00	0.000	0.000
2	0.70	22.0	57.0	111.0	72.0	4.65	2.11	0.00	12.566	0.000
3	0.70	21.9	56.6	110.0	71.0	5.20	1.50	0.00	25.133	0.000
4	0.70	22.1	56.6	110.6	72.0	5.05	0.04	0.00	50.265	0.000
5	0.70	22.0	56.6	110.6	72.2	6.35	0.31	0.00	100.531	0.000
6	0.71	22.2	56.0	110.6	72.0	6.50	0.16	0.00	150.796	0.000
7	0.71	22.2	57.0	110.0	72.0	6.65	0.01	0.00	0.000	0.000

# SECONDARY BOX

N	HS	P2	T2	P2/T2	WST-44	HP	HS	UP	UM	UPT	UPT MACM
RUN							LBH/SEC	LBH/SEC	FT/SEC	FT/SEC	
1	0.0000	0.3954	0.9317	0.4244	0.0000	3.7506	0.0000	102.09	73.16	73.16	0.062
2	0.1657	0.2070	0.9317	0.3089	0.1607	3.7402	0.6199	101.62	93.01	72.66	0.062
3	0.2001	0.2060	0.9316	0.2212	0.2715	3.7331	1.0456	100.94	91.20	72.30	0.062
4	0.4169	0.1147	0.9323	0.1230	0.4043	3.7523	1.5645	101.51	100.70	72.61	0.062
5	0.5079	0.0427	0.9327	0.0450	0.4926	3.7416	1.9003	100.76	106.54	72.31	0.062
6	0.5451	0.0213	0.9323	0.0234	0.5206	3.7570	2.0405	101.40	109.47	72.60	0.062
7	0.0000	0.0014	0.9320	0.0010	0.0000	3.7571	2.6659	101.44	0.0000	72.50	0.062

TABLE 51 - PCD DATA FOR 22.5/20 NOZZLES WITH L/D-1.25 STACK

TERTIARY BOX

N	WT	PT	TT	PTT/TT	WT/TT	WT	UE
LBM/SEC LBM/SEC FT/SEC							
RUN							
1	22222	0.0000	0.9317	0.0000	22222	3.759	22222
2	22222	0.0000	0.9317	0.0000	22222	4.360	22222
3	22222	0.0000	0.9316	0.0000	22222	4.779	22222
4	22222	0.0000	0.9323	0.0000	22222	5.317	22222
5	22222	0.0000	0.9327	0.0000	22222	5.642	22222
6	22222	0.0000	0.9323	0.0000	22222	5.886	22222
7	22222	0.0000	0.9320	0.0000	22222		22222

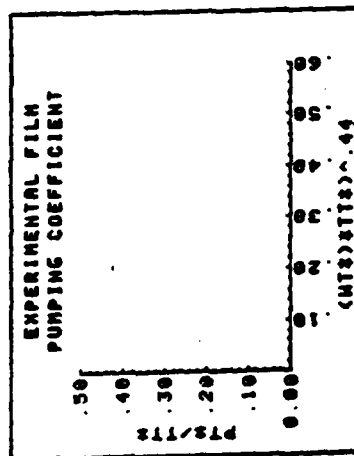
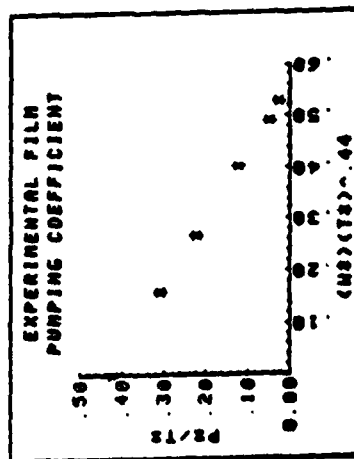


TABLE 51.1 - PCD DATA (CONT) FOR 22.5/20 NOZZLES WITH L/D=1.25 STACK

## APPENDIX: A

### ONE-DIMENSIONAL ANALYSIS OF A SIMPLE EDUCTOR

This thesis is a further extension of the work conducted by Ellin, Moss, Lemke and Staehli, Shaw, and Ryan [Ref. 1,2, 3,4, and 5] and uses the same one-dimensional analysis of a simple eductor system. Similarity between the basic geometries tested by previous researchers was maintained to correlate data and preserve the error analysis conducted by Ellin. The dimensionless parameters controlling the flow phenomena used previously were also used in the present research along with the basic means of data analysis and presentation. Dynamic similarity was maintained by using Mach number similarity to establish the gas eductor model's primary flow rate.

Although the analysis presented here is for an eductor model with only primary and secondary air flows, the basic discussion applies as well to systems with primary, secondary, and tertiary flows. Systems with tertiary and film or wall cooling air flows have been non-dimensionalized with the same base parameters as the secondary air flow and have been calculated using the same non-dimensional analysis. This allows easier comparison of tabulated and graphic results. Parameters pertaining to the secondary systems are subscripted with an "s" and those relating to the tertiary box are subscripted with a "t".

#### A. MODELING TECHNIQUE

Dynamic similarity between the models tested and an actual prototype was maintained by using the same primary air flow Mach number. For the primary air flow Mach number used (0.064), and based on the average flow properties within the mixing stack and the hydraulic diameter of the mixing stack, the air flow through the eductor system is turbulent ( $Re > 10^5$ ). As a consequence of this, momentum exchange is predominant over shear interaction, and the kinetic and internal energy terms are more influential on the flow than are viscous forces. It can also be shown that the Mach number represents the ratio of kinetic energy of a flow to its internal energy and is, therefore, a more significant parameter than the Reynolds number in describing the primary flow through the uptakes.

#### B. ONE-DIMENSIONAL ANALYSIS OF A SIMPLE EDUCTOR

The theoretical analysis of an eductor may be approached in two ways. One method attempts to analyse the details of the mixing process of the primary and secondary air streams as it takes place inside the mixing stack. This requires an interpretation of the mixing phenomenon which, when applied to a multiple nozzle system, becomes extremely complex. The other method, which was chosen here, analyzes the overall performance of the eductor system and is not concerned with the actual mixing process. The one-dimensional analysis based on a single primary nozzle exhausting into a mixing stack, is



shown in Figure A-1. To avoid repetition with previous reports, only the main parameters and assumption will be represented here. A complete derivation of analysis used can be found in Reference [1] and [9]. The one-dimensional flow analysis of the simple eductor system described depends on the simultaneous solution of the continuity, momentum and energy equations coupled with the equation of state, all compatible with specific boundary conditions.

The idealizations made for simplifying the analysis are as follows:

1. The flow is steady state and incompressible.
2. Adiabatic flow exists throughout the eductor with isentropic flow of the secondary stream from the plenum (at section 0) to the throat or entrance of the mixing stack (at section 1) and irreversible adiabatic mixing of the primary and secondary streams occurs in the mixing stack (between sections 1 and 2).
3. The static pressure across the flow at the entrance and exit planes of the mixing-tube (at sections 1 and 2) is uniform.
4. At the mixing-stack entrance (section 1) the primary flow velocity  $U_p$  and temperature  $T_p$  are uniform across the primary stream, and the secondary flow velocity  $U_s$  and temperature  $T_s$  are uniform across the secondary stream, but  $U_p$  does not equal  $U_s$ , and  $T_p$  does not equal  $T_s$ .

5. Incomplete mixing of the primary and secondary streams in the mixing stack is accounted for by the use of a non-dimensional momentum correction factor  $K_m$  which relates the actual momentum rate to the pseudo-rate based on the bulk-average velocity and density and by the use of a non-dimensional kinetic energy correction factor  $K_e$  which relates the actual kinetic energy rate to the pseudo-rate based on the bulk-average velocity and density.
6. Both gas flows behave as perfect gases.
7. Flow potential energy position changes are negligible.
8. Pressure changes  $P_{s0}$  to  $P_{s1}$  and  $P_1$  to  $P_a$  are small relative to the static pressure so that the gas density is essentially dependent upon temperature (and atmospheric pressure).
9. Wall friction in the mixing stack is accounted for with the conventional pipe friction factor term based on the bulk-average flow velocity  $U_m$  and the mixing stack wall area  $A_w$ .

The following parameters, defined here for clarity, will be used in the following development.

$\frac{A_p}{A_m}$  area ratio of primary flow area to mixing stack cross sectional area

$\frac{A_w}{A_m}$  area ratio of wall friction area to mixing stack cross sectional area

$k_p$  momentum correction factor for primary mixing

$k_m$  momentum correction factor for mixed flow

$f$  wall friction factor

Based on the continuity equation, the conservation of mass principle for steady flow yields

$$W_m = W_p + W_s + W_t \quad (1)$$

where

$$W_p = \rho_p U_p A_p$$

$$W_s = \rho_s U_s A_s$$

$$W_t = \rho_t U_t A_t$$

$$W_m = \rho_m U_m A_m$$

(1a)

All of the above velocity and density terms, with the exception of  $\rho_m$  and  $U_m$ , are defined without ambiguity by the virtue of idealizations (3) and (4) above. Combining equations (1) and (1a) above, the bulk average velocity at the exit plane of the mixing stack becomes

$$U_m = \frac{W_s + W_t + W_p}{\rho_m A_m} \quad (1b)$$

where  $A_m$  is fixed by the geometric configuration and

$$\rho_m = \frac{P_a}{RT_m} \quad (2)$$

where  $T_m$  is calculated as the bulk average temperature from the energy equation (9) below. The momentum equation stems from Newton's second and third laws of motion and is the conventional force and momentum-rate balance in fluid mechanics.

$$K_p \left( \frac{W_p U_p}{g_c} \right) + \left( \frac{W_s U_s}{g_c} \right) + \left( \frac{W_t U_t}{g_c} \right) + P_1 A_1 = K_m \left( \frac{W_m U_m}{g_c} \right) + P_2 A_2 + F_{fr} \quad (3)$$

Note the introduction of idealizations (3) and (5). To account for a possible non-uniform velocity profiles across the primary nozzle exit, the momentum correction factor  $K_p$  is introduced here. It is defined in a manner similar to that of  $K_m$  and by idealization (4), supported by work conducted by Moss, it is set equal to unity.  $K_p$  is carried through this analysis only to illustrate its effect on the final result. The momentum correction factor for the mixing stack exit is defined by the relation

$$K_m = \frac{1}{W_m U_m} \int_0^{A_m} U_m^2 \rho_2 dA \quad (4)$$

where  $U_m$  is evaluated as the bulk-average velocity from equation (1b). The wall skin friction force  $F_{fr}$  can be related to the flow stream velocity by

$$F_{fr} = f A_w \left( \frac{U_m^2 \rho_m}{2g_c} \right) \quad (5)$$

using idealization (9). As a reasonably good approximation for turbulent flow, the friction factor may be calculated from the Reynolds number

$$f = 0.046 (Re_m)^{-0.2} \quad (6)$$

Applying the conservation of energy principle to the steady flow system in the mixing stack between the entrance and exit planes,

$$\begin{aligned} W_p \left( h_p + \frac{U_p^2}{2g_c} \right) + W_s \left( h_s + \frac{U_s^2}{2g_c} \right) + W_t \left( h_t + \frac{U_t^2}{2g_c} \right) \\ = W_m \left( h_m + K_e \frac{U_m^2}{2g_c} \right) \end{aligned} \quad (7)$$

neglecting potential energy of position changes (idealization 7). Note the introduction of the kinetic energy correction factor  $K_e$ , which is defined by the relation

$$K_e = \frac{1}{W_m U_m^2} \int_0^{A_m} U_2^3 \rho_2 dA \quad (8)$$

It may be demonstrated that for the purpose of evaluating the mixed mean flow temperature  $T_m$ , the kinetic energy terms may be neglected to yield

$$h_m = \frac{W_p}{W_m} h_p + \frac{W_s}{W_m} h_s + \frac{W_t}{W_m} h_t \quad (9)$$

where  $T_m = \phi(h_m)$  only, with the idealization (6).

The energy equation for the isentropic flow of the secondary air from the plenum to the entrance of the mixing stack may be shown to reduce to

$$\frac{p_o - p_s}{\rho_s} = \frac{U_s^2}{2g_s} \quad (10)$$

similarly, the energy equation for the tertiary air flow reduces to

$$\frac{p_o - p_t}{\rho_t} = \frac{U_t^2}{2g_c}$$

The previous equations may be combined to yield the vacuum produced by the eductor action in either the secondary or tertiary air plenums. For the secondary air plenum, the vacuum produced is

$$P_a - P_{os} = \frac{1}{g_c A_m} \left( K_p \frac{W_p^2}{A_p \rho_p} + \frac{W_s^2}{A_s \rho_s} \left( 1 - \frac{1}{2} \frac{A_m}{A_s} \right) - \frac{W_m^2}{A_m \rho_m} \left( K_m + \frac{f}{2} \frac{A_w}{A_m} \right) \right) \quad (11)$$

where it is understood that  $A_p$  and  $\rho_s$  apply to the secondary flow at this same section, and  $A_m$  and  $W_m$  apply to the mixed flow at the exit of the mixing stack system.  $P_a$  is atmospheric pressure, and is equal to the pressure at the exit of the mixing stack.  $A_w$  is the area of the inside wall of the mixing stack.

For the tertiary air plenum, the vacuum produced is

$$P_a - P_{ot} = \frac{1}{g_c A_m} \left( K_p \frac{(W_p + W_s)^2}{(A_p \rho_p + A_s)} + \frac{W_t^2}{A_t \rho_t} \left( 1 - \frac{1}{2} \frac{A_m}{A_t} \right) \right) \\ = \frac{W_m^2}{A_m \rho_m} \left( K_m + \frac{f}{2} \frac{A_w}{A_m} \right) \quad (11a)$$

where the primary flow now consists of both the primary and secondary air flows.

### C. NON-DIMENSIONAL FORM OF THE SIMPLE EDUCTOR EQUATION

In order to provide the criteria of similarity of flows with geometric similarity, the non-dimensional parameters which govern the flow must be determined. The means chosen for determining these parameters was to normalize equations (11) and (11a) with the following dimensionless groupings.

$$P^* = \frac{\frac{P_a - P_{os}}{\rho_s}}{\frac{U_p^2}{2g_c}}$$

a pressure coefficient which compares the pumped head  $P_a - P_{os}$  for the secondary flow to the driving head  $\frac{U_p^2}{2g_c}$  of the primary flow

$$PT^* = \frac{\frac{P_a - P_{ot}}{\rho_t}}{\frac{U_p^2}{2g_c}}$$

a pressure coefficient which compares the pumped head  $P_a - P_{ot}$  for the tertiary flow to the driving head  $\frac{U_p^2}{2g_c}$  of the primary flow

$$W^* = \frac{W_s}{W_p}$$

a flow rate ratio, secondary to primary mass flow rate

$$WT^* = \frac{W_t}{W_p}$$

a flow rate ratio, tertiary to primary mass flow rate

$$T^* = \frac{T_s}{T_p}$$

an absolute temperature ratio, secondary to primary



$$T T^* = \frac{T_t}{T_p}$$

an absolute temperature ratio,  
tertiary to primary

$$\rho_s^* = \frac{\rho_s}{\rho_p}$$

a flow density ratio of the sec-  
ondary to primary flows. (Note  
that since the fluids are con-  
sidered perfect gases,

$$\rho_s^* = \frac{T_p}{T_s} = \frac{1}{T_s^*}$$

$$\rho_t^* = \frac{\rho_t}{\rho_p}$$

a flow density ratio of the ter-  
tiary or fil, cooling flow to  
primary flows. (Note that since  
the fluids are considered per-  
fect gases,

$$\rho_t^* = \frac{T_p}{T_t} = \frac{1}{T_t^*}$$

$$A_s^* = \frac{A_s}{A_p}$$

an area ratio of secondary flow  
area to primary flow area

$$A_t^* = \frac{A_t}{A_p}$$

an area ratio of tertiary flow  
area to primary flow area

With these non-dimensional groupings, equations (11) and (11a) can be rewritten in dimensionless form. Since both equations follow the same format, only the results for the secondary air plenum will be presented here.

$$\frac{P^*}{T^*} = 2 \frac{A_P}{A_m} \left( (K_P - \frac{A_P}{A_m} \beta) - W^* (K_P + T^*) \frac{A_P}{A_m} \beta \right) + W^{*2} T^* \left( \frac{1}{A^*} (K_P - \frac{A_m}{2A^* A_P}) - \frac{A_P}{A_m} \beta \right) \quad (12)$$

where

$$\beta = K_m + \frac{f}{2} \frac{A_w}{A_m}.$$

This may be rewritten as

$$\frac{P^*}{T^*} = C_1 + C_2 W^* (T + 1) + C_3 W^{*2} T^* \quad (13)$$

where

$$C_1 = 2 \frac{A_P}{A_m} (K_P - \frac{A_P}{A_m} \beta),$$

$$C_2 = - \left( \frac{A_P}{A_m} \right)^2 \beta, \text{ and}$$

$$C_3 = 2 \frac{A_P}{A_m} \left( \frac{1}{A^*} - \frac{A_m}{2A^* A_P} \beta - \frac{A_P}{A_m} \beta \right).$$

As can be seen from equation (13),

$$P^* = F(W^*, T^*).$$

The additional dimensionless quantities listed below were used to correlate the static pressure distribution down the length of the mixing stack.

$$PMS^* = \frac{\frac{PMS}{\rho_s}}{\frac{U_p^2}{2g_c}}$$

a pressure coefficient which compares the pumping head  $\frac{PMS}{\rho_s}$  for

the secondary flow to the driving head  $\frac{U_p^2}{2g_c}$  of the primary flow,

where PMS = static pressure along the mixing stack length

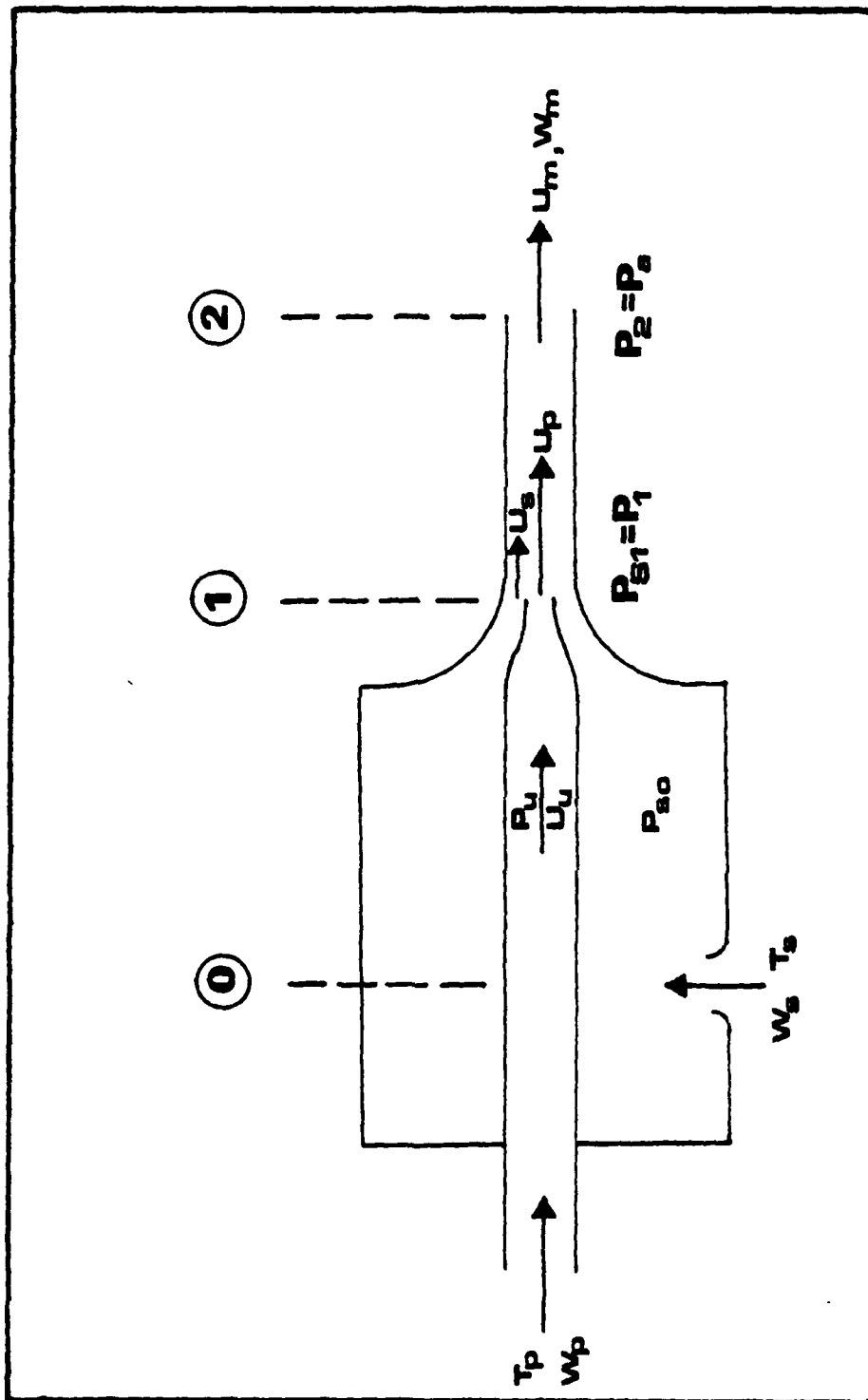


FIGURE A-1. SIMPLE SINGLE NOZZLE EDUCTOR SYSTEM

## APPENDIX: B

### FORMULAE

Presented here are the formulas used to obtain the primary and secondary mass flow rates. According to the ASME primary Test Code [Ref. 8], the general equation for mass flow rate appearing in equation (a)

$$W(\text{lbm/sec}) = (0.12705) K A Y F_a (\rho \Delta P)^{0.5} \quad (a)$$

may be used with flow nozzles and square edge orifices provided the flow is subsonic. In the above equation, K (dimensionless) represents the flow coefficient for the metering device and is defined as  $K = C(1 - \beta^4)^{-0.5}$  where C is the coefficient of discharge and  $\beta$  is the ratio of throat to inlet diameters;  $A(\text{in}^2)$  is the total cross sectional area of the metering device; Y (dimensionless) is the expansion factor for the flow;  $F_a$  (dimensionless) is the area thermal expansion factor;  $\rho$  ( $\text{lbm/ft}^3$ ) is the flow mass density; and  $\Delta P$  (inches  $\text{H}_2\text{O}$ ) is the differential pressure across the metering device. Each of these quantities are evaluated, according to the guidelines set forth in Reference [8], for the specific type of flow measuring device used.

Using a square edge orifice for measurement of the primary mass flow rate, the quantities in equation (a) are defined as follows:

1. The flow coefficient  $K$  is 0.62 based on a  $\beta$  of 0.502 and a constant coefficient of discharge over the range of flows considered of 0.60.
2. The orifice area is 37.4145 in<sup>2</sup>.
3. Corresponding to the range of pressure ratios encountered across the orifice, the expansion factor  $Y$  is 0.8.
4. Since the temperature of the metered air is nearly ambient temperature, thermal expansion factor is essentially 1.0.
5. The primary air mass density  $\rho_{or}$  is calculated using the perfect gas relationship with pressure and temperature evaluated upstream of the orifice.

Substituting these values into equation (a) yields

$$W_p \text{ (lbm/sec)} = (2.88455) (\rho_{or} \Delta P_{or})^{0.5} \quad (b)$$

The secondary mass flow rate is measured using long radius flow nozzles for which case the quantities in equation (a) becomes:

1. For a flow nozzle installed in a plenum,  $\beta$  is approximately zero in which case the flow coefficient is approximately equal to the coefficient of discharge. For the range of secondary flows encountered, the flow coefficient becomes 0.98.
2.  $A$  is the sum of the throat areas of the flow nozzles in use (in<sup>2</sup>).

3. Since the pressure ratios across the flow nozzles are very close to unity, the expansion coefficient  $Y$  is 1.0.
4. Since the temperature of the metered air is nearly ambient temperature, the thermal expansion factor is essentially 1.0.
5. The secondary air mass density  $\rho_s$  is evaluated using the perfect gas relationship at ambient conditions.

Substituting these values into equation (a) yields the equation for the secondary mass flow rate measured using long radius flow nozzles.

$$W_s \text{ (lbm/sec)} = 0.12451 A (\rho_s \Delta P_s)^{0.5} \quad (c)$$

## APPENDIX: C

### UNCERTAINTY ANALYSIS

The determination of the uncertainties in the experimentally determined pressure coefficients, pumping coefficients, and velocity profiles was made using the methods described by Kline and McClintock [Ref. 10]. The basic uncertainty analysis for the cold flow eductor model test facility was conducted by Ellin [Ref. 1]. The uncertainties obtained by Ellin using the second order equation suggested by Kline and McClintock were applicable to the experimental work conducted during the present research and are listed in the following table.

#### UNCERTAINTY IN MEASURED VALUES

$T_s$	$\pm 1 \text{ R}$
$T_p$	$\pm 1 \text{ R}$
$P_a$	$\pm 0.01 \text{ psia}$
$\Delta P$	$\pm 0.01 \text{ in. H}_2\text{O}$
$P_v$	$\pm 0.01 \text{ in. H}_2\text{O}$
$P_u$	$\pm 0.05 \text{ in. H}_2\text{O}$
$\Delta P_s (+)$	$\pm 0.01 \text{ in. H}_2\text{O}$
$\Delta P_t (**)$	$\pm 0.01 \text{ in. H}_2\text{O}$
$P_{or}$	$\pm 0.01 \text{ in. H}_2\text{O}$
$\Delta P_{or}$	$\pm 0.20 \text{ in. H}_2\text{O}$
$T_{or}$	$\pm 1 \text{ R}$



$T_a$	$\pm 1 \text{ R}$
PT (***)	$\pm 0.1 \text{ in. H}_2\text{O}$

# UNCERTAINTY IN CALCULATED VALUES

$\frac{P^*}{T^*}$	1.9%
$W^*T^{*0.44}$	1.4%
$V/V_{\text{avg}}$	2.5%
(+)	The pressure differential across the secondary flow nozzles, $P_s$ , is the major source of uncertainty in the pumping coefficient.
(++)	The pressure differential across the tertiary flow nozzles, $P_t$ , is the major source of uncertainty in the pumping coefficient.
(+++)	The measurement of the total pressure for the velocity profile is the major source of uncertainty in the velocity calculation.

## APPENDIX: D

### ASME FLOW METERING COMBINATION NUMBERS AND DATA SHEETS

The total cross-sectional area of the ASME long radius nozzles is one of the major inputs for determining the secondary air flow rate. Calculation of these areas as the nozzles are sequentially opened to the atmosphere can be difficult, time consuming, and possibly error prone. To increase accuracy while lowering the data acquisition time, past research was conducted using nozzle combination numbers to represent the areas involved.

Past combination numbers were determined by taking the diameters of the nozzles in use, squaring them, and then dividing by four. For example, if one-four inch and one-eight inch nozzle had been opened,  $4^2 = 16$

$$8^2 = 64$$

$$16 + 64 = 80/4 = 20$$

The combination number, 20, is thus easily calculated and easier still to input into the reduction programs. When multiplied by PI, the area becomes 62.832 square inches.

This research deviated from this past practice by eliminating all calculations in the acquisition process. The combination numbers used for the data sheets and for computer data reduction entry made the flow metering area calculations still easier to use. A set of areas which gave the optimum plotting points for the pumping coefficient plots were

determined, and the number and type of nozzles to be opened for each run were added to the data sheets along with the corresponding combination number. These standard combinations proved effective and efficient during this investigation, and room was left on the data sheets for non-standard combinations should they be needed at a future data. The reduction program uses the actual areas in calculating the secondary air flow, and the pumping coefficient program "PCDSTORE" performs the combination number/area conversion. This was done to allow the older combination numbers to be used again by modifying the smaller, less complicated input program without having to modify the more complex reduction program if such a need should arise.

The reduced size listings of the various combination numbers and corresponding areas are given in Table D-1. Reduced size samples of the data acquisition sheets are provided in Figures D-1, D-2, and D-3. The reduction makes the combination numbers difficult to read under the headings CSEC and CTER for secondary and tertiary combination numbers respectively in Figure D-1, but the ease of use should be apparant.

# ASME FLOW NOZZLE COMBINATIONS

NUMBER OF NOZZLES			AREA (SQ INCHES)	COMBINATION NUMBER	
2 INCH	4 INCH	8 INCH		SECONDARY	TERTIARY
0	0	0	000.000	1	1
1	0	0	3.140	2	2
2	0	0	6.283	3	3
0	1	0	12.566	4	4
1	1	0	15.708	5	5
2	1	0	18.850	6	6
0	2	0	25.133	7	7
1	2	0	28.850	8	8
2	2	0	31.416	9	9
0	3	0	37.699	10	10
1	3	0	40.841	11	11
2	3	0	43.982	12	12
0	0	1	50.265	13	13
1	0	1	53.407	14	14
2	0	1	56.549	15	15
0	1	1	62.832	16	16
1	1	1	65.973	17	17
2	1	1	69.115	18	18
0	2	1	75.398	19	19
1	2	1	78.540	20	20
2	2	1	81.681	21	21
0	3	1	87.965	22	22
1	3	1	91.106	23	23
2	3	1	94.248	24	24
0	0	2	100.531	25	25
1	0	2	103.673	26	26
2	0	2	106.814	27	27
0	1	2	113.097	28	28
1	1	2	116.239	29	29
2	1	2	119.381	30	30
0	2	2	125.664	31	31
1	2	2	128.805	32	32

TABLE D-1 ASME FLOW METERING NOZZLE COMBINATION NUMBERS

# ASME FLOW NOZZLE COMBINATIONS (CONTINUED)

NUMBER OF NOZZLES			AREA (SQ INCHES)	COMBINATION NUMBER	
2 INCH	4 INCH	8 INCH		SECONDARY	TERTIARY
2	2	2	131.947	33	33
0	3	2	138.230	34	34
1	3	2	141.372	35	35
2	3	2	144.513	36	36
0	0	3	150.796	37	--
1	0	3	153.938	38	--
2	0	3	157.080	39	--
0	1	3	163.263	40	--
1	1	3	166.504	41	--
2	1	3	169.646	42	--
0	2	3	175.929	43	--
1	2	3	179.071	44	--
2	2	3	182.212	45	--
0	3	3	188.496	46	--
1	3	3	191.637	47	--
2	3	3	194.779	48	--
0	0	4	201.062	49	--
1	0	4	204.204	50	--
2	0	4	207.345	51	--
0	1	4	213.628	52	--
1	1	4	216.770	53	--
2	1	4	219.911	54	--
0	2	4	226.125	55	--
1	2	4	229.336	56	--
2	2	4	232.478	57	--
0	3	4	238.761	58	--
1	3	4	241.903	59	--
2	3	4	245.044	60	--
DOORS/NOZZLES OPEN			785.000	999	999

TABLE D-1 (CONTINUED)

# **PUMPING COEFFICIENT DATA**

NOZZLE	
TILT ANGLE	(DEG)
ROTATION ANGLE	(DEG)
FLOW AREA	10.752 (IN <sup>2</sup> )

MIXING STACK	
LENGTH	(IN)
DIAMETER	(IN)
L/D RATIO	
S/D RATIO	

ATMOSPHERIC PRESSURE (IN HG)	
START	STOP

AMBIENT TEMPERATURE	
START	STOP
(°F)	(°F)

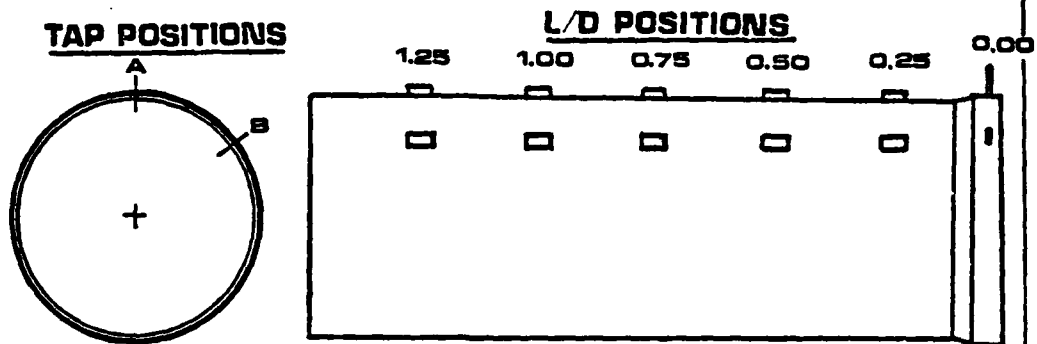
RUN	POR	DPOR	TOR TCN2	TUPT TCN3	PUPT	PSEC SCN1-2	PTER SCN3	CSEC 240-5	CTER 240-5
1								0001	
2								0104	
3								0207	
4								00113	
5								0022	
6								0037	
7								OPEN	
8									
9									
10									

DATE	RUN
------	-----

DATA RECORDER
---------------

FIGURE D-1 SAMPLE PUMPING COEFFICIENT DATA SHEET

## MIXING STACK DATA



L/D POSITION	PRESSURE TAP DATA			
	POSITION A		POSITION B	
	PRESSURE	ROTATION	PRESSURE	ROTATION
0.00	6		7	
0.25	8		9	
0.50	10		11	
0.75	12		13	
1.00	14		15	
1.25	16		17	
1.50	18		19	
1.75				
2.00				
2.25				
2.50				

DATE  RUN

DATA RECORDER

FIGURE D-2 SAMPLE MIXING STACK DATA SHEET

# **VELOCITY TRAVERSE DATA**

**ROTATION ANGLE**   °  

<b>HORIZONTAL</b>		
<b>POSITION</b>		<b>PRESSURE</b> (IN H <sub>2</sub> O)
<b>STD (IN)</b>	<b>NON-STD</b>	
.0		
.2		
.4		
.6		
.8		
1.0		
1.5		
2.0		
2.5		
3.0		
3.5		
4.0		
4.5		
5.0		
5.5		
6.0		
6.5		
7.0		
7.5		
8.0		
8.5		
9.0		
9.5		
10.0		
10.5		
11.0		
11.2		
11.4		
11.6		
11.8		
12.0		

<b>DIAGONAL</b>		
<b>POSITION</b>		<b>PRESSURE</b> (IN H <sub>2</sub> O)
<b>STD (IN)</b>	<b>NON-STD</b>	
.0		
.2		
.4		
.6		
.8		
1.0		
1.5		
2.0		
2.5		
3.0		
3.5		
4.0		
4.5		
5.0		
5.5		
6.0		
6.5		
7.0		
7.5		
8.0		
8.5		
9.0		
9.5		
10.0		
10.5		
11.0		
11.2		
11.4		
11.6		
11.8		
12.0		

**DATE**   **RUN**  

**FIGURE D-3 SAMPLE VELOCITY TRAVERSE DATA SHEET**



## APPENDIX: E

### COMPUTER PROGRAMMING INFORMATION

The research conducted by Ryan [Ref. 5] utilized a semi-automated data acquisition system in the later stages of eductor model testing. The system used the Hewlett Packard HP-85 computer which also served to reduce the data and to plot the results for more detailed analysis. The data input, reduction, and plot programs were designed for the eductor geometries used by Shaw and Ryan in their investigations. With the introduction of the angled nozzles and straight mixing stack, the programs written by Ryan no longer applied. Had more research time been available, the equipment suggested by Ryan to further automate the data acquisition could have been obtained and the programs written for the new geometries. In the configuration and state of automation available at the start of the present research, the semi-automatic data acquisition system actually would have taken longer to acquire the same amount of data that could be taken manually. The decision was reached to place the system in a standby status and to rewrite the necessary programs for the angled nozzles with straight mixing stack. Ryan's programs were left intact and are available on floppy disc Volume: DLRNAN should research be directed toward the symmetric concealment plug concept.

#### A. PROGRAMMING CONCEPTS

The programs written for the angled nozzles and straight mixing stack were designed to be versatile, have room for growth, and to anticipate immediate future needs. As such, they were written for full secondary and tertiary flow data reduction, plotting, and comparison vice to fulfill just the secondary data reduction and plotting needed in this research. The programs were written to maximize man-machine interfacing. Operators with little skill in the HP Basic Language used should have no problems entering data, reducing the inputs, storing the outputs, and generating the numerous plots required for this particular research. Each program was designed to ask simple questions on the computer's display screen, give the possible answer of data input formats, and provide numerous data error correction techniques. The data sheets listed in Appendix D, Figures D-1, D-2, and D-3 were designed to further assist the data acquisition process by providing blanks or spaces in the same order that the particular programs would ask for data entry. The programs were written so that all data entry, reduction, and plotting routines were located on one floppy disc and the temporary and permanent data files were stored on another floppy disc. This feature was incorporated to allow future researchers to store their data on their own individual floppy disc, prevent filling the disc during a data run, and allow easier data comparison with past research files.

## B. OPERATING PROCEDURES

Each program contains its own instructions. The programs are loaded by the LOAD command. For example, to load the program to store the pumping coefficient data, the operator would type in LOAD "PCDSTORE" and press the ENDLINE key. After the program is loaded, the operator could press the LIST key to see what capabilities are present. The operator could have also pressed the RUN key if the capabilities were already known. Once the program is running, the operator just has to make basic decisions and answer simple questions.

The programs are generally used in the following order and this sequence is strongly recommended:

PCDSTORE	Enters all of the header information/data for the pumping coefficients. It also converts combination numbers to actual metering flow nozzle areas.
MSDSTORE	Enters data for the mixing stack pressure and flow rotation distributions.
VTDSTORE	Enters data for the two velocity traverse profiles.
DRPSMS	Asks if mixing stack data and velocity traverse data are to be reduced, and it then runs for about 20 minutes reducing the data, placing the data into temporary files, printing about eight feet of output formatted for the thesis requirements, and includes up to six mini-plots for immediate comparison.
DATSTORE	Reads all of the data for the particular run, sorts out the data needed for graphical comparison, and then permanently stores the comparison data.

SEC PLOT	Allows stored data retrieval or manual data input comparisons of secondary flow pumping coefficients with capability to add comments located by the same units used to graph the data.
TER PLOT	Identical to SEC PLOT except it plots the tertiary pumping coefficient comparisons.
MSD PLOT	Identical to SEC PLOT except it plots the mixing stack pressure distributions in many different data combinations.
ROT PLOT	Same type program as MSD PLOT but plots the rotation angle distributions.
VTD PLOT	Plots only stored velocity profile data which cannot be compared with other data since the velocities are not dimensionless. It does have the option to compare the horizontal and diagonal velocity profiles, and allows comments to be added like the other programs.
FIG COM	Allows adding figure or table numbers to finished plots or tables, adding comments which may have been left out, and has the option of locating these inputs on the plots by manually entering X-Y coordinates in plotter units or by using the digitizing feature of the plotter.
INITIALIZE	Initializes new floppy discs for data storage with properly dimensional memory allocations for the six temporary input/output storage files. It has several safeguards to prevent accidental purging of valuable data.
AUX PLOT	Plots the pumping coefficients by nozzle tilt/rotation angles for the summary plots. It has only manual data entry capability but retains comment addition similar to the other programs.

The INITIALIZE program would only be used once per thesis as sufficient memory is available on one floppy disc to handle all the data that could be taken over a six month span. FIGCOM and AUXPLOT are used mainly after all of the plots have been analyzed and finished products and summaries are desired.

For the inexperienced operator, a listing of programs can be obtained by typing in CAT and pressing ENDLINE with the program storage disc in the DRIVE 0 slot on the HP 82901M Flexible Disc Drive. Data listings can be obtained by typing CAT".DRIVE1.D701" and pressing ENDLINE with the data disc the DRIVE 1 slot on the disc drive. Further operating instructions can be found in the various operating manuals.

#### C. DATA FILES

Data files for this research period as stored on floppy disc Volume:DRIVE1 which is disc number two in the research manual. The information is stored by date-time-group and run number. For example, data for the pumping coefficients (secondary and tertiary) for the fourth data run on 26 August 1981 would be stored as P2608814. To facilitate future comparisons with the data derived during this research period, the data available and the file numbers are listed in the Summary of Tabulated Data which can be found in Tables 1.1, 1.2, and 1.3.

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